5th March 2026

Exceptional Metallurgical Recoveries Achieved

Silver recoveries reached 78% (77% average) and gold 77% (74% average), under early-stage heap leach test conditions.

Highlights:

- **Intermittent Bottle Roll (IBR) cyanide leach tests on coarse-crush material achieved:**
  - **Silver Recoveries up to 78.3%, averaging 77%;**
  - **Gold Recoveries up to 77.3%, averaging 74%**
- **IBR tests provide an estimate of Heap Leach recoveries**
- **Metallurgical testwork indicates ore is non-refractory and non-preg robbing in nature**
- **Cyanide leach tests (which provide an estimate of a fine grind tank leach) achieved:**
  - **Silver Recoveries up to 90%, averaging 87.25%**
  - **Gold Recoveries up to 84.70%, averaging 82.15%**
- **Independent Metallurgical Operations (IMO) previous review of historical test work highlighted that extended leach durations provide conditions for higher silver recoveries, consistent with silver's slower leaching kinetics. This has been confirmed via the recent IBR tests**
- **Reducing chlorides in process water via reverse osmosis presents a potential opportunity to further enhance recoveries at Maverick Springs**

Sun Silver Limited (**ASX: SS1; OTCQX: SSLVF**) ("**Sun Silver**" or "**the Company**") is pleased to announce exceptional metallurgical test work results from Intermittent Bottle Roll ("IBR") tests which provide an estimate of heap leach recoveries. The results demonstrate high silver and gold recoveries across three crush sizes, reinforcing the potential for a low capital heap leach development pathway, for the Maverick Springs Silver-Gold Project in Nevada, USA ("**Maverick Springs"** or "**the Project**").

Sun Silver Managing Director, Andrew Dornan, said*:*

"Achieving silver recoveries approaching 78% and gold recoveries exceeding 77% under early-stage heap leach test conditions marks a significant milestone for Maverick Springs. These results provide a de-risked, low-capital, scalable heap leach pathway and represents a real catalyst for advancing the project."

Sun Silver Limited

1/1 Tully Road, East Perth
Western Australia 6004

info@sunsilver.com.au
www.sunsilver.com.au

Metallurgical Testwork

Metallurgical testwork was undertaken, managed, and reviewed by Independent Metallurgical Operations ("**IMO**"), a subsidiary of SGS.

A total of 242 intervals of half diamond drill core were derived from existing diamond core samples, comprising oxide and transitional mineralisation.

Two composite samples were prepared:

- Composite sample 1: 147kg total weight
- Composite sample 2: 127kg total weight

Sample intervals and drill hole information is detailed within Appendix A and B below.

IBR tests were conducted on both sample composites at three crush sizes; P_{100} 6.3mm, 3.35mm and 2.0mm, with each sample weight being 5kg.

Cyanide leach tests were conducted on both sample composites at three grind sizes (P_{80}), 106 µm, 75µm and 53µm, with each sample weight being 1kg.

IBR tests, never previously completed on Maverick Springs mineralisation, provide an initial estimate of heap leach recoveries.

Table 1 – IBR Metallurgical Test Results

Sample ID	Unit	Composite Sample 1 (CS1)			Composite Sample 2 (CS2)			Average recoveries by crush size		
Test Number		IBR-01	IBR-03	IBR-05	IBR-02	IBR-04	IBR-06	IBR-01 & 02	IBR-03 & 04	IBR-05 & 06
Crush Size (P_{100})	mm	6.3	3.35	2.0	6.3	3.35	2.0	6.3	3.35	2.0
Ag Extraction Solids Assay (Recoveries - 58 Days)	%	66.2%	74.7%	78.3%	56.3%	62.4%	75.6%	61.3%	68.6%	76.95%

As a Nevada benchmark, Coeur Mining Inc's (NYSE:CDE) Rochester Silver Mine in Nevada reports the following heap leach recoveries in its technical report[1]:

- Stage I Pad: ~56% silver recovery
- Stage II Pad: ~61% silver recovery
- Stage III Pad: ~48% silver recovery
- Stage IV Pad: ~60% silver recovery
- Overall cumulative silver recovery ~58% across all pads to date

[1] Coeur Mining Rochester Operations, Nevada – Technical Report Summary **https://s201.q4cdn.com/254090064/files/doc_downloads/operations/Rochester.pdf**

Table 2 – IBR Tests Silver and Gold Recoveries for Each Composite Sample

Sample ID	**Unit**	**Sample 1**			**Sample 2**		
Test Number		**IBR-01**	**IBR-03**	**IBR-05**	**IBR-02**	**IBR-04**	**IBR-06**
Crush Size (P100)	**mm**	**6.3**	**3.35**	**2.0**	**6.3**	**3.35**	**2.0**
Ag Residue Grade	g/t	78.7	59	50.6	101.8	94	61
Au Residue Grade	g/t	0.13	0.12	0.1	0.21	0.19	0.18
Ag Equiv. Residue Grade	g/t	85.9	65.3	56.1	113.5	104.7	70.8
Ag Head	ppm	276	276	276	226	226	226
Au Head	ppm	0.32	0.32	0.32	0.76	0.76	0.76
Feed SxA and Solid Assay Extractions							
Ag Extraction Solids Assay	%	66.20%	74.70%	78.30%	56.30%	62.40%	75.60%
Au Extraction Solids Assay	%	61.70%	66.40%	70.90%	73.00%	75.30%	77.30%
Ag Residue Grade	**g/t**	**78.7**	**59.0**	**50.6**	**101.8**	**94.0**	**61.0**
Au Residue Grade	**g/t**	**0.13**	**0.12**	**0.10**	**0.21**	**0.19**	**0.18**

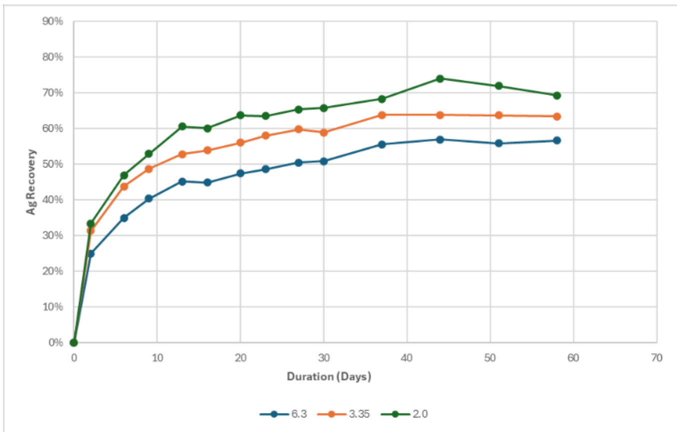

Figure 1 – Composite Sample 1 IBR Ag Recoveries

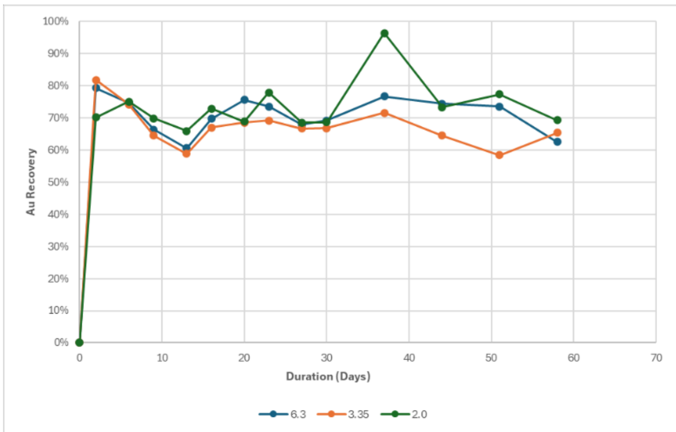

Figure 2 – Sample 1 IBR Ag Recoveries

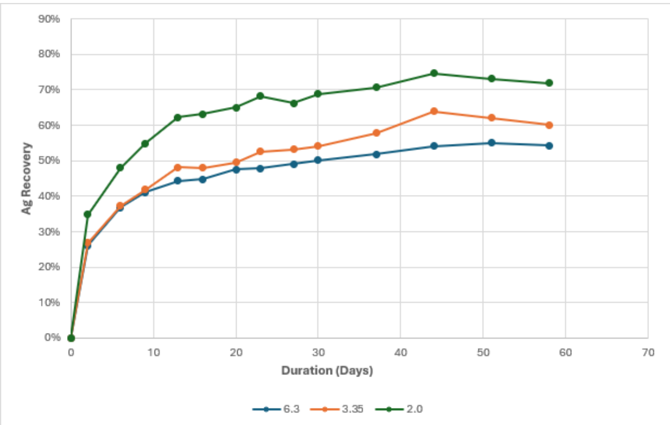

Figure 3 – Composite Sample 2 IBR Ag Recoveries

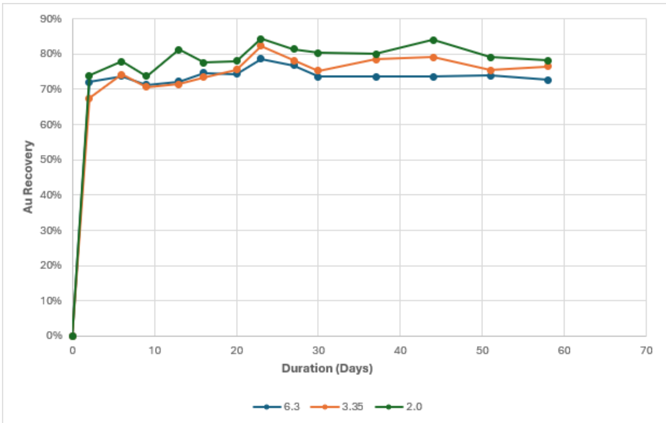

Figure 4 – Composite Sample 2 IBR Au Recoveries

Metallurgical Testwork confirms Non-Refractory and Non-Preg Robbing

High recoveries achieved under standard cyanide leach conditions, indicating no refractory mineralisation within the samples tested.

Preg-robbing testwork shows no evidence of gold or silver loss due to preg-robbing.

Side by side carbon in leach bottle roll tests confirm the material is not preg-robbing, supporting conventional processing flowsheet suitability.

What is Heap Leaching?

Heap leaching is a widely used, low-cost processing method suited to bulk-tonnage silver and gold deposits. The process involves:

1. Crushing ore to a defined size;
2. Stacking the ore on a lined leach pad;
3. Irrigating the heap with a leach solution (typically cyanide for silver and gold);
4. Recovering dissolved metals from solution via dewatering, precipitation and smelting processes.

Benefits of Heap Leach Processing

- **Lower capital intensity** compared to conventional milling and tank leaching;
- **Lower operating costs** due to reduced power consumption and simplified processing infrastructure;
- **Scalable development pathway,** enabling staged expansion;
- **Reduced processing complexity** relative to traditional milling operations**.**

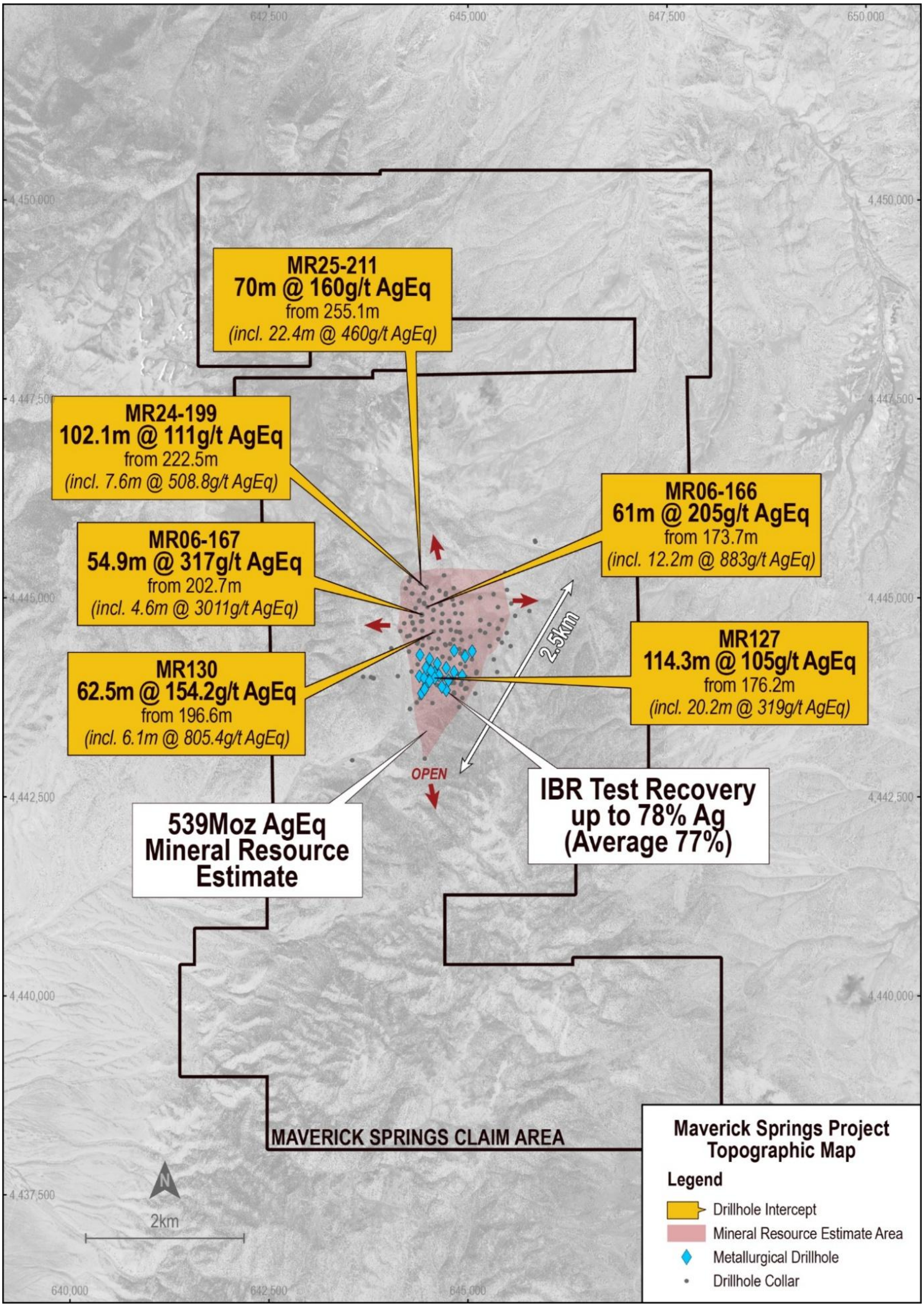

Figure 5 – Maverick Springs Project detailing metallurgical samples drill hole locations[2]

[2] For previously released drill intercepts refer to the Company's ASX announcements dated 14 January 2025 (MR24-199), 26 March 2025 (MR06-166, MR06-167, MR127 and MR130) and 2 July 2025 (MR25-211). For previously released estimates of mineral resources refer to Annexure A and the Company's ASX announcement dated 9 December 2025.

Figure 6 – Composite Sample 1 – Pre Metallurgical Testing

Figure 7 – Composite Sample 2 – Pre Metallurgical Testing

Figure 8 – IBR Metallurgical Testing two sample composites three grind sizes (6.3mm, 3.35mm, 2mm)

Cyanide Leach Tests

Strong Silver Leach Performance: Both Composite Samples 1 and 2 demonstrate robust silver recoveries under cyanide tank leach conditions, with solid residue extractions ranging from **83–90%**, confirming the high-recovery potential of Maverick Springs mineralisation.

Rapid Early-Stage Kinetics: Ag extraction after 2–4 days averaged **~66%**, supporting operationally realistic cyanide leach residence times for heap or tank leach design.

Coarser Grinds Offer Economic Advantage: While finer grind sizes marginally increase silver recovery, coarser grind sizes (P_{80} 75–106 µm) provide favourable kinetics with lower capital and operating costs, representing an economically preferred option.

No Preg-Robbing Observed: Both CN and CIL leach tests indicate consistent recovery patterns, with no evidence of preg-robbing in samples tested, demonstrating predictable metallurgical behaviour.

Table 3 – Tank Leach Tests Silver and Gold Recoveries for each composite sample

Sample ID	Units	Sample 1				Sample 2				Average recoveries by crush size			
Test Number		LT01	LT03	LT05	LT07	LT02	LT04	LT06	LT08	LT01 & LT02	LT03 & LT04	LT05 & LT06	LT07 & LT08
Grind Size (P_{80})	µm	106	75	53	106	106	75	53	106	106	75	53	106
% NaCN (Init)	ppm	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000
% NaCN (Mtn)	ppm	500	500	500	500	500	500	500	500	500	500	500	500
pH		10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11	10.5-11
% Solids	%	40	40	40	40	40	40	40	40	40	40	40	40
O_2/Air Sparge		Air	Air	Air	Air	Air	Air	Air	Air	Air	Air	Air	Air
Carbon Conc.	g/L	NA	NA	NA	26.73	NA	NA	NA	26.73	NA	NA	NA	26.73
Feed SxA and Solid Assay Extractions													
Ag Extraction Solids Assay		83.30%	84.40%	85.70%	86.40%	87.70%	90.10%	89.40%	88.40%	85.50%	87.25%	87.55%	87.40%
Au Extraction Solids Assay		76.70%	79.60%	79.60%	79.60%	83.40%	84.70%	84.70%	84.70%	80.05%	82.15%	82.15%	82.15%
Ag Equiv. Extraction Solids Assay		82.80%	84.00%	85.30%	85.90%	87.00%	89.30%	88.70%	87.80%	84.90%	86.65%	87.00%	86.85%
Lime Consumption	kg/t	0.94	1.02	1.06	0.86	1.23	1.36	1.32	1.64	1.09	1.19	1.19	1.25
Cyanide Consumption	kg/t	0.91	0.63	0.74	3.47	1.05	0.82	1.08	5.17	0.98	0.73	0.91	4.32

Opportunity for Water Purification Targeting Removal of Chloride

Treatment of process water to reduce chloride levels has the potential to further improve recoveries. Nevada water is not chloride-free, and simple purification of processing water could provide additional benefits to metal recoveries. A reverse osmosis (RO) plant is highly effective, capable of removing up to 99% of chlorides. RO works by forcing water through a semipermeable membrane that blocks dissolved salts, including chlorides. While RO is established in industrial water treatment in the US, it does not appear to be regularly applied in heap leach operations, representing a potential opportunity to enhance recoveries at Maverick Springs.

Next Steps

- Column leach tests simulating heap leach at scale are planned for Composite Samples 1 and 2.
- 2025 drill samples program review is complete, with composite domains defined and finalised to support master composites and variability testing for PFS level testing.
- Internal studies, mine and processing underway targeting conversion into a reportable Scoping Study / Preliminary Economic assessment later in 2026.

Maverick Springs Project

Sun Silver's cornerstone asset, the Maverick Springs Project, is located 85km from the fully serviced mining town of Elko in Nevada and is surrounded by several world-class gold and silver mining operations including Barrick's Carlin Mine.

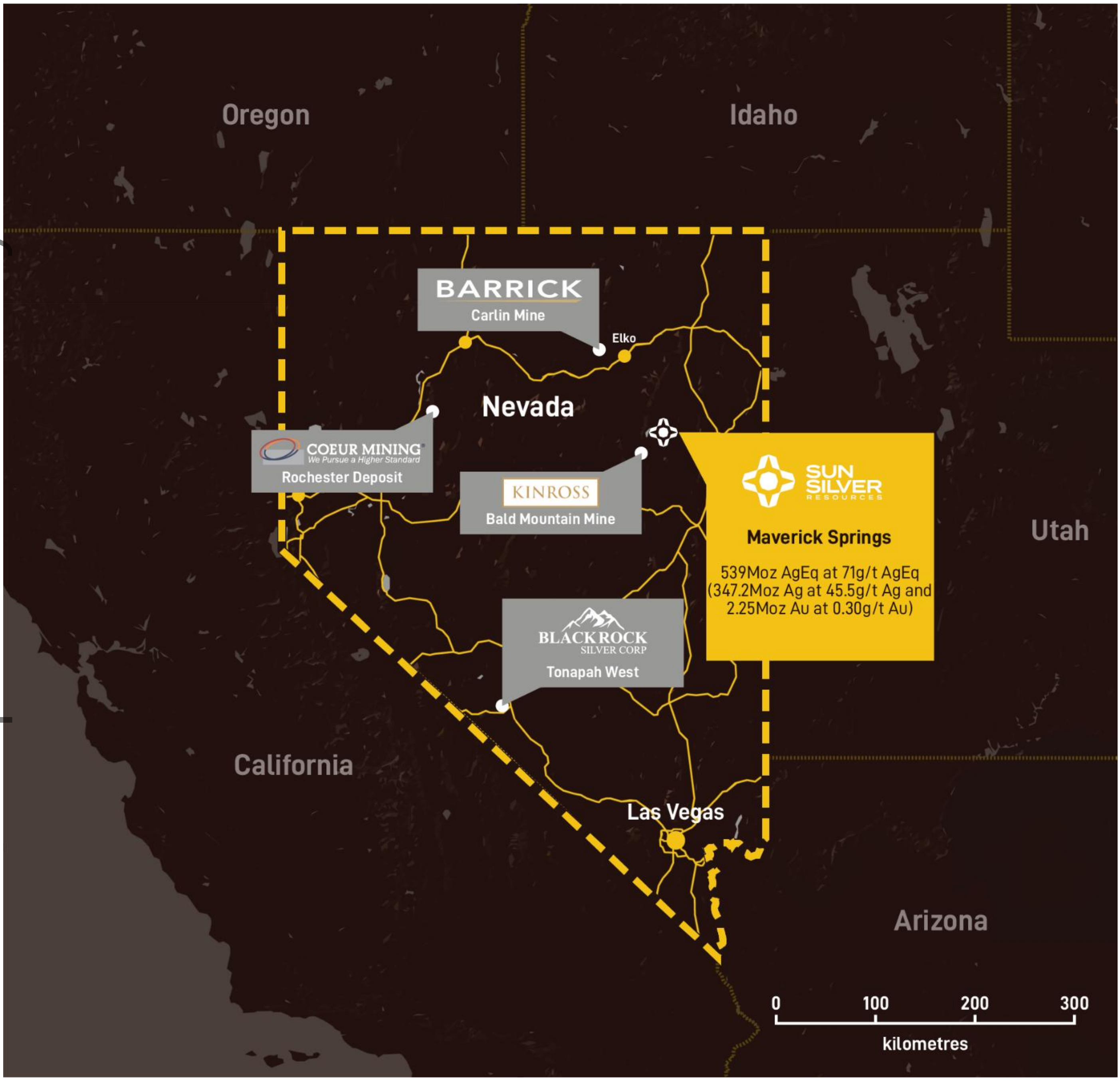

Figure 9 – Sun Silver's Maverick Springs Project location and surrounding operators.

Nevada is a globally recognised mining jurisdiction which was rated as the Number 1 mining jurisdiction in the world by the Fraser Institute in 2022.

The Project, which is proximal to the prolific Carlin Trend, hosts a JORC Inferred Mineral Resource of 237Mt grading 45.5g/t Ag and 0.30g/t Au for 347.2Moz of contained silver and 2.25Moz of contained gold (539Moz of contained silver equivalent)[3].

The deposit itself remains open along strike and at depth, with multiple mineralised intercepts located outside of the current Resource constrained model.

This announcement is authorised for release by the Board of Sun Silver Limited.

ENDS

For more information:

Investors:
Andrew Dornan
Managing Director
Sun Silver
info@sunsilver.com.au

Media:
Nicholas Read
Read Corporate
P: +61 419 929 046
E: nicholas@readcorporate.com.au

Forward-looking statements

*This announcement may contain certain forward-looking statements, guidance, forecasts, estimates or projections in relation to future matters (**Forward Statements**) that involve risks and uncertainties, and which are provided as a general guide only. Forward Statements can generally be identified by the use of forward-looking words such as "anticipate", "estimate", "will", "should", "could", "may", "expects", "plans", "forecast", "target" or similar expressions and include, but are not limited to, indications of, or guidance or outlook on, future earnings or financial position or performance of the Company. The Company can give no assurance that these expectations will prove to be correct. You are cautioned not to place undue reliance on any forward-looking statements. None of the Company, its directors, employees, agents or advisers represent or warrant that such Forward Statements will be achieved or prove to be correct or gives any warranty, express or implied, as to the accuracy, completeness, likelihood of achievement or reasonableness of any Forward Statement contained in this announcement. Actual results may differ materially from those anticipated in these forward-looking statements due to many important factors, risks and uncertainties. The Company does not undertake any obligation to release publicly any revisions to any "forward- looking statement" to reflect events or circumstances after the date of this announcement, except as may be required under applicable laws.*

Competent Person Statement

The information in this announcement that relates to Exploration Results or Estimates of Mineral Resources at the Maverick Springs Project are based on, and fairly represent, information and supporting documentation reviewed, and approved by Mr Brodie Box, MAIG. Mr Box is a geologist at Cadre Geology and Mining Ltd and has adequate professional experience with the exploration and geology of the style of mineralisation and types of deposits under consideration to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr Box consents to the form and context in which the results are presented in this announcement.

The information in this announcement that relates to Exploration Results from metallurgical test work is based on, and fairly represents, information and supporting documentation compiled by Mr Peter Adamini, BSc (Mineral Science and Chemistry), who is a Member of The Australasian Institute of Mining and Metallurgy (AusIMM). Mr Adamini is a full-time employee of SGS Australia owned Independent Metallurgical Operations Pty Ltd, a wholly owned subsidiary of SGS Australia Holdings Pty Ltd, and has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr. Adamini is an independent consultant engaged by Sun Silver Limited for metallurgical representation. Mr Adamini consents to the disclosure of the information in this report in the form and context in which it appears.

*The information in this announcement that relates to previously reported Exploration Results and Estimates of Mineral Resources at the Maverick Springs Project is extracted from the Company's ASX announcements dated 14 January 2025, 26 March 2025, 2 July 2025 and 9 December 2025 (**Original Announcements**). The Company confirms that it is not aware of any new information or data that materially affects the relevant information contained in the Original Announcements and, in the case of Estimates of Mineral Resources, that all material assumptions and technical parameters underpinning the estimates continue to apply and have not materially changed.*

[3] For previously reported estimates of mineral resources see Annexure A and the Company's ASX Announcement dated 9 December 2025.

For personal use only

ANNEXURE A – MAVERICK SPRINGS MINERAL RESOURCE

Classification	Cut-off (g/t AgEq)	Tonnes (Mt)	AgEq (Moz)	AgEq (g/t)	Ag (Moz)	Ag (g/t)	Au (Moz)	Au (g/t)
Inferred	**30**	**237.3**	**539**	**71**	**347.2**	**45.5**	**2.25**	**0.30**

1. Maverick Springs Mineral Resource estimated in accordance with the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code).
2. Refer to the Company's ASX announcement dated 9 December 2025 for further details regarding the Maverick Springs Mineral Resource (**Original Announcement**). New metallurgical test work reported 4/3/26 is a modifying factor in resource estimation but the preliminary results reported above do not materially affect the mineral resource estimate in respect to metal equivalent calculations due to the similar recovery of both gold and silver. The Company confirms that it is not aware of any new information or data that materially affects the information contained in the Original Announcement and that all material assumptions and technical parameters underpinning the mineral resource estimate continue to apply and have not materially changed.
3. References to metal equivalents (AgEq) are based on an equivalency ratio of 85, which is derived from a gold price of USD$2,433 and a silver price of USD$28.50 per ounce, being derived from the average monthly metal pricing for the last three years, and average metallurgical recovery. This is calculated as follows: AgEq = Silver grade + (Gold Grade x ((Gold Price * Gold Recovery) / (Silver Price * Silver Recovery))) i.e. AgEq (g/t) = Ag (g/t) + (Au (g/t) x ((2433 x 0.85) / (28.50 x 0.85))). Metallurgical recoveries of 85% have been assumed for both silver and gold. Preliminary metallurgical recoveries were disclosed in the Company's prospectus dated 17 April 2024, which included a review of metallurgical test work completed by the prior owners of Maverick Springs. Metallurgical recoveries for both gold and silver were recorded in similar ranges, with maximum metallurgical recoveries of up to 97.5% in preliminary historical metallurgical testing in respect of silver and up to 95.8% in respect of gold. Gold recoveries were commonly recorded in the range of 80% - 90%, and the midpoint of this range has been adopted at present in respect of both silver and gold. New preliminary metallurgical results reported here demonstrate similar recoveries for Au (74%) and Ag (77%) from IBR tests, and 82.15% Au and 87.25% Ag recovery from cyanide leach tests, which would not materially affect the metal equivalent ratio and stated resource estimate. It is the Company's view that both elements referenced in the silver and gold equivalent calculations have a reasonable potential of being recovered and sold.

APPENDIX A – Composite Sample Information

Sample 1 – Total Weight – 147kg

Sample No.	Hole Id	Depth From	Depth To	Interval (m)	Au (g/t)	Ag (g/t)	Material Type
1	MR059	250.85	252.37	1.52	0.3	268	Transitional
1	MR059	252.37	253.90	1.52	0.3	174.51	Transitional
1	MR060	311.20	311.51	0.30	0.36	176.91	Transitional
1	MR060	280.42	281.94	1.52	0.33	140	Transitional
1	MR063	210.25	210.80	0.55	0.33	106	Oxidised
1	MR063	212.14	213.66	1.52	0.27	137.83	Oxidised
1	MR063	218.33	219.82	1.49	0.36	415	Oxidised
1	MR063	219.82	220.74	0.91	0.22	625	Oxidised
1	MR063	228.97	230.18	1.22	0.27	61	Oxidised
1	MR063	230.18	231.34	1.16	0.38	94.97	Oxidised
1	MR063	240.24	240.73	0.49	0.25	199.54	Oxidised
1	MR063	270.97	272.19	1.22	0.36	102.51	Transitional
1	MR065	178.31	179.83	1.52	0.25	78.86	Oxidised
1	MR065	196.60	197.82	1.22	0.44	65.4	Oxidised
1	MR065	202.08	203.55	1.46	0.3	117	Oxidised
1	MR065	215.95	216.71	0.76	0.41	230	Oxidised
1	MR065	238.78	240.00	1.22	0.25	73.71	Oxidised
1	MR065	249.33	250.82	1.49	0.33	26.8	Transitional
1	MR065	252.37	253.75	1.37	0.33	143.31	Transitional
1	MR069	134.72	135.64	0.91	0.22	103	Oxidised
1	MR069	135.64	136.55	0.91	0.33	353	Oxidised
1	MR069	183.79	185.01	1.22	0.44	139	Oxidised
1	MR069	218.85	220.37	1.52	0.25	83.4	Oxidised

Sample No.	Hole Id	Depth From	Depth To	Interval (m)	Au (g/t)	Ag (g/t)	Material Type
1	MR069	234.09	235.61	1.52	0.33	121	Oxidised
1	MR070	279.81	281.18	1.37	0.38	151	Transitional
1	MR070	281.94	283.62	1.68	0.33	74.4	Transitional
1	MR070	283.62	283.92	0.30	0.3	140	Transitional
1	MR073	208.18	208.79	0.61	0.33	60	Oxidised
1	MR073	211.23	211.84	0.61	0.36	369.94	Oxidised
1	MR073	222.20	223.11	0.91	0.36	144	Oxidised
1	MR073	258.84	259.38	0.55	0.41	77.14	Transitional
1	MR073	289.22	289.83	0.61	0.27	99.09	Fresh
1	MR076	192.79	194.16	1.37	0.22	241	Oxidised
1	MR076	206.81	208.18	1.37	0.44	140	Oxidised
1	MR082	157.58	158.04	0.46	0.38	88.11	Oxidised
1	MR082	158.95	160.32	1.37	0.3	592.11	Oxidised
1	MR082	169.47	170.84	1.37	0.44	88.9	Oxidised
1	MR082	172.21	172.82	0.61	0.3	64.6	Oxidised
1	MR082	179.53	181.05	1.52	0.27	82.29	Oxidised
1	MR082	192.63	193.40	0.76	0.22	67.89	Oxidised
1	MR082	193.40	194.77	1.37	0.25	84	Oxidised
1	MR082	204.67	206.20	1.52	0.27	91.89	Oxidised
1	MR082	206.20	207.42	1.22	0.25	356.57	Oxidised
1	MR089	222.20	223.42	1.22	0.44	247.2	Transitional
1	MR089	223.42	224.64	1.22	0.38	170.06	Transitional
1	MR089	224.64	225.86	1.22	0.36	67.2	Transitional
1	MR089	247.19	247.80	0.61	0.3	153.26	Transitional
1	MR089	248.41	248.87	0.46	0.36	322.63	Transitional
1	MR091	153.41	155.33	1.92	0.33	77.14	Oxidised
1	MR091	214.58	215.80	1.22	0.27	147.77	Oxidised
1	MR091	223.75	224.67	0.91	0.3	316.46	Oxidised
1	MR095	144.38	145.02	0.64	0.38	288	Oxidised
1	MR095	145.02	145.97	0.94	0.36	126	Oxidised
1	MR095	222.20	222.35	0.15	0.25	179	Oxidised
1	MR095	222.66	223.72	1.07	0.25	139	Oxidised
1	MR098	237.23	237.53	0.30	0.22	123	Transitional
1	MR098	238.75	239.88	1.13	0.36	118	Transitional
1	MR098	246.89	247.80	0.91	0.36	83.4	Transitional
1	MR098	247.80	248.41	0.61	0.25	73.1	Transitional
1	MR098	250.33	251.03	0.70	0.22	115	Transitional
1	MR098	253.14	253.69	0.55	0.36	88.1	Transitional
1	MR098	253.69	254.20	0.52	0.27	15	Transitional
1	MR098	254.20	254.81	0.61	0.44	80.3	Transitional
1	MR098	279.50	281.03	1.52	0.44	21.4	Transitional
1	MR099	307.09	308.15	1.07	0.25	165.6	Transitional
1	MR099	318.06	319.19	1.13	0.22	1187.31	Transitional
1	MR101	235.79	236.01	0.21	0.3	160.46	Transitional
1	MR101	236.01	236.37	0.37	0.36	64.46	Transitional
1	MR101	236.83	236.92	0.09	0.27	65.14	Transitional
1	MR101	259.02	260.51	1.49	0.25	554.06	Transitional
1	MR101	272.40	273.41	1.01	0.33	66.51	Transitional
1	MR101	298.64	299.25	0.61	0.3	125.83	Transitional
1	MR102	202.69	204.22	1.52	0.38	147.43	Oxidised
1	MR102	209.70	210.77	1.07	0.41	75.09	Oxidised
1	MR102	244.60	245.67	1.07	0.3	74.4	Transitional
1	MR102	258.47	259.99	1.52	0.33	86.74	Transitional
1	MR102	287.12	287.73	0.61	0.33	88	Transitional
1	MR103	196.78	198.18	1.40	0.22	98.2	Oxidised

Sample No.	Hole Id	Depth From	Depth To	Interval (m)	Au (g/t)	Ag (g/t)	Material Type
1	MR103	216.44	217.05	0.61	0.36	113	Oxidised
1	MR103	217.05	217.47	0.43	0.27	159	Oxidised
1	MR103	224.64	226.16	1.52	0.36	116	Oxidised
1	MR103	227.69	229.12	1.43	0.44	160	Oxidised
1	MR104	248.11	249.48	1.37	0.27	76.46	Transitional
1	MR104	249.48	249.63	0.15	0.27	296.91	Transitional
1	MR104	249.63	250.64	1.01	0.25	153.94	Transitional
1	MR105	217.02	219.55	2.53	0.44	102	Oxidised
1	MR105	237.38	238.96	1.58	0.33	81.2	Oxidised
1	MR116	256.49	257.46	0.98	0.3	166	Oxidised
1	MR116	257.46	258.93	1.46	0.27	456	Oxidised
1	MR118	267.31	267.61	0.30	0.3	293	Oxidised
1	MR118	267.61	269.14	1.52	0.3	245	Oxidised
1	MR121	181.72	183.06	1.34	0.22	256	Oxidised
1	MR121	224.58	225.92	1.34	0.27	60.69	Oxidised
1	MR121	225.92	226.53	0.61	0.38	157.37	Oxidised
1	MR121	226.53	227.81	1.28	0.27	64.8	Oxidised
1	MR121	227.81	228.11	0.30	0.22	118.29	Oxidised
1	MR121	231.40	231.71	0.30	0.44	139.2	Oxidised
1	MR121	231.71	232.87	1.16	0.38	69.6	Oxidised
1	MR121	232.87	235.58	2.71	0.38	84.69	Oxidised
1	MR121	240.88	242.32	1.43	0.27	156.34	Oxidised
1	MR122	264.57	266.09	1.52	0.33	139	Transitional
1	MR122	267.61	268.53	0.91	0.27	130	Transitional
1	MR122	268.53	269.57	1.04	0.3	136	Transitional
1	MR122	269.57	270.66	1.10	0.36	68.9	Transitional
1	MR124	141.79	142.43	0.64	0.38	100.8	Oxidised
1	MR124	147.43	149.02	1.58	0.33	74.74	Oxidised
1	MR124	151.49	152.70	1.22	0.22	211.2	Oxidised
1	MR124	157.55	158.04	0.49	0.27	180.69	Oxidised
1	MR124	158.04	159.41	1.37	0.38	85.37	Oxidised
1	MR124	165.63	166.54	0.91	0.44	74.4	Oxidised
1	MR126	130.15	131.67	1.52	0.27	143	Oxidised
1	MR126	133.50	134.93	1.43	0.3	86.7	Oxidised
1	MR126	178.64	179.65	1.01	0.27	87.2	Oxidised
1	MR126	214.88	216.41	1.52	0.25	75.4	Oxidised
1	MR126	219.09	220.64	1.55	0.3	137	Oxidised
1	MR127	196.08	197.69	1.62	0.27	123	Oxidised
1	MR127	197.69	199.06	1.37	0.27	83.8	Oxidised
1	MR127	208.67	208.76	0.09	0.25	143	Oxidised
1	MR127	208.76	208.85	0.09	0.25	75.4	Oxidised
1	MR127	215.04	216.56	1.52	0.41	162	Oxidised
1	MR127	233.05	233.26	0.21	0.41	121	Oxidised
1	MR127	234.76	236.34	1.58	0.27	182	Oxidised
1	MR127	239.24	240.82	1.58	0.3	757	Oxidised
1	MR127	240.82	242.35	1.52	0.36	318	Oxidised
1	MR127	242.35	243.87	1.52	0.3	135	Oxidised
1	MR127	243.87	245.39	1.52	0.41	181	Oxidised
1	MR127	245.39	246.92	1.52	0.33	94.2	Oxidised
1	MR127	246.92	248.50	1.58	0.3	80.8	Oxidised
1	MR127	248.50	250.06	1.55	0.33	195	Oxidised
1	MR127	251.58	251.89	0.30	0.3	88.5	Transitional
1	MR127	254.26	255.79	1.52	0.3	93.4	Transitional
Head Assay Grade					**0.32**	**276**	
Total Weight						**147kg**	

Sample 2 – Total Weight – 127kg

Sample No.	Hole Id	Depth From	Depth To	Interval (m)	Au (g/t)	Ag (g/t)	Material Type
2	MR050	207.26	210.01	2.74	0.77	67.2	Oxidised
2	MR050	210.01	211.53	1.52	1.35	225	Oxidised
2	MR059	316.57	317.78	1.22	0.49	125	Transitional
2	MR059	317.78	319.74	1.95	0.66	115	Transitional
2	MR059	199.64	200.95	1.31	3.33	80.4	Oxidised
2	MR059	200.95	202.02	1.07	1.1	82.8	Oxidised
2	MR059	202.02	204.22	2.19	2.45	28.2	Oxidised
2	MR059	206.81	208.12	1.31	0.69	92.1	Oxidised
2	MR059	208.12	209	0.88	0.55	101	Oxidised
2	MR059	209	210.22	1.22	4.37	408	Oxidised
2	MR059	215.19	216.71	1.52	1.05	285	Oxidised
2	MR059	238.35	239.3	0.94	0.58	115	Transitional
2	MR059	239.3	240.79	1.49	0.94	157.71	Transitional
2	MR059	240.79	242.26	1.46	0.77	84.4	Transitional
2	MR060	304.8	306.32	1.52	0.49	102	Transitional
2	MR063	208.64	209.4	0.76	0.58	93.6	Oxidised
2	MR063	209.4	210.25	0.85	0.88	156	Oxidised
2	MR065	190.5	192.27	1.77	0.8	99.8	Oxidised
2	MR065	208.79	210.16	1.37	0.74	292	Oxidised
2	MR073	180.59	181.81	1.22	0.85	221.14	Oxidised
2	MR073	183.18	184.28	1.1	0.69	176.91	Oxidised
2	MR073	184.28	184.5	0.21	0.83	94.97	Oxidised
2	MR073	208.79	210.01	1.22	0.69	799.2	Oxidised
2	MR073	210.01	211.1	1.1	0.63	133.37	Oxidised
2	MR073	211.84	213.36	1.52	0.6	63.09	Oxidised
2	MR073	217.93	219.46	1.52	0.72	218.74	Oxidised
2	MR073	223.11	224.33	1.22	0.99	89.14	Oxidised
2	MR076	197.11	198.64	1.52	0.52	84.34	Oxidised
2	MR076	203.61	205.13	1.52	0.6	144	Oxidised
2	MR076	205.44	206.81	1.37	0.55	76.6	Oxidised
2	MR076	210.98	212.45	1.46	0.49	180	Oxidised
2	MR082	156.36	157.58	1.22	0.47	134.74	Oxidised
2	MR082	160.93	161.85	0.91	1.73	135	Oxidised
2	MR082	161.85	162.92	1.07	0.88	265	Oxidised
2	MR082	191.11	192.63	1.52	0.47	196.8	Oxidised
2	MR082	212.6	213.36	0.76	0.6	67.54	Oxidised
2	MR089	226.5	227.23	0.73	0.77	84	Transitional
2	MR089	227.23	227.75	0.52	1.54	119.66	Transitional
2	MR089	227.75	228.6	0.85	0.49	108	Transitional
2	MR089	228.6	229.67	1.07	0.96	153.6	Transitional
2	MR089	235.92	236.65	0.73	1.79	64.46	Transitional
2	MR089	244.39	245.97	1.58	0.69	108	Transitional
2	MR089	248.87	249.33	0.46	0.69	687.43	Transitional
2	MR089	249.33	249.78	0.46	0.77	1128.69	Transitional
2	MR089	249.78	250.09	0.3	0.58	1032	Transitional
2	MR089	250.09	250.55	0.46	0.49	685.37	Transitional
2	MR091	199.95	200.95	1.01	0.66	112.11	Oxidised
2	MR091	220.43	221.59	1.16	0.58	593.49	Oxidised
2	MR091	242.93	244.42	1.49	0.74	118.63	Oxidised
2	MR095	143.71	144.38	0.67	0.52	1084	Oxidised

Sample No.	Hole Id	Depth From	Depth To	Interval (m)	Au (g/t)	Ag (g/t)	Material Type
2	MR095	218.85	219.76	0.91	0.58	70.6	Oxidised
2	MR095	222.35	222.66	0.3	0.52	332.23	Oxidised
2	MR095	255.12	256.64	1.52	0.8	94	Transitional
2	MR098	224.03	225.55	1.52	0.77	139.54	Oxidised
2	MR098	225.55	226.16	0.61	0.6	59.66	Oxidised
2	MR098	227.84	229.36	1.52	1.05	111	Oxidised
2	MR098	229.36	230.58	1.22	1.68	233	Oxidised
2	MR098	235.92	236.92	1.01	0.55	241	Transitional
2	MR098	239.88	241.01	1.13	0.47	103	Transitional
2	MR098	241.92	242.83	0.91	0.58	121	Transitional
2	MR098	251.03	251.31	0.27	0.47	149	Transitional
2	MR098	251.31	251.61	0.3	0.88	145	Transitional
2	MR098	251.61	252.19	0.58	0.69	161	Transitional
2	MR098	256.49	257.13	0.64	0.47	105	Transitional
2	MR098	257.53	257.86	0.34	0.88	88.2	Transitional
2	MR098	259.38	259.99	0.61	0.94	61.71	Transitional
2	MR101	230.73	231.95	1.22	0.6	418.29	Transitional
2	MR101	234.09	234.76	0.67	0.49	60.34	Transitional
2	MR101	238.41	239.27	0.85	0.49	67.54	Transitional
2	MR101	241.98	243.38	1.4	0.47	490.63	Transitional
2	MR102	316.38	317.91	1.52	0.55	95.31	Transitional
2	MR102	319.43	320.95	1.52	0.47	60.3	Transitional
2	MR102	196.75	198.27	1.52	2.48	62.4	Oxidised
2	MR102	198.27	199.64	1.37	1.16	204.34	Oxidised
2	MR102	228.6	230.12	1.52	0.58	61.37	Oxidised
2	MR102	257.25	258.47	1.22	0.52	63.09	Transitional
2	MR102	285.6	287.12	1.52	2.34	103	Transitional
2	MR103	206.93	207.36	0.43	0.72	85.1	Oxidised
2	MR103	207.84	209.06	1.22	0.47	117	Oxidised
2	MR103	219.7	220.8	1.1	0.72	762	Oxidised
2	MR103	220.8	222.29	1.49	0.49	72	Oxidised
2	MR103	263.07	263.44	0.37	0.55	92.2	Transitional
2	MR104	256.58	257.86	1.28	1.92	108.34	Transitional
2	MR104	260.3	262.13	1.83	1.48	60	Transitional
2	MR104	262.13	263.35	1.22	2.28	197.83	Transitional
2	MR104	263.35	264.69	1.34	1.21	93.26	Transitional
2	MR105	210.98	212.6	1.62	0.55	11.3	Oxidised
2	MR121	208.03	208.76	0.73	1.21	57.4	Oxidised
2	MR121	210.28	210.92	0.64	0.77	263	Oxidised
2	MR121	210.92	211.53	0.61	1.48	235	Oxidised
2	MR121	211.53	212.26	0.73	1.21	123	Oxidised
2	MR121	212.26	212.51	0.24	0.72	117	Oxidised
2	MR121	212.51	214.18	1.68	0.69	85.1	Oxidised
2	MR121	221.99	222.53	0.55	0.55	96.34	Oxidised
2	MR122	270.66	272.19	1.52	0.49	92.9	Transitional
2	MR122	283.77	285.29	1.52	0.47	18.3	Transitional
2	MR122	297.33	298.55	1.22	0.55	208	Transitional
2	MR122	298.55	299.62	1.07	1.16	69.8	Transitional
2	MR124	138.99	140.57	1.58	0.49	630.51	Oxidised
2	MR124	140.57	141.79	1.22	1.1	634.63	Oxidised
2	MR124	155.54	156.33	0.79	0.49	67.54	Oxidised
2	MR124	156.33	157.55	1.22	0.66	405.26	Oxidised
2	MR124	186.32	187.27	0.94	0.49	86.06	Oxidised
2	MR124	191.51	192.33	0.82	0.49	60.69	Oxidised
2	MR127	214.27	215.04	0.76	0.94	107	Oxidised

Sample No.	Hole Id	Depth From	Depth To	Interval (m)	Au (g/t)	Ag (g/t)	Material Type
2	MR127	216.56	218.08	1.52	0.47	152	Oxidised
2	MR127	221.99	223.63	1.65	1.46	265	Oxidised
2	MR127	233.26	233.57	0.3	0.52	82.6	Oxidised
2	MR127	233.57	234.03	0.46	0.52	399	Oxidised
2	MR127	234.03	234.76	0.73	0.49	94.3	Oxidised
2	MR127	236.34	237.68	1.34	0.72	1103	Oxidised
2	MR127	237.68	239.24	1.55	0.55	1133	Oxidised
2	MR127	250.06	251.58	1.52	0.55	237	Transitional
2	MR127	251.89	253.29	1.4	0.55	68.7	Transitional
Head Assay Grade					**0.76**	**226**	
Total Weight						**126kg**	

APPENDIX B – Drill Collar Database

DHID	DEPTH (m)	EAST (m)	NORTH (m)	ELEV (m)	AZM	DIP
HP-1	129.54	644,777	4,444,421	2,185	0	-90
HP-2	116.74	644,282	4,445,261	2,289	0	-90
MR001	74.68	644,762	4,443,989	2,188	0	-90
MR002	91.44	644,791	4,443,991	2,195	0	-90
MR003	54.86	644,822	4,443,988	2,202	0	-90
MR004	92.96	643,782	4,444,005	2,208	0	-90
MR005	27.43	643,814	4,443,992	2,206	0	-90
MR006	9.14	644,914	4,443,909	2,215	0	-90
MR007	56.39	644,915	4,443,916	2,214	0	-90
MR008	99.06	644,983	4,443,864	2,225	0	-90
MR009	99.06	644,974	4,443,859	2,226	0	-90
MR010	103.63	644,975	4,443,861	2,225	0	-90
MR011	42.67	644,915	4,443,918	2,216	0	-90
MR012	99.06	644,828	4,443,931	2,201	0	-90
MR013	68.58	644,800	4,443,930	2,195	0	-90
MR014	88.39	644,690	4,443,986	2,177	0	-90
MR015	156.97	644,907	4,444,303	2,233	0	-90
MR016	167.64	644,957	4,444,333	2,229	0	-90
MR017	91.44	644,963	4,444,283	2,232	0	-90
MR018	48.77	644,894	4,444,360	2,222	0	-90
MR019	109.73	644,974	4,444,005	2,219	0	-90
MR020	7.62	644,873	4,444,045	2,213	0	-90
MR021	15.24	644,969	4,444,139	2,231	0	-90
MR022	60.96	644,907	4,444,170	2,233	0	-90
MR023	24.38	644,919	4,444,024	2,218	0	-90
MR024	18.29	644,931	4,444,018	2,217	0	-90
MR025	80.77	645,025	4,443,984	2,218	0	-90
MR026	35.05	645,037	4,444,350	2,202	0	-90
MR027	27.43	645,070	4,444,350	2,197	0	-90
MR028	30.48	645,160	4,444,721	2,165	0	-90
MR029	67.06	645,377	4,444,613	2,150	0	-90
MR030	25.91	645,269	4,444,667	2,156	0	-90
MR031	27.43	645,154	4,444,590	2,165	0	-90
MR032	48.77	645,383	4,444,482	2,165	0	-90
MR033	115.82	642,985	4,445,065	2,166	0	-90
MR034	59.44	643,028	4,444,992	2,169	0	-90
MR035	117.35	642,701	4,443,710	2,093	0	-90
MR036	111.25	642,706	4,443,642	2,108	0	-90
MR037	38.1	642,702	4,443,595	2,113	0	-90
MR038	128.02	645,843	4,445,719	2,130	0	-90
MR039	103.63	646,787	4,446,253	2,067	0	-90
MR040	182.88	645,676	4,444,969	2,137	0	-90
MR041	141.73	644,811	4,443,947	2,200	0	-90
MR042	164.59	644,700	4,443,997	2,178	0	-90
MR043	195.07	644,985	4,443,993	2,220	0	-90
MR044	85.34	645,018	4,443,975	2,218	0	-90

DHID	DEPTH (m)	EAST (m)	NORTH (m)	ELEV (m)	AZM	DIP
MR045	188.98	644,973	4,443,866	2,226	0	-90
MR046	175.26	644,585	4,444,055	2,165	0	-90
MR047	64.01	644,928	4,444,020	2,217	0	-90
MR048	115.82	644,616	4,444,175	2,169	0	-90
MR049	171.6	644,935	4,444,015	2,218	0	-90
MR050	213.66	644,503	4,443,960	2,160	0	-90
MR051	206.35	644,612	4,443,905	2,173	0	-90
MR052	51.82	644,821	4,443,799	2,197	0	-90
MR053	201.17	645,092	4,443,799	2,207	0	-90
MR054	162.15	644,727	4,443,846	2,181	0	-90
MR055	201.17	644,930	4,443,742	2,211	0	-90
MR056	195.07	644,829	4,443,801	2,197	0	-90
MR057	140.36	644,725	4,444,122	2,182	0	-90
MR058	393.19	645,848	4,445,704	2,131	0	-90
MR059	502.16	644,498	4,443,963	2,160	91	-90
MR060	387.71	644,391	4,444,017	2,171	196	-90
MR061	609.6	644,458	4,442,980	2,195	0	-90
MR062	358.75	644,369	4,444,165	2,186	258	-90
MR063	312.42	644,471	4,444,115	2,171	259	-89
MR064	557.78	645,377	4,444,614	2,151	239	-90
MR065	316.99	644,593	4,444,051	2,166	274	-90
MR066	609.6	645,157	4,444,722	2,165	190	-90
MR067	286.51	645,105	4,444,054	2,195	0	-90
MR068	487.68	645,216	4,444,561	2,160	137	-90
MR069	324.22	644,723	4,443,860	2,182	8	-90
MR070	388.62	644,399	4,444,286	2,188	260	-90
MR071	396.24	645,273	4,444,394	2,162	0	-90
MR072	304.5	644,619	4,443,903	2,175	24	-90
MR073	324.22	644,512	4,444,229	2,176	246	-90
MR074	374.23	644,291	4,444,074	2,178	345	-90
MR075	330.71	645,050	4,444,361	2,199	317	-90
MR076	332.54	644,613	4,444,177	2,169	40	-90
MR077	329.18	645,051	4,444,228	2,207	214	-90
MR078	518.16	645,326	4,444,227	2,179	68	-90
MR079	548.64	645,378	4,444,884	2,162	20	-90
MR080	607.47	645,427	4,444,439	2,168	301	-90
MR081	516.64	645,322	4,445,047	2,158	349	-90
MR082	281.03	644,725	4,444,121	2,184	172	-90
MR083	615.7	645,545	4,444,930	2,152	291	-90
MR084	603.5	645,491	4,445,101	2,156	349	-90
MR085	145.3	645,110	4,444,074	2,195	0	-90
MR086	349	645,368	4,444,070	2,194	28	-90
MR087	617.22	645,772	4,444,835	2,143	347	-90
MR088	542.54	645,466	4,445,317	2,156	185	-90
MR089	322.78	645,052	4,444,349	2,199	5	-90
MR090	518.16	645,537	4,444,394	2,174	228	-90
MR091	296.88	644,836	4,444,065	2,201	352	-89
MR092	402.34	644,966	4,443,857	2,225	306	-90
MR093	576.07	645,427	4,444,724	2,147	177	-90
MR094	569.98	645,488	4,444,560	2,156	8	-90
MR095	365.15	644,826	4,444,343	2,203	0	-90
MR096	640.08	645,593	4,444,775	2,141	79	-90
MR097	308.46	644,890	4,443,628	2,204	0	-90
MR098	458.66	644,478	4,443,907	2,160	2	-89
MR099	443.18	644,475	4,443,906	2,158	311	-89
MR100	738.23	643,817	4,443,989	2,206	260	-90
MR101	492.86	644,419	4,443,801	2,155	280	-89
MR102	401.73	644,538	4,444,012	2,162	335	-89
MR103	419.16	644,533	4,444,081	2,165	200	-89
MR104	426.57	644,446	4,443,990	2,164	340	-89
MR105	396.36	644,928	4,444,018	2,218	242	-89
MR106	603.5	644,260	4,444,326	2,196	241	-90
MR107	412.7	644,402	4,443,740	2,153	304	-88
MR108	633.98	643,683	4,444,009	2,224	340	-89

DHID	DEPTH (m)	EAST (m)	NORTH (m)	ELEV (m)	AZM	DIP
MR109	609.6	642,936	4,444,163	2,119	57	-88
MR110	505.97	642,744	4,443,716	2,095	280	-90
MR111	981.46	642,976	4,445,046	2,164	230	-89
MR112	609.6	646,370	4,445,662	2,091	35	-87
MR113	926.59	642,926	4,445,355	2,179	270	-89
MR114	589.79	645,790	4,444,954	2,131	266	-89
MR115	609.6	646,790	4,446,254	2,067	3	-89
MR116	356.77	644,965	4,444,274	2,232	169	-88
MR117	822.96	642,906	4,443,424	2,117	39	-89
MR118	387.1	644,448	4,443,852	2,156	116	-45
MR119	755.9	642,312	4,443,683	2,074	197	-89
MR120	655.32	643,547	4,442,960	2,099	123	-89
MR121	357.53	644,640	4,444,027	2,173	249	-90
MR122	421.39	644,447	4,443,852	2,156	118	-67
MR123	609.6	644,120	4,444,017	2,167	261	-90
MR124	351.13	644,673	4,443,882	2,179	121	-89
MR125	391.06	645,153	4,445,003	2,177	276	-89
MR126	314.55	644,760	4,443,967	2,187	45	-88
MR127	370.64	644,587	4,443,986	2,168	351	-89
MR128	405.32	644,446	4,443,854	2,156	294	-69
MR129	304.8	644,680	4,444,799	2,206	274	-89
MR130	304.8	644,572	4,444,578	2,196	186	-89
MR131	310.9	644,546	4,444,364	2,181	245	-89
MR132	304.8	644,610	4,444,362	2,179	284	-89
MR133	304.8	644,633	4,444,484	2,184	181	-89
MR134	304.8	644,785	4,444,598	2,190	0	-90
MR135	304.8	644,842	4,444,806	2,202	0	-90
MR03-136	298.7	644,681	4,444,261	2,175	11	-89
MR03-137	152.4	644,772	4,444,237	2,191	0	-90
MR03-137A	286.51	644,771	4,444,241	2,191	83	-89
MR03-138	365.76	644,555	4,443,679	2,168	344	-89
MR03-139	335.28	644,700	4,445,284	2,208	289	-89
MR03-140	181.36	644,569	4,444,848	2,217	0	-90
MR03-140A	304.8	644,569	4,444,848	2,217	241	-89
MR03-141	304.8	644,666	4,444,582	2,194	57	-89
MR03-142	286.51	644,509	4,444,497	2,194	172	-88
MR03-143	265.18	644,432	4,444,405	2,196	109	-89
MR03-144	304.8	644,817	4,444,477	2,193	27	-89
MR03-145	231.65	644,722	4,444,406	2,180	27	-89
MR03-146	210.31	644,902	4,444,565	2,194	0	-90
MR03-147	256.03	644,760	4,444,706	2,198	224	-89
MR03-148	297.18	644,880	4,444,686	2,192	147	-89
MR03-149	190.5	644,669	4,444,685	2,201	0	-90
MR04-150	304.8	644,823	4,444,910	2,213	164	-88
MR04-151	304.8	644,559	4,444,731	2,204	164	-89
MR04-152	304.8	644,671	4,444,696	2,202	60	-89
MR04-153	304.8	644,766	4,444,709	2,198	241	-89
MR04-154	304.8	644,897	4,444,571	2,189	175	-89
MR04-155	304.8	644,427	4,444,587	2,204	283	-89
MR04-156	310.9	644,425	4,444,707	2,215	221	-89
MR04-157	304.8	644,822	4,445,123	2,190	209	-89
MR04-158	304.8	644,326	4,444,600	2,214	272	-89
MR04-159	304.8	644,429	4,444,493	2,196	327	-89
MR04-160	304.8	645,033	4,444,512	2,184	148	-89
MR04-161	304.8	644,923	4,444,800	2,202	0	-89
MR04-162	304.8	644,655	4,444,923	2,219	356	-89
MR06-163	304.8	644,920	4,444,940	2,226	60	-89
MR06-164	304.8	644,723	4,445,062	2,225	79	-89
MR06-165	304.8	644,804	4,444,989	2,218	332	-89
MR06-166	335.28	644,492	4,444,885	2,225	263	-89
MR06-167	316.99	644,419	4,444,792	2,223	50	-89
MR06-168	335.28	644,303	4,444,693	2,221	198	-89
MR06-169	280.42	644,272	4,443,605	2,147	0	-90
MR06-170	286.51	644,273	4,443,605	2,147	125	-69

DHID	DEPTH (m)	EAST (m)	NORTH (m)	ELEV (m)	AZM	DIP
MR06-171	316.99	644,270	4,444,526	2,214	34	-89
MR06-172	304.8	644,372	4,444,448	2,201	314	-89
MR06-173	260.6	644,922	4,444,473	2,205	134	-89
MR06-174	304.8	644,357	4,443,686	2,151	97	-89
MR06-175	310.9	644,930	4,443,744	2,213	185	-89
MR06-176	304.8	644,826	4,443,812	2,199	288	-89
MR06-177	158.5	642,980	4,445,373	2,187	18	-89
MR06-178	152.4	642,887	4,445,422	2,184	0	-90
MR06-179	152.4	642,960	4,445,305	2,178	0	-90
MR06-180	152.4	642,881	4,445,325	2,184	0	-90
MR08-181	341.38	644,417	4,444,782	2,226	338	-70
MR08-182	335.28	644,417	4,444,794	2,223	291	-70
MR08-183	341.38	644,450	4,444,936	2,234	31	-89
MR08-184	350.52	644,390	4,444,972	2,241	303	-89
MR08-185	256.03	644,555	4,445,004	2,233	90	-89
MR24-186	294.13	644,343	4,444,871	2,245	0	-90
MR24-187	178.31	644,424	4,444,783	2,226	120	-70
MR24-188	268.22	644,425	4,444,787	2,226	0	-90
MR24-189	68.58	644,298	4,445,054	2,252	0	-90
MR24-189A	320.04	644,301	4,445,054	2,256	0	-90
MR24-190	304.8	644,452	4,444,925	2,235	0	-90
MR24-191	301.75	644,448	4,445,059	2,243	0	-90
MR24-192	326.14	644,280	4,444,767	2,240	0	-90
MR24-193	350.52	644,152	4,444,583	2,227	0	-90
MR24-194	320.04	644,335	4,444,606	2,214	0	-90
MR24-195	304.8	644,306	4,444,680	2,223	0	-90
MR24-196	295.66	644,200	4,444,681	2,240	0	-90
MR24-197	304.8	644,413	4,444,703	2,217	0	-90
MR24-198	352.04	644,400	4,445,185	2,268	0	-90
MR24-199	338.33	644,479	4,445,126	2,259	0	-90
MR24-200	304.8	644,643	4,445,092	2,242	0	-90
MR24-201	304.8	644,722	4,445,038	2,226	0	-90
MR24-202	320.04	644,806	4,444,980	2,219	0	-90
MR24-203	365.76	644,260	4,445,213	2,285	0	-90
MR24-204	335.28	644,219	4,445,119	2,270	0	-90
MR24-205	210.31	644,422	4,444,785	2,224	120	-70
MR24-206	326.14	644,387	4,444,959	2,245	0	-90
MR24-207	335.28	644,235	4,444,516	2,213	0	-90
MR24-208	320.04	644,552	4,444,991	2,235	0	-90
MR24-209	320.04	644,662	4,444,913	2,218	0	-90
MR24-210	252.98	644,567	4,444,845	2,217	0	-90
MR25-211	360.27	644,400	4,445,179	2,265	30	-60
MR25-212	357.53	644,481	4,445,137	2,257	30	-60
MR25-213	253.11	644,478	4,445,126	2,257	0	-90
MR25-214	354.18	644,412	4,444,707	2,214	0	-90
MR25-215	201.17	644,794	4,445,151	2,195	30	-70
MR25-216	249.94	644,272	4,444,768	2,240	0	-90
MR25-217	219.46	644,335	4,444,868	2,243	300	-65
MR25-218	308.15	644,422	4,444,794	2,224	120	-70
MR25-219	274.32	644,194	4,444,678	2,240	0	-90
MR25-220	188.98	644,447	4,445,065	2,244	0	-90
MR25-221	360.27	644,259	4,445,218	2,289	30	-60
MR25-227	342.9	644,532	4,443,869	2,165	0	-90
MR25-228	152.4	644,485	4,443,900	2,160	300	-86
MR25-229	340.46	644,425	4,443,916	2,163	0	-89
MR25-230	335.28	644,511	4,443,936	2,163	110.3	-75.35
MR25-231	166.73	644,484	4,444,034	2,164	0	-90
MR25-232	140.21	644,795	4,443,797	2,196	300	-82
MR25-233	152.4	644,538	4,444,134	2,169	0	-90
MR25-234	335.28	644,610	4,444,112	2,168	300	-86
MR25-235	202.69	644,525	4,444,008	2,164	0	-90
MR25-237	246.28	644,701	4,443,985	2,177	0	-90
MR25-247	305.07	644,585	4,444,049	2,164	0	-90
MR25-248	48.77	644,852	4,443,830	2,198	0	-90

DHID	DEPTH (m)	EAST (m)	NORTH (m)	ELEV (m)	AZM	DIP
MR25-248a	134.11	644,852	4,443,825	2,202	0	-90
MR25-249	164.59	644,903	4,443,892	2,210	300	-80
MR25-250	331.01	644,579	4,443,973	2,170	0	-90
MR25-253	59.44	644,913	4,443,920	2,211	300	-85
MR25-253a	152.4	644,914	4,443,920	2,218	300	-85
MR25-253b	134.11	644,914	4,443,920	2,218	300	-85

JORC Code, 2012 – Table 1

Section 1 Sampling Techniques and Data – Maverick Springs Silver Gold Project

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. • In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	**Historic** • Samples have been assayed at various laboratories through the history of ownership. Pre 2002 NQ core and 'five feet' (1.5m) RC and percussion composite length samples from ~94 drill holes were analysed at Angst Resources' Goldbar Mine laboratory in Beatty, Nevada. Vista's 2002-2006 also utilised 1.5m samples, including wet samples (flocculent mix) and were assayed by AAL in Sparks, Nevada. 2008 RC drilling was analysed by ALS Chemex in Reno and Vancouver. • Pre-2002 samples are reported to have been subject to 1 assay ton (AT) fire assay with AA finish for gold and silver, additional tests via cyanide soluble leach were not used in resource calculations. Approximately 5,000 pulps from this era have been re-analysed by four acid digest at AAL in 2025. • 2002-2006 drill samples underwent similar analysis which record typical dry, crush, split, pulverise preparation work. Routine analyses at AAL included 1 assay ton fire with an AA finish for gold and 0.4-gram aqua regia leach with AA finish for silver. Any silver value of 100 parts per million (ppm) or greater was re-run by 1 assay ton fire with a gravimetric finish. Results were reported in ppm with detection limits of 0.005 ppm for gold and 0.05 ppm for silver. • 2008 RC drilling utilised fire assay for gold and a 33 element ICP-AES analysis (4 acid digest) for silver and pathfinder elements. Silver was re-analysed by fire assay if over 100ppm. • Assay certificates have not been provided for Pre 2002 drilling hence the pulp re-analysis program. 2002 to 2008 assay certificates have been supplied and recompiled in the database. **2024 and 2025** • 2024 and 2025 RC drilling has used a rotary wet splitter for wet sample collection at 5ft intervals (1.52m) into large bags contained in 3 gallon buckets which are dried before dispatch in effort to reduce loss of fines and produce representative sample. • Drill assay analysis of silver and multi-elements is by 4 acid digest with ICP-MS or OES finish, over limit silver (100g/t) analysed by gravimetric fire assay and gold analysed by fire assay with ICP-OES finish. • 2025 diamond drilling includes HQ and PQ core drilling from surface and as diamond tails. Core is cut in half for sampling. • Samples delineated by drill string and downhole surveys utilise a Reflex Omni X-42 North Seeking Gyro calibrated prior to use, with readings taken typically every 50ft. • 2025 Metallurgical samples were composited from historic drill core material representative of oxide and transitional material. Two composite samples were prepared from 147kg and 127kg total weight. • Head assay grades for metallurgical test work were derived from 30g fire assay for gold and 0.2g 4-acid digest for silver on pulverised sample. • Intermittent Bottle Roll (IBR) tests were conducted on both sample composites at three crush sizes; P100 6.3mm, 3.35mm and 2.0mm, with each sample weight being 5kg.

Criteria	JORC Code explanation	Commentary
		• Cyanide Leach tests were conducted on both sample composites at three grind sizes (P80), 106 µm, 75µm and 53µm, with each sample weight being 1kg.
Drilling techniques	• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	• Drilling is via NQ, HQ and PQ diamond coring, RC drilling, conventional rotary and hammer drilling methods. **Historic** • 2002-2003 RC drilling is recorded as via 5 1/8th-5 1/4” inch face sampling hammer and 2004 via 5.5”. In some instances a tri-cone bit was used to aid sample recovery. Majority of the open-hole techniques are too shallow to be utilised in the resource estimate and no issues of contamination from these methods are expected. • All core is believed to be NQ, with some RC and HQ precollars. • Core orientation techniques or methods are currently unknown. **2024 and 2025** • 2024 RC drilling is using a 2013 Foremost MPD Explorer track mounted rig drilling 5” holes. RC sampled via a traditional hammer setup (2ft lead between the bit interface and the sample return) which has shown the most reliable recovery. Water injection is used to maximise sample recovery due to ground conditions and is typical to the area. • Diamond drilling utilises triple tube for HQ or PQ size core drilling by a track mounted Longyear LF 90 drill rig or Hydrocore 4000. • Diamond drilling is often as diamond tails with RC precollar depths varying based on mineralisation potential and overburden thickness. • Core is not oriented due to ground conditions.
Drill sample recovery	• Method of recording and assessing core and chip sample recoveries and results assessed. • Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	**Historic** • Drilling recoveries are not specifically recorded in the logging database and drill recovery issues in RC drilling have been reported through broken ground. 2002-2008 drilling implemented additional procedures to enhance recovery: A rotary wet splitter was used to collect composites which were mixed with a flocculent and large 20-30pound samples taken to minimise loss of fines. This drilling also included using hammers with a cross-over sub and tricone bits. • Diamond drilling recovery has not been recorded in the database but 2006 reports state that viewing some of the core showed no obvious issues. Compilation of paper logs is in progress to provide more information on historic core sampling and recoveries. • A slight bias in the 2002 RC drilling towards lower gold and silver grades compared to diamond drill results and 2003 RC drilling is reported from an investigation by Thomas C. Doe and Associates provided to Snowden in 2004. This may be due to the loss of fines but is not considered significant based on the small amount of drilling data affected and that it doesn’t contribute to over-estimation. It is unknown if similar issues existed in Pre 2002 RC drilling. **2025** • RC drilling utilizes a rotary wet splitter to maximise recovery of drill material and fines with samples in large 20x24” bags with water allowed to seep out through canvas bag before analysis. • Poor sample recovery is recorded by visual inspection and laboratory weights. • No Sample is generally due to broken ground conditions. • Sample recovery does not appear to contribute to a sample bias from results received so far. • Diamond drilling recoveries are measured on drill core and against run lengths. Core loss is recorded as no sample intervals. Core loss is typical in heavily broken ground.
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	• The logging is qualitative in nature. • The historic dataset shows 50% of the total drill holes at the Project have been logged with a broad formation unit, 30% has detailed logging and 20% has not been logged. Legacy data compilation and relogging remains ongoing. • 100% of 2024 and 2025 drilling has been logged by Sun Silver. • Logging intervals are in imperial units and are converted to metric.

Criteria	JORC Code explanation	Commentary
	• Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. • The total length and percentage of the relevant intersections logged.	
Subsampling techniques and sample preparation	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all subsampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled.	• 5ft (1.5m) composite samples were taken during percussion drilling (RC, rotary) and drill core was sampled as half core cut longitudinally down its axis at various interval lengths to mineralised/geological boundaries. Core assay intervals range from 0.1 foot (3cm) to 10.7 ft (3.26m). **Historic** • RC drilling records are minimal, but reports detail splitting samples fed from a cyclone. Vista/SS 2002-2008 drilling details the use of RC tricone bits and hammers with a cross-over sub to improve recovery. • They used wet sampling via 36" rotary wet splitter, mixed with a flocculent and collected into a sample bag before being allowed to dry. This produced ~5kg samples in an attempt to minimise loss of fines. • Diamond drilling sampling protocols are not specifically known for Pre 2002 diamond holes, but no core loss exists in the sample database provided. • Field duplicates are reported to have been used since the 2002 RC drilling but have not been provided and no records exist from prior drilling. 2008 drilling showed field duplicates, blanks and standards insert every ~20 samples. **2024 and 2025** • 5ft (1.52m) composite samples were taken during RC drilling. • RC drilling utilises wet drilling with sampling via a rotary wet splitter. Large samples are taken in attempt to minimise loss of fines. Field duplicates are used to as checks for this method. • Sample sizes are considered to reflect industry standards, be appropriate for the material being sampled and show attempts made to improve recovery. • Diamond core is cut down the longitudinal axis with half core sampled. Sample lengths vary from 0.15m to 1.52m. Samples are made around intervals of core loss as to not carry grade through core loss. • 2024 and 2025 drilling inserted standards, blanks, and duplicates into the sample stream at approximately 1 in 20 samples near mineralisation, and ~1 in 40 in overburden.
Quality of assay data and laboratory tests	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (e.g., standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e., lack of bias) and precision have been established.	**Historic** • QAQC protocols utilising Certified Reference Material (standards), blanks and duplicates have been reported in 2002-2008 drill programs under instruction from Snowden. Results from standards have been reviewed for some drilling but no blanks or duplicates have been. No issues were raised by Snowden, SRK or SGS in previous reports. • There is no QC data on drilling prior to 2002. Subsequently this data underwent investigative checks via re-assaying pulps by independent laboratories in 2004 and has recently undergone more significant reanalysis testwork in 2025. Silver by fire assay is considered total but due to lack of QC there may be limitations to this. • All samples from 2002-2006 were prepared and assayed by an independent commercial laboratory (AAL), and 2008 drilling by ALS Chemex whose instrumentation are regularly calibrated, utilising appropriate internal checks in QAQC. Silver underwent analysis by aqua-regia (2 acid digest) and may not be considered total digestion. • Gold by fire assay for all historic test work is considered total. **2024 and 2025** • Internal lab QAQC and field inserted blanks, standards and duplicates inserted into the 2024 sample stream show acceptable results. Rare cases of failed blanks have been rectified by re-analysis of pulps. • All CRM is generally within 2 standard deviations with some outliers within 3 standard deviations from the expected.

Criteria	JORC Code explanation	Commentary
		• Laboratory procedures are considered total utilising fire assay for gold and four acid digest for silver and mutli-elements, overlimit samples are sent for re-assay (silver by gravimetric fire assay). • Pulp reanalysis of historic pulps utilised internal lab QC of blanks, standards and repeats, and company inserted standards for validation checks with good performance.

Verification of sampling and assaying	• The verification of significant intersections by either independent or alternative company personnel.
	• The use of twinned holes.
	• Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.
	• Discuss any adjustment to assay data.
		Historic
		• Significant intercepts have not specifically been verified but Snowden reviewed and re-sampled select intervals from 2002, 2003 and 2006 and reported good correlation with original assays. Bulk historic assays have been re-assayed for verification checks detailed in the Snowden and SGS reports but raw data has not been provided.
		• Primary data and data entry details are not provided for all drill campaigns which has been passed through several operators over the years, but all compiled data has been provided in csv(digital) format which is assumed to have been collected and transcribed accurately from prior operators. 2025 relogging and pulp reanalysis has utilised paper copies of logging and sampling of pulp records resulting in updating some intervals.
		• Twin holes are not specifically reported but a small number of drill holes within 5-10m from each other can be observed in 3D space and show generally good correlation.
		• The key adjustment to assay data are:
		  ○ Un-assayed intervals were given a composite value of 0.0034g/t Au and Ag for Pre 2002 drilling.
		  ○ Historic oz/ton has been converted to ppm if no raw lab file in ppm is available.
		  ○ For 2002-2008 drilling from AAL and ALS assay results for gold and silver were reported in parts per million (ppm). For samples that were assayed a second time, the mean of the two samples was used.
		• A regression of silver and gold values for drilling prior to 2002 was implemented by SGS of: Gold = 0.806 * Au_original and Silver = 0.842 * Ag_original to account for overestimation in historic assays outlined in a pulp re-assay investigation by SRK in 2002. Original assay columns are still preserved in the database. Pulp reanalysis of over 5,000 pre-2002 pulps at AAL, with check analysis of ~200 samples at ALS, in 2025 indicated silver underestimation of over 20% in the regression silver via QQ plot and descriptive statistics analysis and resulted in the removal of the ~15% silver regression that was previously applied to the raw assays. The gold regression remains in place.
		
		2024 and 2025
		• Drilling is logged digitally and uploaded into a database along with digital exports from pXRF and gyro devices. Logs and assay results are checked for any discrepancies, if needed, referencing notes and core photos.
		• Assay data below detection limit is reported as a negative from the lab, this has been converted to a number half the detection limit, so no negative values are in the database for future resource work. Eg. -0.05 is changed to 0.025.
		• Assay intervals are converted between feet and metres (x0.3048).
		• 2024 twin drilling of historic drill holes (2003-2008) showed a bias towards higher silver grades in the 2024 drilling (with adequate QAQC), but a similar grade distribution for gold. This may be due to 4 acid digest over 2 acid digest analysis and warrants further investigation. No adjustment has been made as historic data without QAQC appears conservative or lower grade than new data.
		• 2025 twin drilling of historic Pre 2002 diamond core shows good spatial correlation with some variation in grade distribution.

Criteria	JORC Code explanation	Commentary
Location of data points	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control.	• 2024 drilling and locatable historic collars have been surveyed by DGPS for accurate pickup (104 of 222 collars surveyed). • 2025 drilling is located by a handheld GPS, with accuracy to within 2-5m. DGPS pickups of 2025 collars was not available at time of resource estimation. • Downhole survey data appears to have been completed by gyroscopic tool, although this is only specifically stated for the 2002-2008 drilling. 2024 and 2025 drilling uses a north seeking gyro during drilling for down hole surveys for accurate drill string delineation. • The grid system used for locating the historic collar positions of drillholes is NAD27 / UTM Zone 11N (ft). This has been converted to NAD83 UTM Zone 11 (m) for GIS and 3D work using the NCAT conversion tool. • A three-dimensional (3D) DTM surface model representing topography to 0.5m, was supplied and used to validate the location of surface drill holes. This remains sufficient considering the depth of the resource and current drill spacing.
Data spacing and distribution	• Data spacing for reporting of Exploration Results. • Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • Whether sample compositing has been applied.	• Drilling has been completed on an approximately 120x120m grid with localised clustering and some infill drilling to 60m spacing. • Data spacing and distribution is believed to be sufficient to establish the degree of geological and grade continuity appropriate for an Inferred Mineral Resource. • A composite length of 5ft (1.52m) was chosen for resource estimation which reflects the length of majority of drill samples.
Orientation of data in relation to geological structure	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralized structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	• The drilling is predominantly conducted at or close to vertical with an average dip of -85° in historic drilling, -88° in 2024 drill holes and -87.5° in 2025 vertical drill holes. The dip is approximately perpendicular to the flat-lying mineralisation. • The drill orientation is not expected to have introduced any sampling bias. • 2025 angled extensional or infill drillholes appear to represent true width or +95% of it.
Sample security	• The measures taken to ensure sample security.	• Historic samples sent from site to laboratory have no record of security protocols reported but are assumed to follow industry standards. Snowden, 2006 noted that Vistas protocols of sample security were acceptable. • 2024 and 2025 drill samples are prepared on site and collected by the laboratory's transport team or selected couriers. • 2025 metallurgical samples were shipped from site (Nevada) to IMO (Australia) for testing.
Audits or reviews	• The results of any audits or reviews of sampling techniques and data.	• Issues with sample recovery in fractured ground may result in missing sample intervals, and recoveries are recorded on a sample-by-sample basis into the drill logging database. Twin drilling will be compared to historic drilling. • Wet drilling of RC holes is industry standard for deep drilling in Nevada due to ground conditions and is not expected to introduce sample bias. Verification of 2024 and 2025 RC assay results against field blanks show good results. Comparison to twin drilling remains ongoing. • 2025 diamond core sample intervals around core loss to minimise grade spread where core has not been recovered, this may differ from historic core sampling techniques. • Reviews of sampling techniques, data and assays have been undertaken by Newmont in 2001, by Snowden in 2002, 2003, 2006, SRK in 2016, and by SGS in 2022. A 1174 sample pulp re-assay program circa 2002 concluded assays from the Goldbar Lab overestimated gold and silver prompting a grade regression calculation. The 2025 pulp re-assay program of over 5000 Pre 2002 pulps by four acid digest showed consistent under-estimation of silver grades

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>in historic data of around 20%. As a result, the regression calculation on silver has been removed, and only gold remains.
<table>
<tr><th></th><th>SRK</th><th>SGS</th><th>2025</th></tr>
<tr><td>Original Au</td><td>x 0.896 and -0.001</td><td>x 0.806</td><td>x 0.806</td></tr>
<tr><td>Original Ag</td><td>x 0.794 and -0.066</td><td>x 0.842</td><td>Original Ag</td></tr>
</table>
</td></tr>
</table>

Section 2 Reporting of Exploration Results – Maverick Springs Silver Gold Project

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC 2012 Explanation	Comment
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The Maverick Springs property is in northeast Nevada, USA, ~85 km SE of the town of Elko, Nevada. The property currently consists of 767 Maverick, Willow and NMS unpatented lode mining claims registered with the US Department of the Interior Bureau of Land Management ("BLM") with a total area of approximately 60sq km. • The tenements are held in the name of Artemis Exploration Company ("AEC") and Sun Silver. Sun Silver holds a 100% interest in the Maverick Springs Project. • Gold and Silver Net Smelter Royalties (NSR) to tenement owner AEC of 5.9% which include ongoing advance royalty payments, and to Maverix Metals of 1.5% exists. AEC has additional NSR of 2.9% for all other metals. • Archaeological surveys have been undertaken on certain areas of the Project to allow drilling activities. • All claims are in good standing and have been legally validated by a US based lawyer specialising in the field
Exploration done by other parties.	• *Acknowledgment and appraisal of exploration by other parties.*	• Gold exploration at the Project area has been carried out by three previous explorers – Angst, Inc from 1986-1992, Harrison Western Mining L.L.(Harrison) C in 1996, Newmont in 2001, Vista Gold Corp (Vista) and Silver Standard in 2002-2016. • Angst undertook first stage exploration with geochemical surveys, mapping, and drilling 128 drill holes for 39,625m outlining initial mineralisation at the project. • Harrison drilled 2 exploration holes in 1998 for 247m. • Vista advanced the project significantly drilling 54, mostly deep, RC holes over several years until 2006 which equated to ~15,267m. • Silver Standard completed 5 deep RC holes for 1,625m in 2008. • Reviews of the historic exploration show it was carried out to industry standards to produce data sufficient for mineral resource calculations.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• Previous Technical Reports have identified the Maverick Springs mineralisation as a Carlin-type or sediment/carbonate-hosted disseminated silver-gold deposit. However, the 2022 review by SGS is of the opinion that the deposit has more affinity with a low-sulphidation, epithermal Au-Ag deposit. Recent fieldwork notes similarities to a Carbonate Replacement Deposit (CRD). The definition may be in conjecture, but the geological setting remains the same. The mineralisation is hosted in Permian sediments (limestones, dolomites). The sediments have been intruded locally by Cretaceous acidic to intermediate igneous rocks and overlain by Tertiary volcanics, tuffs and sediments and underlain by Paleozoic sediments.

Criteria	JORC 2012 Explanation	Comment
		• Mineralisation in the silty limestones and calcareous clastic sediments is characterised by pervasive decalcification, weak to intense silicification and weak alunitic argillisation alteration, dominated by micron-sized silver and gold with related pyrite, stibnite and arsenic sulphides associated with intense fracturing and brecciation. • The mineralisation has formed a large sub-horizontal gently folded (antiformal) shaped zone with a shallow plunge to the south with the limbs of the arch dipping shallowly to moderately at 10-30° to the east and west from approximately 120m below surface to depths of over 500m below surface. • Horst and Graben features including faults and offsets appear to be present at the Project with the effect on mineralization yet to be fully understood.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* • *easting and northing of the drill hole collar* • *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* • *dip and azimuth of the hole* • *down hole length and interception depth* • *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• Relevant criteria is reported in Appendix A and B of this release. • Multi element assay data is received but only select elements that are material or have relationships have been reported. Reporting all 28 elements is not practical and their exclusion does not detract from the understanding of the report.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Ag and Au metal equivalents have been used. Gold price of $USD 2433/oz and Silver price of $USD 28.5/oz for a ratio of 85 based on average monthly metal pricing for the last 3 years. • Metallurgical recoveries are assumed at 85% for both Gold and Silver from historic test work and therefore negate each other in the equivalent calculations, updated metallurgical studies continue to show similar recovery for each metal. The resource is reported as an AgEq grade where AgEq = Ag+Au*85. • Length weighted assays were calculated from individual assays in metallurgical composites for grade checks.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Drill hole intersections are reported as downhole drill intercepts and generally reflect true widths based on the flat-lying mineralisation and near to vertical drill holes. Long, angled holes often drop dip during drilling and represent true width with undulating mineralisation. Review of drill strings in 3D is used to verify this with any anomalies stated in the report.

Criteria	JORC 2012 Explanation	Comment
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Figures are included in the report. Figures include data from historic holes previously reported and have not materially changed.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All metallurgical sample assay intervals and material metallurgical test results have been reported for gold and silver material to this release.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Historic metallurgical test work from 2002,2004 and 2006 has shown variable recoveries experimenting with different processing scenarios. Maximum recoveries of 97.5% for Ag and 95.8% for Au have been recorded but show variation across material and test parameters (grind size, leach time etc). • Optimized metallurgical test work was recently completed with results reported within the announcement above and includes IBR and cyanide leach tests on two composite samples derived from historic drill material. IBR tests on coarse-crush material achieved 77% Ag and 74% Au average recoveries and cyanide Leach tests (fine grind) achieved 87.25% Ag and 82.15% Au recoveries respectively. • Bulk density measurements have been taken during 2025 drilling via water immersion method of drill core on site. 192 measurements from 7 holes produced average values for Oxide and Transitional material of 2.47, and for Fresh material 2.33g/cm³. The higher density above fresh rock may be due to more iron, intense silicification, and/or mineralisation in samples compared to fresh rock. Further tests are recommended to refine values and further differentiate material. • Shallow anomalous silver and antimony mineralisation has been intercepted in historic drilling realised from the pulp-reassay program. These provide exploration targets for material above the mineralised body subject to the resource estimate. The extent or economic value of this material remains unknown and to be investigated.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Potential exists for additional drilling to test extensions of the mineralisation model, which is open to the north and south along the hinge, and east and west as lateral extensions. Shallow drilling could test theories for up-dip mineralisation. Infill drilling could be used to increase confidence within the current model extents. Additional planned metallurgical test work is stated in the report.