ASX ANNOUNCEMENT 10 MAR 2026

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Victory Delivers Project's Highest REE Intersection to Date 11,565ppm

Victory Metals Limited (ASX:VTM) is proud to announce this exceptional 11,565 ppm TREO peak intersection as a standout achievement, reinforcing North Stanmore's position as one of the highest-grade regolith clay-hosted heavy rare earth projects worldwide. Combined with shallow mineralisation, high heavy REE/total REE ratios, low radioactivity and demonstrated metallurgical success, these results significantly enhance the project's development potential and strategic value in securing Western supply chains for critical rare earth elements.

HIGHLIGHTS

- **Record breaking intercept** being the highest total rare earth oxide (TREO) grade ever recorded at North Stanmore totalling **11,565ppm from 15m depth, world class for a clay hosted heavy rare earth project.**
- **Additional exceptional shallow intersections**
  - **5m @ 3,312 ppm** (hole 2025IFAC017) from 15m
    - 1m @ 11,565ppm from 15m
  - **5m @ 1,278 ppm** (hole 2025IFAC015) from 15m
  - **13m @ 821 ppm** (hole 2025IFAC047) from 18m
  - **22m @ 781 ppm** (hole 2025IFAC050) from 13m
- **These results coupled with Victory's 48x upgrade bring the project exceptional value.** [1]
- This ultrahigh grade zone ranks among the **highest heavy rare earth enriched peak grades reported globally in clay hosted** where typical resource grades range from **500–2,500 ppm TREO** and peak intervals rarely exceed several thousand ppm in most global peers.
- Continuity confirmed over **~1km strike** in the southwestern high grade heavy rare earth zone, reinforcing North Stanmore's status as a **world-class heavy REE-enriched clay hosted system**.
- 63 hole aircore infill program (3,134m) successfully tightens central deposit spacing to 100m N × 50m E, **paving the way for Measured Resource classification post PFS modifying factors.**
- **Shallow depths, subhorizontal geometry, high heavy REE ratios, low radioactivity, and proven rapid leach kinetics position North Stanmore as a premier non-Chinese source** of critical heavy rare earths (Dy, Tb, Y), Scandium & Hafnium.

[1] Refer to ASX announcement dated 3rd March 2026 titled "48x Rare Earth Upgrade to 5.9% TREO.

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Victory Metals Chief Executive Officer and Executive Director Brendan Clark commented: "*This is a landmark result for North Stanmore. Achieving our highest TREO grade to date with a peak of over 11,500ppm TREO in a clay hosted system is truly world class and places us among the elite globally, especially with our heavy rare earth ratios. In a market desperate for secure, non-Chinese sources of heavy rare earths like dysprosium, terbium, and yttrium, North Stanmore's combination of exceptional grades, shallow depths, and processing advantages positions us as a standout future supplier. We are excited to advance this transformative asset through PFS and into production.*"

December 2025 Drill Program

Victory Metals completed an aircore drill programme at North Stanmore REE project of 63 drillholes for 3,134m in December of 2025.

The drill programme was designed to achieve potential conversion of Indicated Mineral resources to Measured Mineral resources, with the drill spacing closed to 100m N x 50m E in the central area of the deposit. This spacing will allow the reporting of a section of the Mineral Resource as Measured Resources when the PFS modifying factor studies have been completed.

Assays reported today total 1,001m with 4 drillholes remaining and expected to be reported in March 2026.

Figure 1. Bostech Drillings AC drill rig at North Stanmore along with zero impact full rehabilitation equipment.

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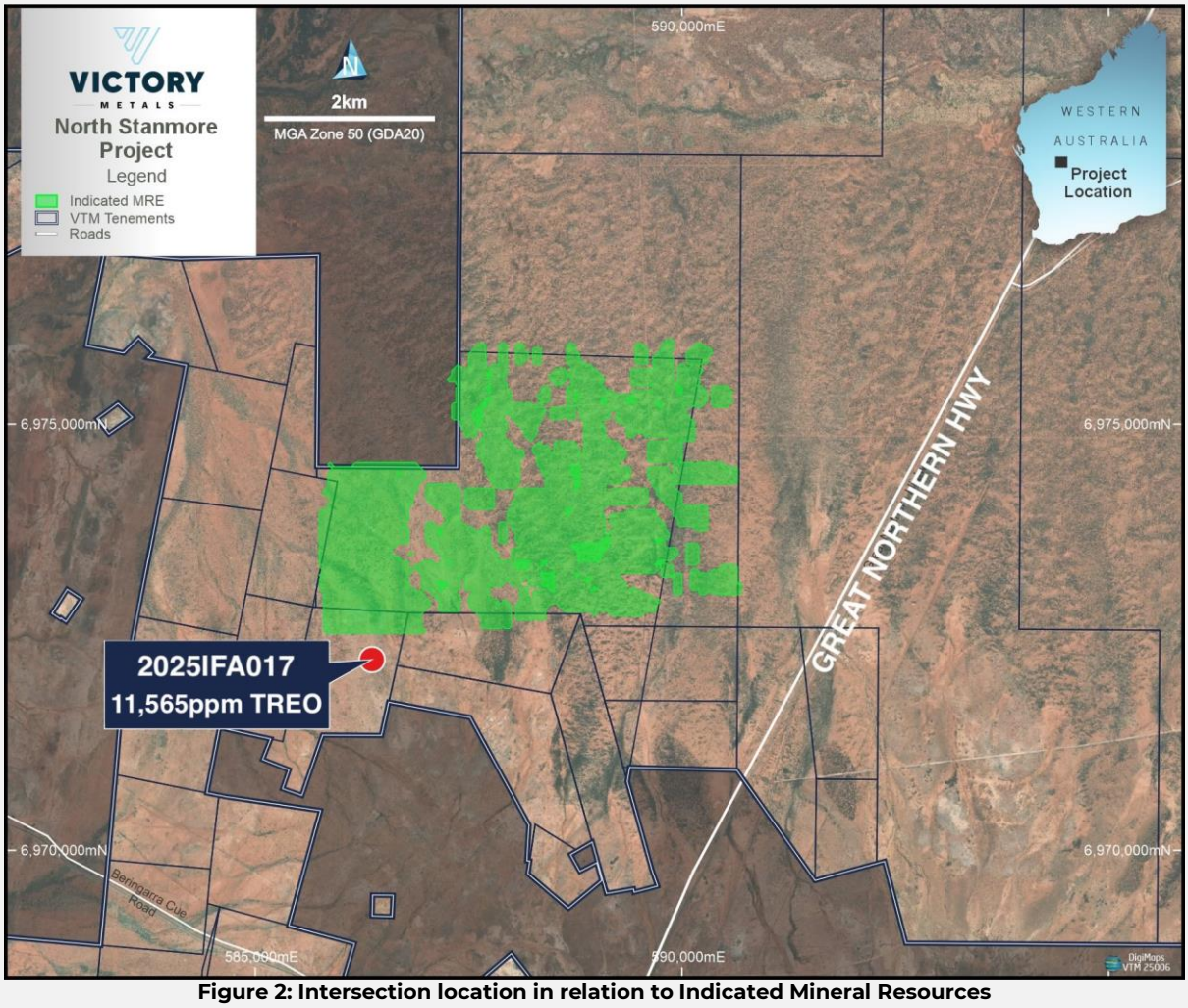

Figure 2: Intersection location in relation to Indicated Mineral Resources

Assays Confirm Mineralogical Control on HREE Composition

HREO/TREO ratio versus TREO concentrations of the in-fill drilling assays are plotted in Figure 3. They clearly show that the majority of the regolith assays are HREE enriched, with HREO/TREO ratios >24% and ranging up to ~90%. In addition to the presence of ~26% of AMUSUL soluble ionically bonded REEs in North Stanmore regolith clays, there is also a strong mineralogical control on REE distribution due to the presence of secondary phosphate minerals and relict zircon.

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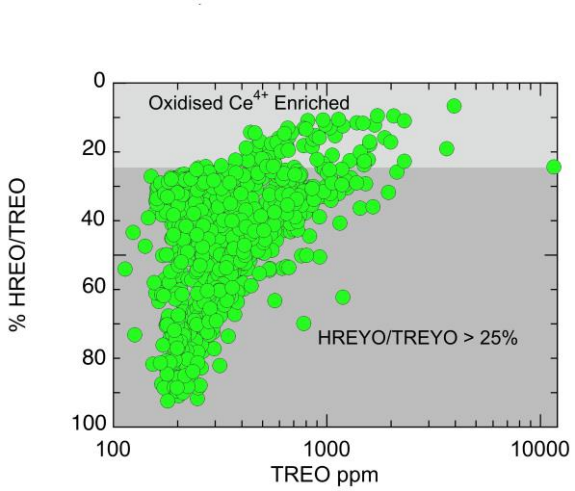

Figure 3: Plot of HREO/TREO ratio versus TREO content of the In Fill drilling assays.

The extreme range in HREO/TREO ratios shown in Figure 3, reflects the presence of variable amounts of Rhabdophane (after monazite) and Churchite (after xenotime) formed by oxidation. However, samples with very high HREO/TREO ratios >~55% also reflect the presence of primary relic zircon. This mineralogical control is shown in Figure 3.

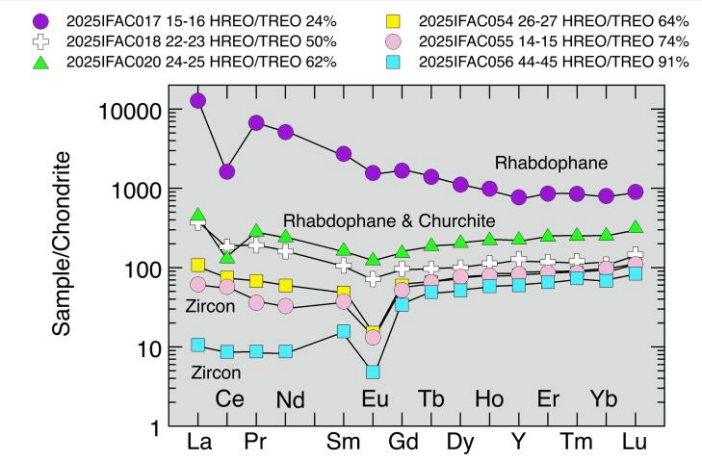

Figure 4: Chondrite normalised plot showing variation in REE patterns for Infill drilling samples with HREO/TREO ratios ranging from 24% to 91%.

The Chondrite normalised plot (Figure 4) identifies variation in REE patterns for Infill drilling samples with HREO/TREO ratios ranging from 24% to 91%. The rhabdophane and churchite bearing samples all show deviations in REE profiles between La and Pr indicating loss of Ce^{4+}due to oxidation during chemical weathering. The zircon bearing samples show no deviation in REE profiles between La and Pr indicating that relict zircon of primary igneous origin is also present in the North Stanmore regolith.

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Knowledge of this mineralogical control on REE distribution has greatly assisted the metallurgical test work reported previously.

This announcement has been authorised by the Board of Victory Metals Limited.

For further information please contact:

Brendan Clark
CEO and Executive Director
admin@victorymetalsaustralia.com

Jim Carden
Investor and Media Relations
jimc@bastionagency.com

Victory Metals Limited

Victory is dedicated to the exploration and development of its flagship North Stanmore Heavy Rare Earth Elements (HREE), Scandium, Hafnium and Gallium Project located in the Cue Region of Western Australia. The Company is committed to advancing this world-class project to unlock its significant potential.

In August 2025, Victory Metals announced a robust Mineral Resource Estimate (MRE) for North Stanmore, totalling 320.6 million tonnes, with the majority of the resource, classified in the indicated category. This positions the North Stanmore Project as Australia's largest indicated clay heavy rare earth resource, underscoring its pivotal role as a future supplier of critical materials for the future.

North Stanmore Mineral Resource Estimate

Table 1: North Stanmore August 2025 MRE (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREOSc (ppm)	TREO (ppm)	HREO (ppm)	LREO (ppm)	HREO/TREO (%)	Sc_2O_3 (ppm)	Ga_2O_3 (ppm)
INDICATED	176,522,000	532	505	190	316	39	26	26
INFERRED	144,118,000	484	463	166	297	37	21	25

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Forward-looking statements

This announcement contains "forward-looking statements". All statements other than those of historical facts included in this announcement are forward-looking statements. Where a company expresses or implies an expectation or belief as to future events or results, such expectation or belief is expressed in good faith and believed to have a reasonable basis. However, forward-looking statements are subject to risks, uncertainties and other factors, which could cause actual results to differ materially from future results expressed, projected or implied by such forward-looking statements. Such risks include, but are not limited to, metals price volatility, currency fluctuations, increased production costs and variances in ore grade or recovery rates from those assumed in mining plans, as well as political and operational risks and governmental regulation and judicial outcomes. Neither company undertakes any obligation to release publicly any revisions to any "forward-looking" statement.

Competent Person Statement - Geochemistry results

Statements contained in this report relating to metallurgy results, scientific evaluation, and potential, are based on information compiled and evaluated by Emeritus Professor Ken Collerson. Professor Collerson (PhD) Principal of KDC Geo Consulting and Director of Victory Metals Limited, and a Fellow of the Australasian Institute of Mining and Metallurgy (AusIMM No. 100125), is a geochemist/geologist with sufficient relevant experience in relation to rare earth element and critical metal mineralisation being reported on, to qualify as a Competent Person as defined in the Australian Code for Reporting of Identified Mineral resources and Ore reserves (JORC Code 2012). Professor Collerson consents to the use of this information in this report in the form and context in which it appears.

Competent Persons statement – Exploration results

Information contained in this document relating to Exploration results is based on information that has been compiled by Mr Dean O'Keefe who is a Fellow of the Australasian Institute of Mining and Metallurgy (#112948). Mr O'Keefe is contracted full time to Victory Metals as Chief Technical Officer. Mr O'Keefe has sufficient experience which is relevant to the style of mineralization and type of deposit under consideration and to the activity being undertaken to qualify as the Competent Person as defined in the 2012 edition of the Australasian code for the reporting of exploration results, Mineral Resources and Ore Reserves. Mr O'Keefe consents to disclosure of the information in this report in the form and content in which it appears.

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APPENDIX 1: 2012 JORC CODE

Table 1: JORC Code

Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as downhole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g*	• Note that at the time of compiling Table 1 and reporting of significant results that 5 drillholes in the north of the project were still pending assay return, drillholes 2025IFAC059 to 63. • (AC) Air core drillholes were drilled vertically and spaced 100m apart along 200m - 400m spaced drill lines. • (AC) drilling samples were collected as 1-m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite. • Each sample was then split using a 3-tier (87.5% - 12.5%) splitter and the split sample was placed into calico sample bags for transport to Perth. • Sample weights and recoveries were recorded on site and weighed 1.5 - 2.5 kg depending on the sample recovery from the drill hole. The mean bulk sample weight was 8.45kg. • A commercial transport company was used to transport the bags to the Victory warehouse in Perth. • A handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REO (Rare earth element) geochemistry (La, Ce, Pr, Nd and Y) from the 1-m sample piles. pXRF reading times were 45 secs over 3 cycles for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their integrity was checked using Certified REO -bearing geochemical standards. • The handheld pXRF is used as a guide to the relative presence or absence of certain elements, including REOs vectors (La, Ce, Pr, Nd and Y) to help direct the sampling program. Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. REO anomalism thresholds are determined by VTM technical lead based on historical data analysis. Currently the anomaly threshold is plus 30ppm Yttrium. • Victory attended North Stanmore to collect the green sample bag which was transported by Victory to Victory's secure warehouse in Perth. • Measures taken to ensure sample representivity included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight. • RC drill samples were collected as 1-m samples from the rig cyclone and placed on top of black plastic, which was laid on the natural ground surface to prevent contamination, in separate piles and in

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	charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information	orderly rows. A hand-held trowel was used to collect 4-m composite samples from the 1-m piles. Compositing did not account for lithology changes. These composite samples weighed between 2 and 3 kg.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	• (AC) drilling uses a three bladed steel or tungsten drill bit to penetrate the weathered layer of loose soil and rock fragments. The drill rods are hollow and have an inner tube with an outer barrel (similar to RC drilling). • (AC) drilling uses small compressors (750 cfm/250 psi) to drill holes into the weathered layer of loose soil and fragments of rock. • (RC) Drilling used a 5½" face sampling hammer with 1,350cfm/500 psi onboard compressor, which was occasionally supplemented with an additional booster (2,100cfm/1,000 psi). • After drilling is complete, an injection of compressed air is unleashed into the space between the inner tube and the drill rods inside wall, which flushes the cuttings up and out of the drill hole through the rod's inner tube, resulting in less chance of cross-contamination. • (AC) Drilling was conducted by Bostech Drilling for the 63 drillhole programme. • The drill rigs were inspected daily by VTM personnel for safety and rig hygiene
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and*	• The majority of samples were dry, where excessive water flows were encountered during drilling the sample recovery was variable. The depth that water was encountered was recorded in the database. • Representative percussion drillhole samples were collected as 1-metre intervals, with corresponding chips placed into chip trays and kept for reference at VTM's facilities. • Measures taken to ensure sample representivity and recovery included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.

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	whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	• All percussion samples in the chip trays were lithologically logged using standard industry logging software on a notebook computer. • All (AC) samples have been logged for lithology, alteration, quartz veins, colour, fabrics. • All (AC) samples have been analysed by a handheld pXRF. • All samples were subjected to a NIR spectrometer for the identification of minerals and the variations in mineral chemistry to detect alteration assemblages and regolith profiles. • All geological information noted above has been reviewed by a competent person as recognised by JORC.
	• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.*	• Logging is qualitative in nature. • (AC) samples have been photographed.
	• *The total length and percentage of the relevant intersections logged.*	• 90% of the sample intervals were logged.
Subsampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.*	• Diamond drilling was PQ core. • Half core samples were taken, with the exception of when twin samples were collected and then the samples were quarter core.
	• *If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.*	• Air core and RC sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. • Samples from the cyclone were placed into green drill bags and were laid out in orderly rows on the ground. • Using a hand-held trowel, 1m samples were collected from the one-metre drill bags after splitting of the sample. • These samples were placed into calico bags and weighed between 1.5 and 2.5 kgs.
	• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*	• Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory. The assay methods used include: o ME-4ACD81: Four acid digestion followed by ICP-AES measurement o ME-MS81: Lithium borate fusion followed by acid dissolution and ICPMS measurement o ME-ICP06: Fusion decomposition followed by ICP-OES measurement

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		• REOs were all analysed by ME-MS81 (four acid digestion followed by ICPMS measurement) with results returned in their elemental form. Elements were then converted to oxides using the appropriate stoichiometric conversion factors. • Base metals are assayed by ME-ICP06: Fusion decomposition. • Non-ferrous metals are assayed by ME-4ACD81: Four acid digestion.
	• *Quality control procedures adopted for all subsampling stages to maximise representivity of samples.*	• Using a riffle splitter, 1m composite samples were collected from the individual sample bags. • Quality control of the assaying comprised the collection of a bulk repeat sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples. The repeat sample was collected by passing the bulk reject obtained from the first split stage through the riffle splitter once more. The repeat sample is not a duplicate.
	• *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.*	• Fourteen twin samples of quarter core (diamond PQ) were compared to the original sample for each REO element and results were found to be acceptable to the CP.
	• *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Composite samples weighed between 1 and 2 Kg's. • Sample sizes are considered appropriate to the grain size of the material being sampled.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	• All samples were analysed in the field using a handheld Olympus Vanta XRF unit to identify geochemical thresholds. These results are not considered dependable without calibration using chemical analysis. They were used as a guide to the relative presence or absence of certain elements, including REOs to help guide the drill program and selection of samples to be submitted for analytical analysis. • All pXRF anomalous samples were sent to ALS Wangara in Perth for analysis. Over time the mineralised sample criteria has evolved from an initial sampling threshold value of La+Ce+Nd+Pr+Y > 200ppm (for the RSC MRE), to Ce>30ppm (for the post RSC to July 2024 MRE), and most recently Y>30ppm (POST July 2024 to July 2025 MRE). • Samples were submitted for sample preparation and geochemical analysis by ALS in Wangara, Perth, a NATA accredited laboratory. All samples were crushed and pulverized to generate a pulp aliquot

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		sample with 95% of the aliquot sample passing 75µ (ALS methods CRU-31, PUL-31). Aliquots were analysed using the following methods: o Lithium borate fusion prior to acid dissolution and ICPMS (ALS method ME-MS81, a total assay technique) for Ba, Ce, Cr, Cs, Dy, Er, Eu, Ga, Gd, Hf, Ho, La, Lu, Nb, Nd, Pr, Rb, Sc, Sm, Sn, Sr, Ta, Tb, Th, Ti, Tm, U, V, W, Y, Yb, and Zr. o Lithium borate fusion prior to acid dissolution and ICPOES (ALS method ME-ICP06, a total assay technique) for Al2O3, BaO, CaO, Cr2O3, Fe2O3, K2O, MgO, MnO, Na2O, P2O5, SiO2, SrO, TiO2, and Total. o 4-acid digest and read by ICP-AES (ALS method ME-4ACD81, a partial assay technique) for Ag, As, Cd, Co, Cu, Li, Mo, Ni, Pb, Sc, Tl, and Zn (base metals). o Thermogravimetric analysis to determine loss on ignition (LOI) content. • The sample preparation and analysis are considered appropriate for the analytes. • As a result of the pXRF analysis leading the selection criteria for assaying by a laboratory, only 16,620 metres of drilling of the total 45,340 drill metres (or 37% of total metres) has been assayed.
	• *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	• At Victory's Perth facility spot checks were completed on selected samples using a handheld Olympus Vanta XRF unit. The pXRF device was used to determine anomalous REO geochemistry (La, Ce, Nd, Pr and Y) from the 1-m sample piles. • pXRF reading times were 45 secs over 3 beams for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their analytical accuracy was checked using REO -bearing geochemical standards. • The pXRF results were not used for estimation.
	• *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Sample weights were measured for 174 of the AC drillholes, and recovery was measured for 7 of the diamond drillholes. Sample recovery for the diamond drillholes recovery was 100 %. Based on the information available, sample recovery is acceptable for the diamond holes. • Assay analytical precision was established by laboratory repeats and was deemed acceptable to the Competent Person. • OREAS 464 is a high grade ore, rare earth element (TREO = 5.10%) matrix-matched certified reference material (MMCRM) prepared and certified by Ore Research & Exploration. OREAS 461 is an ore grade, rare earth element (TREO = 1.06%) matrix-matched certified reference material (MMCRM) prepared and certified by Ore Research & Exploration. The materials constituting OREAS 464 were sourced from Lynas

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		Corporation's Mount Weld Project (the 'Central Lanthanide Deposit') which is located 35 kilometres south of Laverton in Western Australia. The Mount Weld source materials (waste, low and medium grade REE ores) were found to be highly hygroscopic to the extent that significant analytical errors would likely result during analysis unless strict moisture handling procedures were adhered. To avoid this complication, the hygroscopic property was destroyed by roasting the materials at 900°C for 2 hours. o The overall performance of standards was deemed to be acceptable. It was noted that Y in the CRM OREAS461 have expected values above the detection limits of the lab method ME_MS81. Dy and Tb were within action limits. o OREAS464 which is a higher grade standard returned good results within limits for Y, Dy, and Tb. • The overall performance of the blanks was deemed to be acceptable to the CP. There was a small increase in Yttrium values observed and no increase in values such as terbium and dysprosium. • Field diamond duplicate data points taken from the same drillholes is available only for 14 samples from diamond drill core. The mean grade of the original sample was generally reproduced by the duplicate for the various analytes and is acceptable to the Competent Person. • In April 2024, 37 samples were submitted to an umpire laboratory, Intertek Genalysis in Perth. The results were compared to the original assay results from ALS laboratories for the key analytes of interest to the project. There was no observable bias between the original assays completed by ALS and the checks completed by Intertek Genalysis Perth. • There are 14 duplicates collected over the entire project drilling campaign. • Assays for the 63 drillholes were completed at ALS.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.*	• Victory's representative Prof Kenneth Collerson (PhD, FAusIMM) undertook verification of significant intersections.
	• *The use of twinned holes.*	• Eleven percussion (air core and RC) drillholes have been twinned with diamond drilling (DD001 to DD011). Samples were submitted to the laboratory for analysis only where the initial screening by handheld pXRF satisfied the anomalous value threshold as set by company policy, whereas the diamond drilling was sampled and assayed along the entire length of the drillhole. • QQ plots were prepared between the percussion and diamond assays paired at 5m, with good correlation between the two drillhole types.

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	• *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*	• ALS laboratories routinely re-assayed anomalous assays as part of their normal QAQC procedures
	• *Discuss any adjustment to assay data.*	• REO assay results were adjusted to convert elemental values to the oxide equivalent for REOs. The oxide stoichiometric conversion factors used are provided below:
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	• 51% of the drillholes were surveyed by RTK/DGPS. The remaining holes were surveyed by handheld GPS with a horizontal accuracy of +/- 5 m. Elevation values (Z) were assigned from the topography surface where no DGPS data was available. • There were no downhole surveys completed. Drillholes were both vertical and inclined. The majority of drill intervals (99%) were to a drill hole depth of less than 100m. Downhole survey was completed for the diamond drillholes.
	• *Specification of the grid system used.*	• All coordinates are in GDA94 Zone 50.
	• *Quality and adequacy of topographic control.*	• A LiDAR based DEM has been produced for the project.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.*	• The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m.
	• *Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*	• Given the nature of the exploration programs, the spacing of the exploration drilling is appropriate for understanding the exploration potential and the identification of structural controls on the mineralisation. In areas of closer spaced drilling the spacing demonstrates grade and geological continuity sufficient to support Indicated Mineral Resources. Where drillhole spacing increases, grade and geological continuity can be implied and has been classified as an Inferred Mineral Resource. Areas where the drillhole spacing is such that grade and geological continuity cannot be implied, were excluded from the Mineral Resource. • The applied Mineral Resource classification is commensurate with the grade continuity demonstrated.
	• *Whether sample compositing has been applied.*	• Percussion samples were collected as 1.0 m samples. Core was collected at a nominal 1.0 m samples. Air core samples were collected as 1.0 m and 4.0 m samples.

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Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	• Mineralisation is sub horizontal, as such the vertical drillholes are suitable to test mineralisation thickness. • It is concluded from aerial magnetics that the mineralisation trends 010°-030°. • Air core drilling was vertical as the mineralisation is interpreted to be sub parallel to the regolith profile. RC percussion drilling was angled. • Downhole widths of mineralisation are known with percussion drilling methods to +/- 1 metre.
	• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Mineralisation is sub-horizontal. Azimuths and dips of drilling was designed to intersect the strike of the rocks at right angles.
Sample security	• *The measures taken to ensure sample security.*	• All samples were packaged and managed by VTM personnel. • Larger packages of samples were couriered to Core from Cue by professional transport companies in sealed bulka bags. • Unused samples from the percussion drilling are stored at Victory's secure warehouse in Perth.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• MEC conducted an audit of the project data and the historic MRE in April of 2024. The findings were as follows - o Several validation issues have now been corrected in the drillhole database, and the data is of sufficient quality to inform an Indicated and Inferred mineral resource. o There are no downhole surveys so there is a risk of the hole paths deviating from planned, particularly with the deeper drillholes >100m which account for less than 1% of all drilled metres. • MEC completed a further review upon the completion of the 2025 drilling which focussed on the adequateness of lithological logging procedures in order to produce accurate bottom of hole (bedrock) lithology map and to qualify the rock hardness to allow a rock model to be generated.

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Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The North Stanmore REO Project MRE comprises ten tenements E20/0544, E20/0871, E20/0971, E20/1016, E20/2468, E20/2469, P20/0543, P20/2007, P20/2153, and P20/2403. The 63 drillholes were completed on E20/0871, P20/2468, P20/2469, M20/0494, M20/543, P20/2007, and P 20/215. • All tenements are held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory Metals Ltd. MEC has verified that at the time of the report date that all tenements are currently in good standing. • Native Title claim WC2004/010 (Wajarri Yamatji #1) was registered by the Yaatji Marlpa Aboriginal Corp in 2004 and covers the entire project area, including Coodardy and Emily Wells.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• The area has been previously explored by Harmony Gold (2007-2010) in JV with Big Bell Ops, Mt Kersey (1994- 1996), and Westgold (2011), and Metals X (2013). • Exploration by these companies has been piecemeal and not regionally systematic. • Harmony Gold intersected 3m @ 2.5 g/t Au and 2m @ 8.85 g/t Au in the Mafeking Bore area but did not follow up these intersections. • Other historical drill holes in the area commonly intersected > 100 ppb Au. • There has been no historical exploration for REOs in the tenement.
Geology	• *Deposit type, geological setting and style of mineralisation*	• Victory's tenements lie north of Cue, within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgaranga greenstone belts, the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late faults. The greenstone belts were intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions.

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		• Two large Archaean gabbroid intrusions occur south of Cue. These are the Dalgaranga-Mount Farmer gabbroid complex in the southwest, and the layered Windimurra gabbroid complex in the southeast. The North Stanmore alkaline intrusion, north of Cue, was not recognised on regional geological maps. The petrological and geochemical data indicate that it is post-tectonic and post Archean in age. Similar alkaline intrusions in the vicinity of Cue are interpreted to be related to the early Proterozoic plume track responsible for alkaline magmatism, which extends in a belt from Mt Weld through Leonora to Cue. • Mafic and ultramafic sills are abundant in all areas of the Cue greenstones. Gabbro sills are often differentiated with basal pyroxenite and/or peridotite and upper leucogabbric units. • The greenstones are deformed by large scale fold structures which are dissected by major faults and shear zones which can be mineralised. Two large suites of granitoids intrude the greenstone belts. • The western margin of the project has a signature reflecting a rhyolite, rhyolite-dacite and/or dacitic rock (predominantly acid or felsic rock type). This coincides with an area of elevated TREO/LREO/HREO grades and greater average mineralisation thickness. • The deposit type is regolith-hosted REO mineralisation overlying the North Stanmore alkaline intrusion. The REO mineralisation at North Stanmore is predominantly hosted within a relatively flat-laying saprolite-clay horizon and partially extends into the Sap rock. The Saprolite is covered by 0–36m of unconsolidated colluvium. The saprolite thickness ranges from 14–58m, and overlies a basement of granite, mafic rocks, and other felsic rocks. Mineralogy studies demonstrate that the REOs are mainly hosted by sub-20-µm phases interpreted to be churchite (after xenotime) and rhabdophane (after monazite). The mineralisation is hosted in the saprolite zone of the weathering profile, between the basement granite and surface colluvium.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*	• Eight hundred and thirty four (834) drill holes for 45,339.9m, inclusive of 773 Air-core (AC) drillholes for 41,409m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m were available for the MRE. Drillhole depths range from 3m to 222m. All drillholes were completed by Victory from 2022 to 2025.

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	o *easting and northing of the drill hole collar* o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* o *dip and azimuth of the hole* o *down hole length and interception depth* o *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• The North Stanmore drilling completed to the end of December 2025 is shown as follows -
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g., cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• No top cuts were applied as few extreme values were identified. • Samples were composited to 1 m intervals based on the dominant raw sample length. • A geological cutoff grade of 150ppm TREO + Sc representing the on-set of mineralisation was used during interpretation to separate mineralised from unmineralised material for the MIN domain. A high-grade (HGMIN) domain was modelled above a TREO + Sc 600ppm cut-off. • All MRE were reported above an economic cut-off grade of 330ppm TREO + Sc.
Relationship between mineralisation	• *These relationships are particularly important in*	• The clay regolith hosted REO mineralisation is interpreted to be sub horizontal.

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widths and intercept lengths	*the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• Intersections approximate the true width of mineralised lodes.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views*	Drillhole collars and tenements are shown below – Drillhole collars for the 63 December 2025 drill programme are shown below - Section lines in plan view and section are shown below Section line 1, looking north, vertical exaggeration x5 Section line 2, looking north, vertical exaggeration x5 Section line 3, looking north, vertical exaggeration x5 Drillhole coordinates are shown in the APPENDIX *Table 2*. These coordinates are planned locations and final survey pickup has not been completed at the time of Announcement release.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All significant intersections have been reported above a 330ppm TREO + Sc cut-off, with a minimum intersection of 2m (APPENDIX *Table 3*).
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical*	• Metallurgical testwork: o Three stages of metallurgical test work have been completed on the North Stanmore project, focusing on beneficiation, and on leach test work to establish potential recoveries o Core Resources ("Core") in Brisbane completed Stage 3 test work

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	survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances	including beneficiation test work in March of 2024 and reported an increase, to the Rare Earth Element ("REO") feed grade of 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material. o The Leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide plus Yttrium (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trialled at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREO"). o Additionally, Scandium oxide (Sc_2O_3) recoveries of (50%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO and Sc_2O_3 from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Further metallurgical testwork will focus on further optimization of the leaching of the upgraded samples and the generation of Mixed Rare Earth Carbonate (MREC) for potential off takers. Additional variability leach testing of individual samples is also planned. Variability leach testwork will inform geo-metallurgical variability across the North Stanmore project. Further metallurgical test work will also focus on the most optimized leaching conditions and removal of gangue materials against the higher rare earth extractions that can be achieved. • A Prefeasibility study is currently in progress.

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Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	• An initial Database was supplied to MEC by RSC, the database was then integrated with newly acquired data by MEC for a data audit before commencing an MRE. All validation issues relating to data were identified and remedied prior to MRE. • Data was stored in an Access relational database.
	• *Data validation procedures used.*	• Drillhole collar, downhole survey, assay, geology, and recovery data were imported into Micromine software. • The imported data was then compared to the database values with no discrepancies identified. • The data was then desurveyed in Micromine and reviewed spatially with no discrepancies identified.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	• Dean O'Keefe, the Competent Person for the Mineral Resource Estimate visited the North Stanmore project site on May 30, 2024, December of 2025, and February of 2026.
	• *If no site visits have been undertaken indicate why this is the case.*	• Multiple site visits have been conducted by the Competent Person, Dean O'Keefe.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	• Confidence in the interpretation of the transported colluvium that truncates the saprolite is commensurate with the drillhole spacing and ranges from low to moderate confidence. • The mineralisation is hosted within the saprolite and sap rock, with some mineralisation extending into the bedrock. • There is reasonable confidence in the interpretation of the saprolite commensurate with the available drilling.
	• *Nature of the data used and of any assumptions made.*	• Surface AC, RC, as well as diamond drilling, have been used to inform the MRE.
	• *The effect, if any, of alternative interpretations on Mineral Resource estimation.*	• The potential for alternate interpretations at a prospect scale is considered unlikely. However, there is a likelihood of variation at the local scale, and this has been reflected in the Mineral Resource classification.
	• *The use of geology in guiding and controlling Mineral Resource estimation.*	• The MRE has been interpreted as mineralised domains (MIN) representing the on-set of REO mineralisation at 150ppm TREO + Sc_2O_3, and high-grade pods (HGMIN) within the

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	• *The factors affecting continuity both of grade and geology.*	mineralised domains where the mineralisation grade is greater than 600ppm TREO + Sc_2O_3.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The North Stanmore deposit extends over 8km across and along strike and is around 70m thick; mineralisation varies between 4m to 60m in true thickness. • The southwestern part of the deposit is thicker than the remainder of the deposit.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*	• The final interpretational wireframes and estimation work was completed using Micromine v2025.5. • The estimation was constrained by hard domain boundaries generated from mineralisation wireframes. • The available samples were coded by domains (HGMIN, MIN), and 1.0m composites were created honouring these boundaries. • The REO analyte grades were estimated using ordinary kriging of the 1.0m composite grades each of the individual REO grades: HREO, and LREO. • The estimation for additional elements was completed using Inverse Distance Cubed for Cu, Ni, Co, Hf, Sc_2O_3, and Ga_2O_3. • There were no extreme values observed that required topcuts to be applied. • For estimation purposes, all boundaries were treated as hard boundaries. • The primary search was 500 m in the direction of maximum continuity, 400 m along the intermediate direction of continuity, and 25 m in the minor direction of continuity. Up to 5 samples per octant sector (maximum number of informing samples was 40 samples) were used. • The secondary search was 1,000 m in the direction of maximum continuity, 800 m along the intermediate direction of continuity, and 50 m in the minor direction of continuity, up to 5 samples per octant sector (maximum of 40 informing samples) was used. • The third search was 1,500 m in the direction of maximum continuity, 1,200 m along the intermediate direction of continuity, and 75m in the minor direction of continuity, with a maximum of 150 informing samples (no octant search applied). • The maximum distance for extrapolation for the Inferred Mineral Resource was 1,500 m. • Values were calculated for HREO, LREO, and TREO + Sc by summing the respective REO estimated grades and Scandium oxide for each OBM block.

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	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*	• The June 2025 MEC MRE was compared to the January 2025 MEC MRE's. • The January 2025 MRE compared to the July 2025 MRE has the same Indicated Mineral Resources tonnage of 176.5Mt, however, the TREOSc ppm grade has increased from 503 to 532 ppm. The January 2025 Inferred Mineral Resources tonnage has increased from 70.9Mt to 144.1Mt for the July 2025 MRE. The Inferred Mineral Resources TREOSc ppm grade has decreased from 561 to 484 ppm. The January 2025 Total Mineral Resources tonnage has increased from 274.5Mt to 320.6Mt for the July 2025 MRE. The Total Mineral Resources TREOSc ppm grade has changed from 520 to 510 ppm. • An economic cutoff grade of TREO + Sc ≥330ppm was applied to the MEC June 2025 MRE due to scandium oxide, being a potential credit element along with the presence of hafnium, nickel, cobalt, and copper. • The June 2025 MEC Indicated and Inferred Mineral Resource for the North Stanmore Project is estimated at ~321 Mt of REE-bearing saprolite and bedrock at 510 ppm TREO + Sc2O3, for 163,660 tonnes of contained TREO + Sc2O3. The MEC Mineral Resource is not limited to tenement E20/871.
	• *The assumptions made regarding recovery of by-products.*	• Test work has demonstrated that Scandium is recoverable and may become a byproduct. • Test work has demonstrated that Gallium is recoverable and may become a byproduct. • Available metallurgical test work has demonstrated that likely processing will be able to recover significant proportions of Scandium, Gallium, Nickel, Cobalt, Copper, and Hafnium.
	• *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).*	• Test work completed by Victory Metals included analysis of Uranium (U) and Thorium (Th) levels across the project. • The assessed levels of uranium and thorium were very low values across the project. Due to the low values within both ore and waste the uranium and thorium were not estimated, however, both values may be estimated in the future if required for integration into processing studies. **Waste** U Max = 24ppm, Mean = 1.7ppm Th Max = 67ppm, Mean = 7.9ppm **MIN Domain (≥150ppm TREO + Sc_2O_3)** U Max = 12ppm, Mean = 2.11ppm Th Max = 61ppm, Mean = 7.15ppm **HGMIN Domain (≥600ppm TREO + Sc_2O_3)** U Max = 11ppm, Mean = 1.8ppm Th Max = 68ppm, Mean = 6.9ppm

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		• Metallurgical recovery to date of deleterious Uranium (U) 2.4ppm and Thorium (Th) 5ppm are less than average abundances in the upper continental crust (U) 3ppm (Th) 10ppm. • Scandium oxide, Gallium oxide, Hafnium, Copper, Cobalt, and Nickel were estimated within this MRE and are considered significant. • Sulphur (S) has not been analysed by the laboratory and cannot currently be estimated.
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*	• Drillhole spacing is consistent and varies in the East and North-East of the deposit. Nominal drillhole spacing is 50 x 50m expanding to ~250 north by 100m east across strike. • The block size used for the estimation 50m east x 50m north and 1 mRL, with sub celled blocks to 25m east x 25m north and 0.5mRL.
	• *Any assumptions behind modelling of selective mining units.*	• No support correction was applied to allow for selective mining units at this stage of the project life.
	• *Any assumptions about correlation between variables*	• No assumptions were made regarding correlations between variables.
	• *Description of how the geological interpretation was used to control the resource estimates.*	• A geological cutoff grade of 150ppm was chosen to distinguish the mineralised material from poorly unmineralised material. • The mineralised domain MIN was then Interpreted at 150ppm TREO Sc_2O_3 reflecting the on-set of mineralisation. • The interpretation was carried out in section lines and a high-grade mineralised domain HGMIN was delineated at 600ppm TREO + Sc_2O_3.
	• *Discussion of basis for using or not using grade cutting or capping.*	• Few extreme values were present and no topcuts were applied.
	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*	• The OBM estimate was validated, validation approaches included: o Visual checks for composite grades versus estimated block grades. o Comparison of global mean grades of composites versus blocks for each Domain. This check ensures that the global statistics for each estimated variable represent the composited statistics in that domain. o Histograms of composites versus block distributions to check preservation of the distribution post-estimate. o Swath plots (also known as trend plots) to compare the spatial variation of grades between composites and blocks across the block model. o On completion of the OBM, checks were conducted for overlapping or missing blocks, and none were found.

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		• Primary relevant elements of interest were estimated individually (Dy_2O_3, Er_2O_3, Eu_2O_3, Gd_2O_3, Ho_2O_3, La_2O_3, Lu_2O_3, Nd_2O_3, Pr_6O_{11}, Sm_2O_3, Tb_4O_7, Tm_2O_3, Y_2O_3, Yb_2O_3, Sc_2O_3, Ga_2O_3).
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages were estimated on a dry basis.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The MRE was reported at a 330ppm TREO + Sc_2O_3 cutoff grade. • The RSC August 2023 MRE economic cut-off grade was ≥400 ppm TREO, inclusive of Yttrium. The economic cut-off grade for the June 2025 MEC MRE was ≥330ppm TREO + Sc_2O_3, inclusive of Yttrium oxide and Scandium oxide. Asra Minerals Limited (ASX: ASR) reported in an ASX Announcement, 16 April 2024, a maiden JORC (2012) Mineral Resource Estimate (MRE) for its 100%-owned Yttria Rare Earth Element (REE) deposit, located on its Mt Stirling Project near Leonora in the northern Goldfields region of Western Australia. The MRE was reported above an economic cut-off grade of 200 ppm TREO, inclusive of Yttrium, minus CeO_2. Asra Minerals Ltd commented that this cut-off grade was selected based on the evaluation of other clay hosted rare earth Mineral Resources.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the*	• The Competent Person deems that there are reasonable prospects for eventual economic extraction using open pit mining methods as a function of: o The relative shallow depth of the mineralisation and presence of loosely consolidated transported Colluvium above the mineralisation, allowing free dig mining. o Proximity to significant existing infrastructure (located adjacent to the Gt Northern Highway and the township of Cue). o The high value of contained REE and transition metals and the current divergence from Chinese REE pricing and the development of a western pricing system at higher levels. • Future pit optimisation studies will confirm the designation of the blocks for RPEEE.

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	mining assumptions made.	
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Extensive metallurgical studies by Core metallurgy regarding the beneficiation and extraction of Ce, Dy, Er, Eu, Ga, Gd, Ho, La, Lu, Mn, Nd, Pr, Sc, Sm, Tb, Th, Tm, U, Y, and Yb have been completed. • The leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trailed at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREO"). • Additionally, Scandium oxide (Sc2O3) recoveries of (50%) were achieved and Gallium oxide (Ga2O3) recoveries of (34%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO, Sc2O3 and Ga2O3 from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C). • LS Metallurgy Perth, Western Australia was appointed in September, 2025 to conduct simple wet classification to isolate the -10.8 µm fraction from a bulk sample composited from the North Stanmore resource area. Grades were assayed on head and fraction products. No chemical upgrading or complex mineral separation was applied. Results demonstrate intrinsic deportment of key critical elements into ultra fine particles, providing a low-capex, low-opex front end upgrade option that reduces throughput of less critical elements and gangue materials. Victory submitted a composite sample to ALS Global Perth in October of 2025 for kinetic leach testwork. The result of the testwork was a major reduction in leach time for the North Stanmore Project with ~90% of rare earths leached in just 15 minutes compared to the 4-hour assumption used in the Scoping Study. The 16 times shorter leach time is expected to lower both CAPEX and OPEX due to a requirement for a smaller leach circuit. These results will be incorporated into the PFS.

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		• In January of 2026 using straightforward gravity separation, the Company achieved a 27 fold increase in Hafnium metal grade (from 4 ppm to 108 ppm) and recovered 66% of the Hafnium into just 3.5% of the original ore mass. 96.5% of the material is rejected early, dramatically reducing the size, capital cost and operating expenses of any future Hafnium processing plant. • The concentration of Hf and Zr rich zircon and baddeleyite was achieved via a simple gravity separation process. A significant grade increase was achieved for hafnium and zircon. Hf assay data for Certified Standards analysed with the Victory Metals samples showed agreement between assay values and certified values over various grade ranges. 2026 Metallurgical testwork results include the following - **Sampling and Representivity: ·** First-pass sighter flotation testwork was conducted on a representative composite sample generated from 47 sample metres across 10 different drillholes. The drillholes are located within the currently defined Indicated Mineral Resource boundary at the North Stanmore project. The composite was formulated to be representative of the high-grade, shallow regolith-hosted mineralization, returning a calculated head grade of 1,251 ppm TREO. **Mineralogical Analysis:** Because the 1251 ppm TREO composite feed is below the practical resolution limits for detailed automated mineralogy, the TIMA was conducted on a separate, higher-grade metallurgical sample sourced from within the same ore-body. This sample is considered representative of the mineralogical deportment across the deposit. · TIMA confirmed that >99% of Yttrium (acting as a proxy for Heavy Rare Earth Elements) is hosted in discrete, well-liberated secondary phosphate minerals, specifically rhabdophane and churchite. · Mineralogical characterisation confirms these secondary phosphates are non-refractory and physically softer than primary phosphates (monazite/xenotime), supporting the appropriateness of simple physical beneficiation. **Testwork Undertaken and Results:** Bench-scale froth flotation testwork was conducted to evaluate the amenability of the ore to physical upgrading. · A standard whole-of-ore rougher flotation test (without front-end desliming) achieved an 81.5% TREO recovery at a mass yield of 41.7%, upgrading the 1,251 ppm TREO feed to a 2,443 ppm TREO rougher concentrate. · A subsequent cleaner flotation stage was conducted on a high-grade, fast-floating rougher concentrate fraction (captured in the first 7 minutes of a separate bulk rougher run without front-end desliming). · The cleaner stage achieved an 83.6% stage recovery at an 11.0% mass yield, producing a combined concentrate grade of 5.5% TREO (54,745 ppm), with a peak discrete fraction grading 5.9% TREO (59,467 ppm). · The resulting

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		concentrate maintained a premium heavy rare earth ratio of ~38% HREO/TREO, highly enriched in Dysprosium (Dy), Terbium (Tb), and Yttrium (Y). **Processing Assumptions and Flowsheet: ·** The testwork demonstrates that the North Stanmore ore is highly responsive to standard, conventional froth flotation using commercially available, low-cost collectors. · The ability to reject >95% of the gangue mass upfront without complex baking or cracking provides a basis for assuming a significantly reduced hydrometallurgical plant sizing (estimated ~5tph) and lower associated CAPEX/OPEX for future economic studies. · Deleterious elements such as Uranium (U) and Thorium (Th) are inherently low in these secondary phosphate profiles. While physical beneficiation naturally concentrates these elements alongside the rare earths, the resulting flotation concentrate exhibits very low-level radioactivity (~2Bq/g), substantially reducing complex radioactive waste management requirements compared to primary hard-rock deposits. · Ongoing locked-cycle testing and bulk flotation will be undertaken to optimise the flowsheet and confirm global recoveries for the upcoming Pre-Feasibility Study.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The North Stanmore prospect is located in the Murchison of Western Australia, a mining district with considerable mining history and well understood environmental standards and protocols. • An environmental study is currently underway as part of the Prefeasibility study. It is assumed that waste will be stockpiled nearby the mined pits and may also be backfilled where practicable. Tailings will be pumped as a slurry from the process plant and may be returned to cells within mined pits.

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Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*	• Downhole geophysical density is available for 10 diamond drillholes at 10cm depth increments, for a total of 5,896 readings. • Core length, diameter and weight are available for 8 of the diamond drillholes for 50 readings • Regression analysis was performed to compare the two different approaches to measuring density. • A single density value was applied to each geology domain regardless of mineralisation profile. Densities were used to estimate the MRE tonnage. • Density measurements are considered to be dry.
	• *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.*	• Downhole density measurements were obtained from 10 diamond drillholes at 10cm depth increments, for 5,896 readings. No anomalous density readings were observed in the data. Downhole geophysical density measurements were taken in rod, then corrected to account for this, using a factor calculated from a calibration drillhole (DD004).
	• *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• Core length, diameter and weight are available for 8 of the diamond drillholes for a total of 50 readings. From this information, density was calculated using the formula: • Where "r" is the radius of the PQ core (0.0425m), "h" is the length of the core in metres, and "m" is the mass in kilograms. The density was converted from kg/m3 to g/cm3 for consistency with units used for downhole geophysical density. Four anomalous calculated density values were identified where density <1 g/cm3. Regression analysis was applied to calculate the density from geophysical measurements for the high grade and low-grade domains. The mean density from regression analysis for the High-grade domain is 1.75t/m3, and for the low-grade domain 2.02t/m3. • The following densities have been applied to the MRE. ***Geology domain*** — **Dry bulk density** (t/m³) *Colluvium* — 1.7 *Saprolite (LG & HG)* — 1.71 *Sap Rock (LG & HG)* — 2.18 *Slightly Weathered (LG & HG)* — 2.2 *Basement (LG & HG)* — 2.3

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Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.*	• Mineral Resources were classified as Indicated and Inferred. Material not classified as either indicated or inferred Material remains unclassified and has been reported as an Exploration Target. Indicated Mineral Resource classification was based on drillhole spacing (250 x 100m closing to 50 x 50m in some areas), acceptable underlying QAQC, and RTK/DGPS survey of drillhole collar. The DGPS survey provided increased certainty regarding the drillhole collar location and compensated for a low-resolution topography survey. The topographical surface was adjusted to include the DGPS surveyed drillhole collar coordinates. • 55% (by tonnage) of the MRE is classified as Indicated Mineral Resources, 45% (by tonnage) is classified as Inferred Mineral Resources.
	• *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*	• Grade and tonnage estimation has been considered for the MRE classification. • The Competent Person has considered all relevant factors
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• The MRE classification of Inferred and Indicated MRE reflects the Competent Persons understanding of the deposit.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• MEC conducted an internal review of the RSC August 2023 MRE. • MEC conducted an audit in May 2025 of the geological logging by reviewing the chip trays. Several drillholes were selected and the chips checked. The audit found that there was strong agreement between the logging and the chip trays. The quality of logging from a limited test program was found to be acceptable to the Competent Person.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or*	• No statistical test of the accuracy and confidence in the MRE has been undertaken. The low variability of the mineralisation grades, the relatively consistent mineralisation geometry, the geometry and large areal extent of the mineralisation provide qualitative confidence in the MRE.

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	geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.	
	• *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.*	• The estimate is considered a good global estimate, and the relative confidence in the underlying data (QAQC), drillhole spacing, geological continuity and interpretation, has been appropriately reflected by the Competent Person/s in the Resource Classification.
	• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• There has been no production at the North Stanmore project.

Table 2: December 2025 Drillhole collar coordinates

HoleID	East	North	RL_TOPO	Depth	Tenement	AZIMUTH °	DIP °	DRILL DATE
2025IFAC001	585,858.0	6,973,482.0	429.445	39.000	E20/0871	0	-90	1/12/2025
2025IFAC002	585,942.0	6,973,475.0	429.500	46.000	E20/0871	0	-90	1/12/2025
2025IFAC003	586,060.0	6,973,490.0	429.966	45.000	E20/0871	0	-90	1/12/2025
2025IFAC004	586,160.0	6,973,479.0	430.000	48.000	E20/0871	0	-90	1/12/2025
2025IFAC005	586,267.0	6,973,483.0	430.500	65.000	E20/0871	0	-90	1/12/2025
2025IFAC006	588,955.0	6,972,450.0	437.000	36.000	P20/2469	0	-90	4/12/2025

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2025IFAC007	589,055.0	6,972,457.0	437.020	48.000	P20/2469	0	-90	4/12/2025
2025IFAC008	589,155.0	6,972,450.0	437.137	54.000	P20/2469	0	-90	4/12/2025
2025IFAC009	589,256.0	6,972,455.0	437.251	60.000	P20/2469	0	-90	4/12/2025
2025IFAC010	589,355.0	6,972,450.0	437.255	76.000	P20/2469	0	-90	3/12/2025
2025IFAC011	586,061.0	6,972,453.0	434.473	60.000	M20/543	0	-90	30/11/2025
2025IFAC012	586,157.0	6,972,458.0	434.577	60.000	M20/543	0	-90	30/11/2025
2025IFAC013	586,253.0	6,972,458.0	434.814	60.000	M20/543	0	-90	30/11/2025
2025IFAC014	586,343.0	6,972,463.0	434.651	43.000	M20/543	0	-90	30/11/2025
2025IFAC015	586,453.0	6,972,468.0	434.586	30.000	M20/543	0	-90	30/11/2025
2025IFAC016	586,167.0	6,972,228.0	435.937	60.000	M20/543	0	-90	30/11/2025
2025IFAC017	586,363.0	6,972,234.0	435.500	34.000	M20/543	0	-90	30/11/2025
2025IFAC018	586,559.0	6,972,248.0	435.270	57.000	M20/543	0	-90	30/11/2025
2025IFAC019	586,053.0	6,971,942.0	437.500	69.000	M20/543	0	-90	28/11/2025
2025IFAC020	586,210.0	6,971,947.0	438.000	53.000	M20/543	0	-90	28/11/2025
2025IFAC021	586,354.0	6,971,942.0	437.299	60.000	M20/543	0	-90	28/11/2025
2025IFAC022	586,540.0	6,971,942.0	437.000	60.000	M20/543	0	-90	28/11/2025
2025IFAC023	588,903.0	6,972,183.0	438.000	50.000	P20/2007	0	-90	4/12/2025
2025IFAC024	588,829.0	6,971,738.0	439.500	42.000	P20/2007	0	-90	5/12/2025
2025IFAC025	588,950.0	6,971,720.0	439.500	35.000	P20/2007	0	-90	5/12/2025
2025IFAC026	589,067.0	6,971,732.0	439.500	45.000	P20/2007	0	-90	5/12/2025
2025IFAC027	589,220.0	6,971,713.0	439.579	66.000	P20/2468	0	-90	4/12/2025
2025IFAC028	589,339.0	6,971,718.0	439.500	69.000	P20/2468	0	-90	4/12/2025
2025IFAC029	589,206.0	6,971,558.0	440.167	84.000	P20/2468	0	-90	4/12/2025
2025IFAC030	589,299.0	6,971,555.0	440.010	60.000	P20/2468	0	-90	4/12/2025
2025IFAC031	589,223.0	6,971,378.0	440.612	32.000	P20/2468	0	-90	5/12/2025
2025IFAC032	588,387.0	6,971,188.0	441.824	42.000	P 20/215	0	-90	6/12/2025
2025IFAC033	588,500.0	6,971,185.0	442.000	48.000	P 20/215	0	-90	6/12/2025
2025IFAC034	588,608.0	6,971,185.0	442.000	57.000	P 20/215	0	-90	6/12/2025
2025IFAC035	588,700.0	6,971,185.0	441.952	48.000	P20/2007	0	-90	6/12/2025
2025IFAC036	588,809.0	6,971,188.0	441.686	50.000	P20/2007	0	-90	6/12/2025
2025IFAC037	588,900.0	6,971,185.0	441.500	60.000	P20/2007	0	-90	5/12/2025
2025IFAC038	589,016.0	6,971,192.0	441.613	39.000	P20/2007	0	-90	5/12/2025
2025IFAC039	589,100.0	6,971,185.0	441.500	50.000	P20/2007	0	-90	5/12/2025
2025IFAC040	589,191.0	6,971,187.0	441.500	42.000	P20/2007	0	-90	5/12/2025
2025IFAC041	589,337.0	6,971,185.0	441.057	40.000	P20/2469	0	-90	5/12/2025
2025IFAC042	589,332.0	6,970,998.0	441.897	30.000	P20/2469	0	-90	5/12/2025
2025IFAC043	588,476.0	6,970,095.0	446.291	30.000	M20/0494	0	-90	6/12/2025
2025IFAC044	588,559.0	6,970,100.0	446.000	24.000	M20/0494	0	-90	6/12/2025
2025IFAC045	588,469.0	6,969,897.0	446.734	20.000	M20/0494	0	-90	6/12/2025

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2025IFAC046	588,584.0	6,969,894.0	446.735	30.000	M20/0494	0	-90	6/12/2025
2025IFAC047	586,336.0	6,973,703.0	429.500	58.000	E20/0871	0	-90	1/12/2025
2025IFAC048	586,395.0	6,973,703.0	429.555	57.000	E20/0871	0	-90	2/12/2025
2025IFAC049	586,522.0	6,973,719.0	429.687	66.000	E20/0871	0	-90	1/12/2025
2025IFAC050	586,591.0	6,973,719.0	429.991	44.000	E20/0871	0	-90	1/12/2025
2025IFAC051	586,463.0	6,973,761.0	429.471	57.000	E20/0871	0	-90	2/12/2025
2025IFAC052	586,559.0	6,973,835.0	429.500	48.000	E20/0871	0	-90	2/12/2025
2025IFAC053	586,581.0	6,973,902.0	429.500	57.000	E20/0871	0	-90	3/12/2025
2025IFAC054	586,656.0	6,973,907.0	429.399	54.000	E20/0871	0	-90	3/12/2025
2025IFAC055	586,667.0	6,973,863.0	429.500	36.000	E20/0871	0	-90	2/12/2025
2025IFAC056	586,593.0	6,973,802.0	429.562	60.000	E20/0871	0	-90	2/12/2025
2025IFAC057	586,497.0	6,973,807.0	429.433	57.000	E20/0871	0	-90	2/12/2025
2025IFAC058	586,540.0	6,973,783.0	429.563	65.000	E20/0871	0	-90	2/12/2025
2025IFAC059	586,666.0	6,973,828.0	429.508	29.000	E20/0871	0	-90	2/12/2025
2025IFAC060	586,731.0	6,973,862.0	429.500	38.000	E20/0871	0	-90	3/12/2025
2025IFAC061	589,946.0	6,975,792.0	427.000	52.000	E20/0871	0	-90	3/12/2025
2025IFAC062	589,997.0	6,975,795.0	426.951	52.000	E20/0871	0	-90	3/12/2025
2025IFAC063	590,049.0	6,975,799.0	426.970	48.000	E20/0871	0	-90	3/12/2025

Drillhole coordinates are planned locations, a final survey pickup had not been completed at the time of Announcement.

Significant intersections are shown in Table 3.

Table 3: Significant intersections

HoleID	From	To	INTERVAL m	TREYSc O_ppm	TREO _ppm	HREO _ppm	LREO _ppm	HRE0 TREO	Sc2O3 _ppm	Th _ppm	U _ppm
2025IFAC001	18	21	3.0	1,185	1,129	350	779	31%	56	3.08	5.11
2025IFAC002	7	19	12.0	481	464	173	292	39%	17	6.89	1.78
2025IFAC002	22	25	3.0	380	366	171	195	47%	14	6.08	2.37
2025IFAC002	27	29	2.0	479	466	190	276	41%	14	6.68	2.46
2025IFAC002	38	40	2.0	454	439	173	266	40%	14	6.08	2.55
2025IFAC003	19	28	9.0	560	545	209	336	41%	15	6.66	2.49
2025IFAC003	41	43	2.0	364	351	153	198	44%	13	6.33	1.75
2025IFAC004	15	37	22.0	460	445	184	261	42%	15	7.19	2.01
2025IFAC004	39	47	8.0	394	377	185	192	49%	17	6.60	1.83
2025IFAC005	8	11	3.0	802	781	152	628	34%	21	15.09	1.80
2025IFAC005	12	21	9.0	566	545	217	328	43%	21	9.65	2.22
2025IFAC005	22	47	25.0	492	473	193	280	43%	18	6.51	1.85
2025IFAC005	49	51	2.0	381	359	185	174	52%	22	6.43	1.79
2025IFAC005	52	54	2.0	408	388	195	193	50%	20	7.07	1.71

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2025IFAC005	57	60	3.0	357	337	174	163	52%	19	6.20	1.78
2025IFAC006	16	21	5.0	1,037	1,018	338	680	36%	19	4.83	2.02
2025IFAC011	19	27	8.0	703	689	126	563	20%	14	11.49	2.93
2025IFAC011	51	55	4.0	501	483	196	287	42%	18	8.22	2.62
2025IFAC012	33	39	6.0	391	374	92	282	25%	17	13.53	3.42
2025IFAC013	22	24	2.0	2,809	2,781	231	2,550	10%	27	13.25	4.49
2025IFAC013	30	34	4.0	685	672	219	453	31%	13	12.49	3.40
2025IFAC015	15	20	5.0	1,278	1,224	190	1,034	20%	54	8.58	6.99
2025IFAC016	16	23	7.0	537	522	136	386	27%	15	14.80	3.78
2025IFAC017	15	20	5.0	3,312	3,286	761	2,524	23%	27	12.91	9.05
2025IFAC018	18	26	8.0	562	536	205	331	37%	26	10.42	4.06
2025IFAC019	0	2	2.0	528	496	123	373	25%	33	11.03	3.48
2025IFAC019	3	6	3.0	831	807	103	704	14%	24	11.22	3.07
2025IFAC020	16	27	11.0	796	766	258	509	37%	30	7.07	4.30
2025IFAC021	36	41	5.0	962	947	263	684	28%	15	10.77	3.15
2025IFAC022	15	24	9.0	476	453	116	337	26%	23	14.44	4.72
2025IFAC023	9	12	3.0	375	353	145	208	41%	22	5.07	0.92
2025IFAC024	26	29	3.0	713	682	216	466	36%	31	7.82	2.75
2025IFAC027	54	59	5.0	714	693	298	395	40%	21	10.50	1.67
2025IFAC027	60	62	2.0	379	358	196	163	55%	21	6.89	1.86
2025IFAC029	40	42	2.0	1,055	1,034	260	774	28%	21	8.07	2.53
2025IFAC029	47	50	3.0	929	908	283	626	31%	21	26.42	1.60
2025IFAC033	17	19	2.0	1,718	1,689	175	1,515	11%	29	23.35	4.22
2025IFAC033	30	33	3.0	565	541	274	267	51%	23	6.23	2.10
2025IFAC034	54	56	2.0	721	694	100	595	15%	27	49.65	9.80
2025IFAC035	24	32	8.0	557	538	137	401	27%	19	8.88	3.32
2025IFAC036	30	36	6.0	825	808	256	552	33%	17	9.99	3.37
2025IFAC037	34	36	2.0	535	504	90	414	18%	32	21.00	2.41
2025IFAC038	22	25	3.0	592	577	114	463	20%	15	10.73	6.22
2025IFAC039	25	31	6.0	579	555	151	404	31%	25	8.20	1.95
2025IFAC040	24	27	3.0	909	885	217	667	27%	24	6.94	2.64
2025IFAC041	22	26	4.0	444	419	139	281	33%	25	7.12	1.42
2025IFAC046	8	12	4.0	510	489	111	378	25%	21	4.97	1.24
2025IFAC047	18	31	13.0	821	794	229	565	33%	27	5.42	2.78
2025IFAC047	35	42	7.0	401	383	174	209	46%	19	6.46	1.80
2025IFAC047	43	46	3.0	364	348	174	175	50%	16	6.28	1.61
2025IFAC047	48	50	2.0	353	337	170	167	50%	16	6.21	1.58
2025IFAC048	23	45	22.0	609	596	220	376	39%	13	10.57	2.42
2025IFAC049	14	19	5.0	889	875	346	529	42%	14	19.24	3.81
2025IFAC049	21	23	2.0	703	693	288	405	44%	10	16.53	3.59
2025IFAC049	44	47	3.0	371	361	193	168	53%	10	13.12	2.43

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2025IFAC050	13	35	22.0	781	767	264	503	39%	14	11.68	2.53
2025IFAC050	38	40	2.0	395	383	197	187	52%	12	11.16	2.10
2025IFAC051	18	26	8.0	787	752	176	576	28%	35	9.35	3.85
2025IFAC051	28	30	2.0	530	511	263	249	51%	18	12.19	2.57
2025IFAC051	35	39	4.0	537	521	207	314	40%	17	10.09	2.49
2025IFAC051	40	43	3.0	520	509	222	287	44%	11	10.04	2.47
2025IFAC051	49	51	2.0	441	430	174	255	41%	11	9.39	1.63
2025IFAC052	29	32	3.0	550	535	214	322	40%	14	18.25	3.65
2025IFAC052	33	34	1.0	671	654	184	470	28%	17	12.85	3.51
2025IFAC052	35	37	2.0	411	391	126	265	33%	20	12.55	3.02
2025IFAC054	15	17	2.0	362	342	109	233	33%	19	9.30	2.54
2025IFAC054	18	21	3.0	428	412	159	253	39%	16	12.65	2.31
2025IFAC054	23	29	6.0	705	694	263	431	43%	10	14.75	2.25
2025IFAC056	11	13	2.0	629	611	203	409	35%	18	14.73	2.99
2025IFAC056	14	29	15.0	636	614	230	383	38%	22	13.04	2.77
2025IFAC057	25	32	7.0	374	352	162	189	45%	22	11.57	3.30
2025IFAC057	54	57	3.0	379	369	171	198	46%	10	9.72	2.01
2025IFAC058	11	13	2.0	498	483	243	240	50%	15	23.45	2.04
2025IFAC058	16	20	4.0	408	398	178	221	46%	10	12.90	1.96
2025IFAC058	29	33	4.0	444	434	221	212	52%	10	16.60	2.79
2025IFAC058	39	42	3.0	464	454	224	231	49%	10	15.80	3.67
2025IFAC058	52	54	2.0	472	461	218	242	48%	11	14.08	3.18
2025IFAC058	55	57	2.0	360	351	199	152	57%	9	13.45	2.66
2025IFAC058	59	63	4.0	497	487	188	298	39%	11	12.06	2.96

Significant intersections have been reported ≥330ppm TREOSc, with a minimum interval thickness of 2m.