VICTORY METALS

Victory Unveils Major Gallium Resource as By-Product to HREEs

Victory Metals Ltd (**ASX:VTM, Victory** or the **Company**) is pleased to announce a significant enhancement to its Mineral Resource Estimate (**MRE**) at the North Stanmore project, with the inclusion of Gallium Oxide (Ga_2O_3).

This strategic addition further strengthens the Company's diversified critical minerals portfolio and positions Victory as a potential dependable Western supplier of metals currently under tight global supply due to Chinese export restrictions.

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HIGHLIGHTS

- **Victory** has added **4,788 tonnes of Gallium Oxide (Ga_2O_3)** to its updated Mineral Resource Estimate (MRE) at the North Stanmore project, which now stands at **247.5 million dry metric** tonnes at 520 ppm Total Rare Earth Oxide plus Gallium Oxide at 26 ppm (TREOSc_2O_3 + Ga_2O_3) (Inferred and Indicated)
- Gallium oxide has a current market price of approximately AUD $770/kg[1]
- **North Stanmore now includes seven critical metals that are currently subject to Chinese export restrictions**, all of these restricted critical metals have been recovered during testwork in Victory's Mixed Rare Earth Carbonate (MREC). These include:
    - **Heavy Rare Earths (HREEs):** Gadolinium (Gd), Terbium (Tb), Dysprosium (Dy), Lutetium (Lu), Yttrium (Y)
    - **Light Rare Earths (LREEs):** Samarium (Sm)
    - **Strategic By-product:** Gallium (Ga), Scandium (Sc)
- Gallium is a **critical technology metal** used in AI chips, semiconductors, quantum computing, defence systems, LEDs, and solar panels – with global supply tightly controlled, particularly by China
- **Gallium is recovered concurrently with Victory's Mixed Rare Earth Carbonate (MREC) no additional processing required**, making it a **cost-effective by-product**
- Addition of Gallium enhances the value and strategic appeal of Victory's Mixed Rare Earth Carbonate (MREC), although the **Company remains firmly focused on its high ratios of heavy rare earths** as the core revenue drivers
- **Victory is now one of the few companies in Australia with a declared Gallium Oxide Mineral Resource**, further positioning the Company as a globally relevant and potential diversified critical minerals supplier

[1] price https://www.fastmarkets.com/insights/chinas-gallium-export-control-continues-to-squeeze-market-despite-higher-december-exports/?utm_source=chatgpt.com); USD/AUD conversion rate of 0.65 applied

- **Downstream engagement and offtake discussions** are being expanded to reflect this new opportunity, with Gallium now included as a bonus value stream in strategic planning

Victory's CEO and Executive Director Brendan Clark commented:

"The addition of Gallium to the MRE is an incredible bonus, not a dependency. Our focus remains on developing a world class heavy rare earth project, but the ability to recover Gallium concurrently through our recovery process without additional complexity significantly enhances the value proposition.

Gallium is a strategic technology metal with growing global demand, and its inclusion as a by-product positions Victory as an even more attractive partner for downstream and offtake discussions."

April 2025 MRE update

On 16 January 2025, Victory announced an updated Mineral Resource Estimate (MRE) for its North Stanmore Heavy Rare Earth Elements (HREE) Project in Western Australia (January 2025 MRE). The January 2025 MRE stood at 247.5 million dry metric tonnes at 493 ppm Total Rare Earth Oxide plus Scandium Oxide (TREO + Sc_2O_3) and Ga_2O_3 @ 26ppm, (Inferred and Indicated), using an economic cut-off grade of 330ppm TREO plus Scandium Oxide, inclusive of high-grade domain (≥600 ppm TREO cut-off) of 53 million tonnes @ 1,012 ppm TREO plus Sc_2O_3 (Inferred and Indicated) (Figure 2).[2]

Victory subsequently commissioned further Mixed Rare Earth Carbonate (MREC) production activities to optimise recovery conditions for Gallium Oxide (Ga_2O_3) while maintaining the heavy rare earth element (HREE) distribution in the final MREC product.

On 26 March 2025, Victory announced the successful production of Gallium (Ga) in its final MREC product from North Stanmore. Gallium confirmed in final MREC product at 258 g/t Ga_2O_3, successfully recovered using low-CAPEX leaching process and recovery occurring concurrently with REEs requiring no additional processing stages.[3]

Victory then commissioned MEC Pty Ltd (MEC) in April of 2025 to update the January 2025 MRE to include Gallium oxide given the recent MREC Gallium recoveries.

Updated April MRE Information

The April 2025 MRE update was estimated within the boundaries of ten tenements; E20/0544, E20/871, E20/971, E20/1016, E20/2468, E20/2469, P20/0543, P20/2007, P20/2153, and P20/2403, with all tenure held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory (Figure 1).

[2] Refer to ASX Announcement of 16 January 2025 for further details.
[3] Refer to ASX Announcement of 26 March 2025 for further details.

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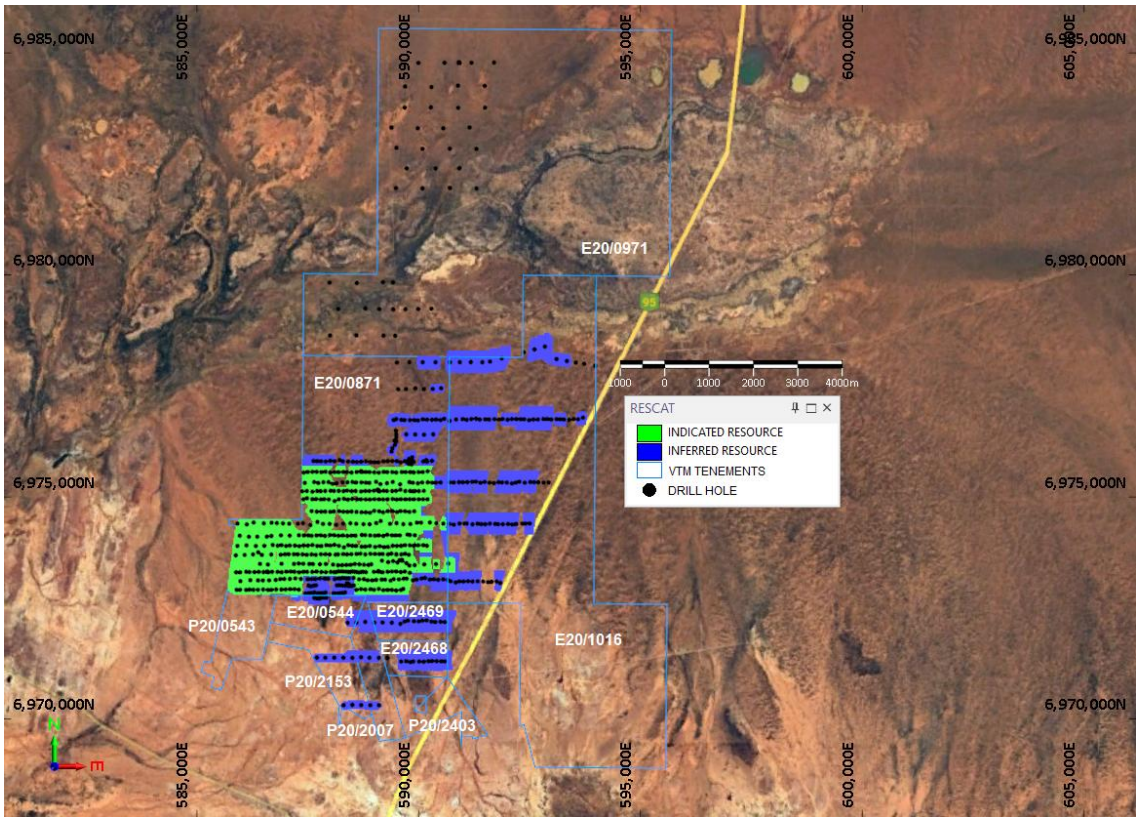

Figure 1: *North Stanmore MRE by ResCat*

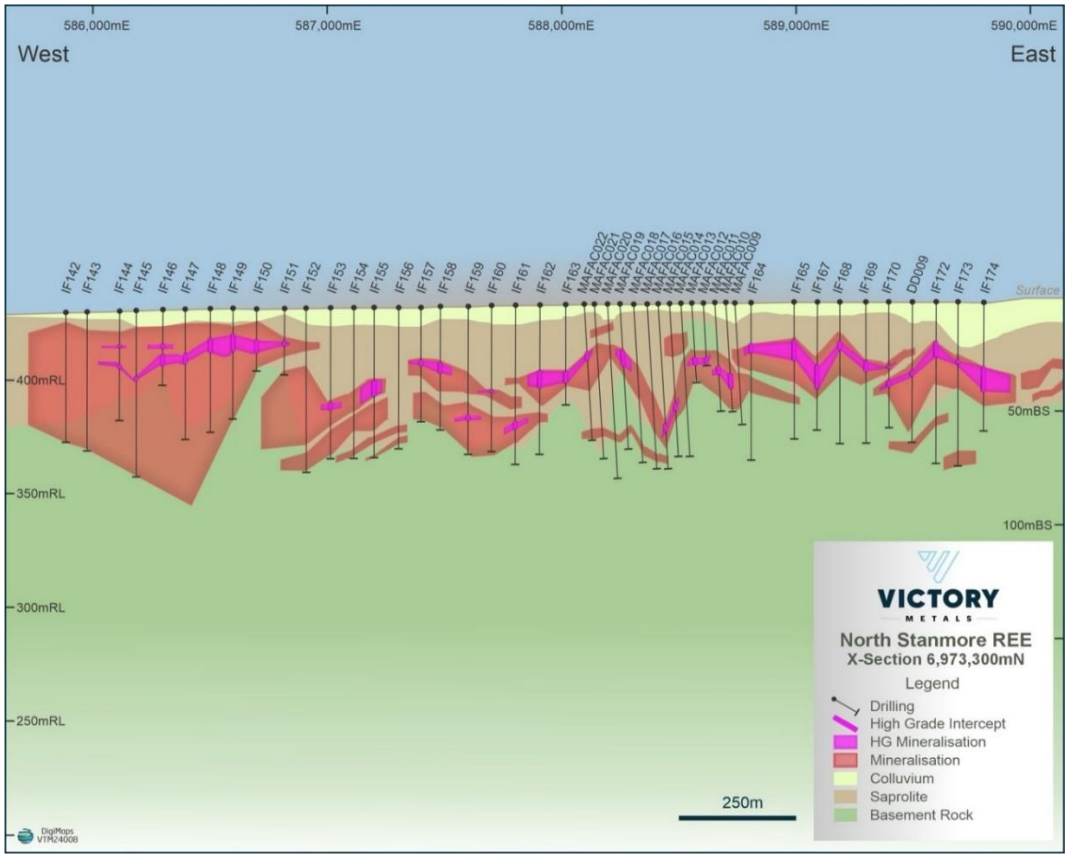

Figure 2: *Cross section 6,973,900mN, looking north, 5x vertical exaggeration and showing the High-Grade intercept.*

A site visit was conducted on May 30, 2024, by MEC Manager of Resources, Mr Dean O'Keefe and MEC Resource Geologist, Mr Issam Digais, accompanied by Victory Metals personnel including Mr Savvas Hagiantoniou, Exploration Site Supervisor. Dean O'Keefe is an MEC Competent Person for the North Stanmore MRE. During the site visit the general layout of the area and project location was checked. MEC also conducted a check survey of drillhole collar locations, the surveyed locations were confirmed as being in close proximity to the planned drillhole locations, all within 3m. No production has occurred at the North Stanmore site.

The North Stanmore MRE occurs in regolith above an alkaline intrusion. Despite its magnetic signature, the North Stanmore intrusion had not been recognised previously on regional geological maps. Petrological data for samples of diamond core confirm its alkaline character and indicate that the intrusion is post-tectonic and hence, post-Archean in age.

The North Stanmore Intrusion is a large (approximately 16km by 5km) differentiated ultramafic to felsic intrusion. Lithologies identified in thin section include kaersutite and carbonate-bearing peridotite, orthopyroxenite, clinopyroxenite, leuco- and leuco-gabbro (ijolite), diorite, monzonite and syenite. Some regolith samples are strongly LREE enriched indicating that the intrusion also contains carbonatite. However, the uniformly high HREO/TREO of the regolith (of approximately 34% to 38%) indicates that carbonatite represents a subordinate phase in the intrusion.

The North Stanmore Intrusion is interpreted to be associated with an early Proterozoic plume track that was responsible for alkaline magmatism extending in a broad belt from Mt Weld carbonatite near Laverton through Leonora to Cue.

The rare earth element mineralisation occurs in a relatively flat-laying saprolite-rich clay horizon beneath a veneer of unconsolidated colluvium that ranges in thickness from 0–36m. The uniformity of Nb/Ta ratios (Nb/Ta 16±4) in the regolith above the North Stanmore Intrusion indicates that the regolith developed in situ. Importantly, studies have shown that Nb/Ta ratio of regolith over carbonatites and other alkaline intrusions closely resembles the Nb/Ta ratio of their source plume generated lithologies.

REEs are adsorbed onto kaolinite or form secondary REE phosphates, rhabdophane (after monazite), churchite (after xenotime), and florencite. QEMSCAN mineralogical studies show that the REEs are mainly hosted by <20µm particles.

Scandium oxide (Sc_2O_3) is enriched throughout the regolith profile due to the breakdown of pyroxene in the North Stanmore source lithologies. Scandium oxide is generally considered to behave differently to the REEs, which are adsorbed as outer-sphere complexes on clay surfaces, found in Al(OH)2SiO sites, or occur as hydrated REE bearing phosphates. However, Sc3+ behaves like the transition metals (Ni2+ , Co2+, Cu2+) and, due to its smaller ionic radius, it adsorbs onto vacancy sites in clay lattices or attaches to the surface of Mn oxides.

Scandium is a highly valuable critical element occurring in the same Group of the Periodic Table (Gp. 3B) as the lanthanides. It occurs predominantly in HREE bearing ultramafic and mafic igneous rocks like the North Stanmore Intrusion. By contrast, felsic alkaline rocks and granitoids are more LREE enriched and contain negligible amounts of Scandium. The chemical properties of Scandium are distinct from the other REO's and Scandium has recently been recognised to have superconducting properties. Scandium has been deemed a critical mineral due to current Chinese and Russian control of the supply chain.

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Yttrium is classified as a REO because of its similar ionic radius to the lanthanides, and similar chemical properties to the HREEs.

A geological cut-off grade of 150ppm TREO + Sc_2O_3 was used to separate mineralised material (MIN) from weakly mineralised material (WMM). A high-grade mineralisation (HGMIN) domain was additionally modelled above a geological cut-off grade of 600ppm TREO + Sc_2O_3.

Logging was completed for 90% of the sample intervals and used to produce surfaces to delineate the colluvium, saprolite, and basement.

Drilling at North Stanmore to support the April 2025 MRE includes seven hundred and fifty-five (755) drillholes for 42,118.9m, inclusive of 694 Air-core (AC) drillholes for 38,188m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory from 2022 to 2024. The drillhole spacing at North Stanmore (MRE area) ranges from 50m x 50m to 250m x 100m.

Eleven percussion (air core and RC) drillholes have been twinned with diamond drilling (DD001 to DD011). Samples were submitted to the laboratory for analysis only where the initial screening by handheld XRF generated a mineralised value, whereas the diamond drilling was sampled and assayed along the entire length of the drillhole. There is good spatial comparison between the percussion and diamond assays for the twin drilling. The use of the handheld XRF tool is a reasonable indicator of zones of mineralisation within the percussion holes.

Local validation was completed by comparing the composite grades used to estimate the block values against the estimated block values. There was close correlation between composite assays and estimated block grades, with some small differences resulting from the smoothing effect of ordinary kriging. Min/max checks were utilised to ensure all blocks were populated. OBM validation functions were used to check for overlapping blocks, there were no incidence of overlapping blocks.

The Resource has been classified as Indicated and Inferred categories, in accordance with the 2012 Australasian Code for Reporting of Mineral Resources and Ore Reserves (JORC Code). Unclassified material based on sparse exploration data has not been reported as part of the Mineral Resource. A range of criteria has been considered in determining this classification including:

- Geological continuity
- Data quality
- Drill hole spacing

An Indicated Mineral Resource classification was based on drillhole spacing (250m x 100m, closing to 50m x 50m), acceptable underlying QAQC, and an RTK/DGPS survey of drillhole collars. An Inferred Mineral Resource classification was based on a drill spacing of ~500m x 100m. Approximately 71% by tonnage of the April 2025 MRE is classified as Indicated Mineral Resources and approximately 29% is classified as Inferred Mineral Resources.

Three stages of metallurgical test work have been completed for the North Stanmore Project, focusing on beneficiation, and leach test work to establish potential recoveries and processing options.

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Core Resources (**Core**) located in Brisbane completed the third stage of test work including beneficiation test work in March of 2024 and reported that the REE feed grade increased by 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material .

The leach test work program involved diagnostic metallurgical testing on a composite blend of the beneficiated samples with a head grade of 1,283 ppm TREO. This was sourced from 23 samples and 13 drillholes from North Stanmore. The initial atmospheric leach test work program was trialled at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREE").

Scandium oxide (Sc_2O_3) recoveries of 50% had previously been achieved, with optimisation work occurring in parallel. These assays were conducted by Australian Laboratory Services, Brisbane. The objective of the diagnostic test work was to recover REE and Scandium oxide from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).

The April 2025 MRE includes a Mineral Resource estimate for Gallium oxide (Ga_2O_3) occurring within the TREO + Sc_2O_3 mineralisation envelope, as Gallium oxide would be a byproduct of the REE recovery. The Gallium oxide estimate used the January 2025 dataset and interpretation and is reported as part of the April 2025 MRE. The grade distribution for Ga_2O_3 (ppm) associated with the TREO mineralisation is shown in Figure 5. The crustal abundance of Gallium is similar to lead (15ppm) but is weakly dispersed and rarely found in concentrations >1,000ppm (Henderson, 1982). For the North Stanmore deposit the Gallium oxide (Ga_2O_3) mineralisation has an enrichment factor of 1.25 compared to the average crustal concentration and proven metallurgical recoveries in the MREC.[4]

MEC deems that there are reasonable prospects for eventual economic extraction using open pit mining on the following basis:

- The North Stanmore Mineral Resources occur close to surface and will be amenable to opencut mining to commence production. Mineralisation that occurs at depth with limited drilling support has been excluded from the stated Mineral Resource,
- Metallurgical testwork has returned favourable process recovery results,
- The North Stanmore project is located approximately 6km from Cue township and ~420km from Geraldton Port via the Great Northern Highway, being one of West Australia's major arterial road networks.

Table 1: North Stanmore April 2025 MRE (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREO (ppm)	HREO (ppm)	LREO (ppm)	HREO/TREO (%)	Sc_2O_3 (ppm)	Ga_2O_3 (ppm)
INDICATED	176,500,000	477	181	296	38	26	26
INFERRED	70,900,000	533	164	369	31	28	26
TOTAL	**247,500,000**	**493**	**176**	**317**	**36**	**27**	**26**

Numbers are rounded to reflect they are an estimate.
Numbers may not sum due to rounding.

[4] Refer VTM ASX release dated 26 March 2025: *Gallium Produced in Final MREC Product*

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The sensitivity of the Mineral Resource estimate to the reporting cut-off grade is shown in Figure 3.

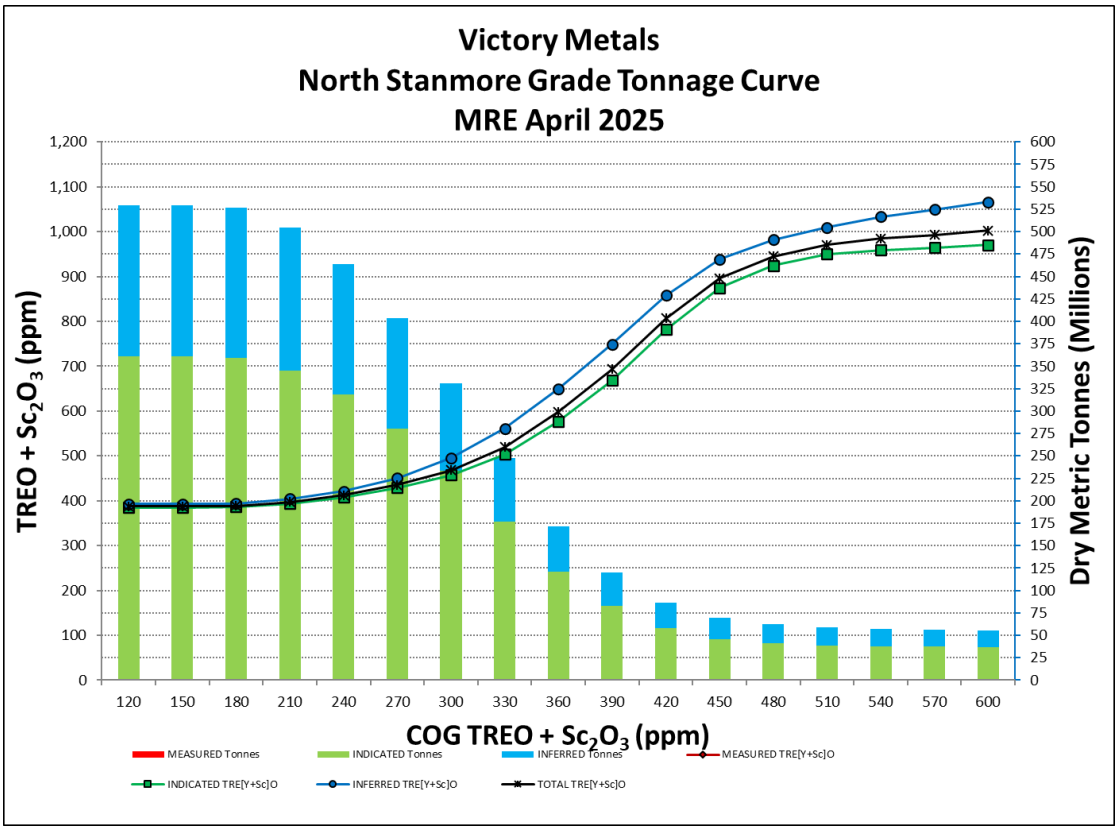

Figure 3: *Grade tonnage curve for the North Stanmore TREO + Sc_2O_3 MRE (Indicated and Inferred)*

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Table 2 shows the HREO within the HGMIN domain by classification, and Table 3 shows the HREO within the MIN domain by classification.

Table 2: North Stanmore April 2025 MRE HREO within the HGMIN domain (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREO + Sc_2O_3 (ppm)	TREO (ppm)	HREO (ppm)	Eu_2O_3 (ppm)	Gd_2O_3 (ppm)	Tb_4O_7 (ppm)	Dy_2O_3 (ppm)	Ho_2O_3 (ppm)	Er_2O_3 (ppm)	Tm_2O_3 (ppm)	Yb_2O_3 (ppm)	Lu_2O_3 (ppm)	Y_2O_3 (ppm)
INDICATED	35,400,000	972	941	318	7.5	30.5	5.0	30.9	6.4	19.1	2.7	17.7	2.6	196
INFERRED	16,500,000	1,099	1,072	354	8.6	33.7	5.5	33.6	7.0	20.8	3.0	18.8	2.7	220
TOTAL	**51,900,000**	**1,012**	**982**	**329**	**7.9**	**31.5**	**5.1**	**31.7**	**6.6**	**19.7**	**2.8**	**18.1**	**2.7**	**203**

Numbers are rounded to reflect they are an estimate. Numbers may not sum due to rounding.

Table 3: North Stanmore April 2025 MRE HRE[Y]O within the MIN domain (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREO + Sc_2O_3 (ppm)	TREO (ppm)	HREO (ppm)	Eu_2O_3 (ppm)	Gd_2O_3 (ppm)	Tb_4O_7 (ppm)	Dy_2O_3 (ppm)	Ho_2O_3 (ppm)	Er_2O_3 (ppm)	Tm_2O_3 (ppm)	Yb_2O_3 (ppm)	Lu_2O_3 (ppm)	Y_2O_3 (ppm)
INDICATED	141,200,000	386	361	146	2.4	12.0	2.1	13.6	3.0	9.2	1.4	9.2	1.4	92
INFERRED	54,500,000	399	370	106	2.6	10.4	1.7	10.1	2.1	6.2	0.9	5.8	0.9	65
TOTAL	**195,700,000**	**390**	**364**	**135**	**2.5**	**11.5**	**2.0**	**12.6**	**2.7**	**8.4**	**1.2**	**8.3**	**1.2**	**85**

Numbers are rounded to reflect they are an estimate. Numbers may not sum due to rounding.

The economic cut-off grade for the April 2025 MEC MRE (Table 1) was ≥330ppm TREO + Sc_2O_3. This cut-off grade was selected based on the evaluation of other like regolith hosted rare earth Mineral Resources.

The MIN domain grade and tonnage is exclusive of the HG grade and tonnage (Table 3).

Table 4 shows the LREO by domain and classification above 330ppm TREO + Sc_2O_3.

Table 5 shows base metals, gallium, and hafnium grades above 330ppm TREO + Sc_2O_3.

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Table 4: North Stanmore April 2025 MRE LREO Grades by Domain and Classification (≥330ppm TREO + Sc_2O_3 cut-off grade)

DOMAIN	CLASSIFICATION	TONNES (t)	TREO+Sc_2O_3 (ppm)	LREO (ppm)	La_2O_3 (ppm)	CeO_2 (ppm)	Pr_6O_{11} (ppm)	Nd_2O_3 (ppm)	Sm_2O_3 (ppm)
HGMIN	INDICATED	35,400,000	972	623	144.8	270.2	36.0	141.0	30.5
HGMIN	INFERRED	16,500,000	1,099	718	182.8	293.8	43.0	163.9	34.1
HGMIN	TOTAL	**51,900,000**	**1,012**	**653**	**156.9**	**277.7**	**38.3**	**148.3**	**31.6**
MIN	INDICATED	141,200,000	386	215	48.7	96.0	11.9	47.2	11.0
MIN	INFERRED	54,500,000	399	264	63.9	121.2	14.4	53.8	10.9
MIN	TOTAL	**195,700,000**	**390**	**229**	**52.9**	**103.1**	**12.6**	**49.1**	**10.9**
Total	TOTAL	**247,500,000**	**520**	**317**	**74.7**	**139.6**	**18.0**	**69.8**	**15.3**

Numbers are rounded to reflect they are an estimate.
Numbers may not sum due to rounding.

Table 5: North Stanmore April 2025 MRE Ni, Co, Cu, Hf, Ga_2O_3 (≥330ppm TREO + Sc_2O_3 cut-off grade)

DOMAIN	CLASSIFICATION	Tonnes (t)	Ni (ppm)	Co (ppm)	Cu (ppm)	Hf (ppm)	Ga_2O_3 (ppm)
HGMIN	INDICATED	35,400,000	36	29	43	6	26
HGMIN	INFERRED	16,500,000	44	26	55	5	26
HGMIN	TOTAL	**51,900,000**	**38**	**28**	**47**	**6**	**26**
MIN	INDICATED	141,200,000	23	14	25	7	26
MIN	INFERRED	54,500,000	45	21	47	5	25
MIN	TOTAL	**195,700,000**	**29**	**16**	**31**	**6**	**26**
Total	TOTAL	**247,500,000**	**31**	**19**	**34**	**6**	**26**

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MRE Proportions Pie Charts

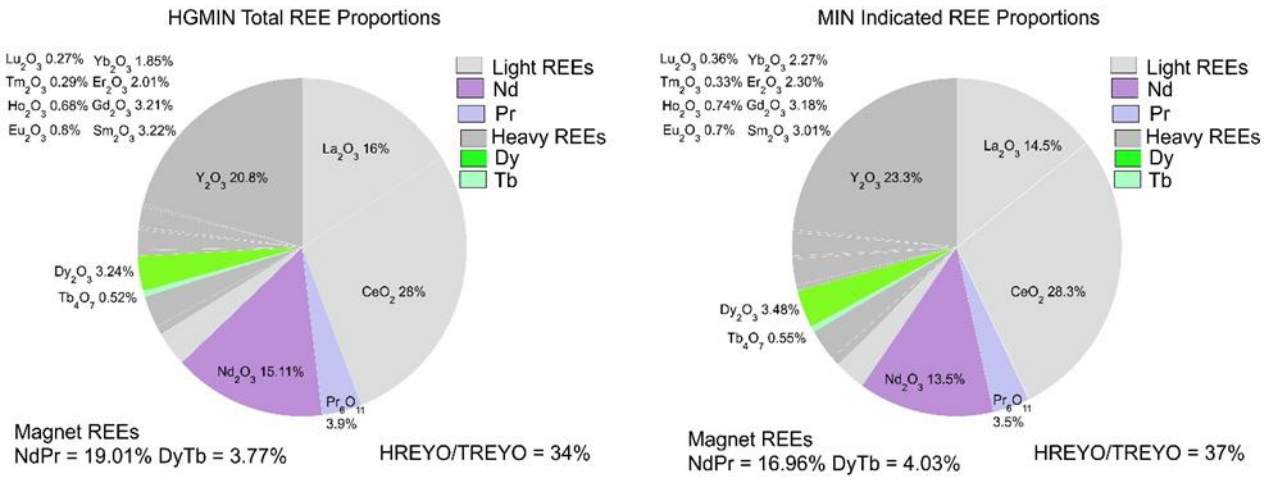

Figure 4: *North Stanmore April 2025 updated MRE composition by percentage in 52.8Mt and 195.7Mt resource domains*

The high HREYO/TREYO ratios shown in Figure indicates that the North Stanmore Mineral Resource contains a significant percentage of the rare, and valuable, HREE's Dysprosium (Dy) and Terbium (Tb).

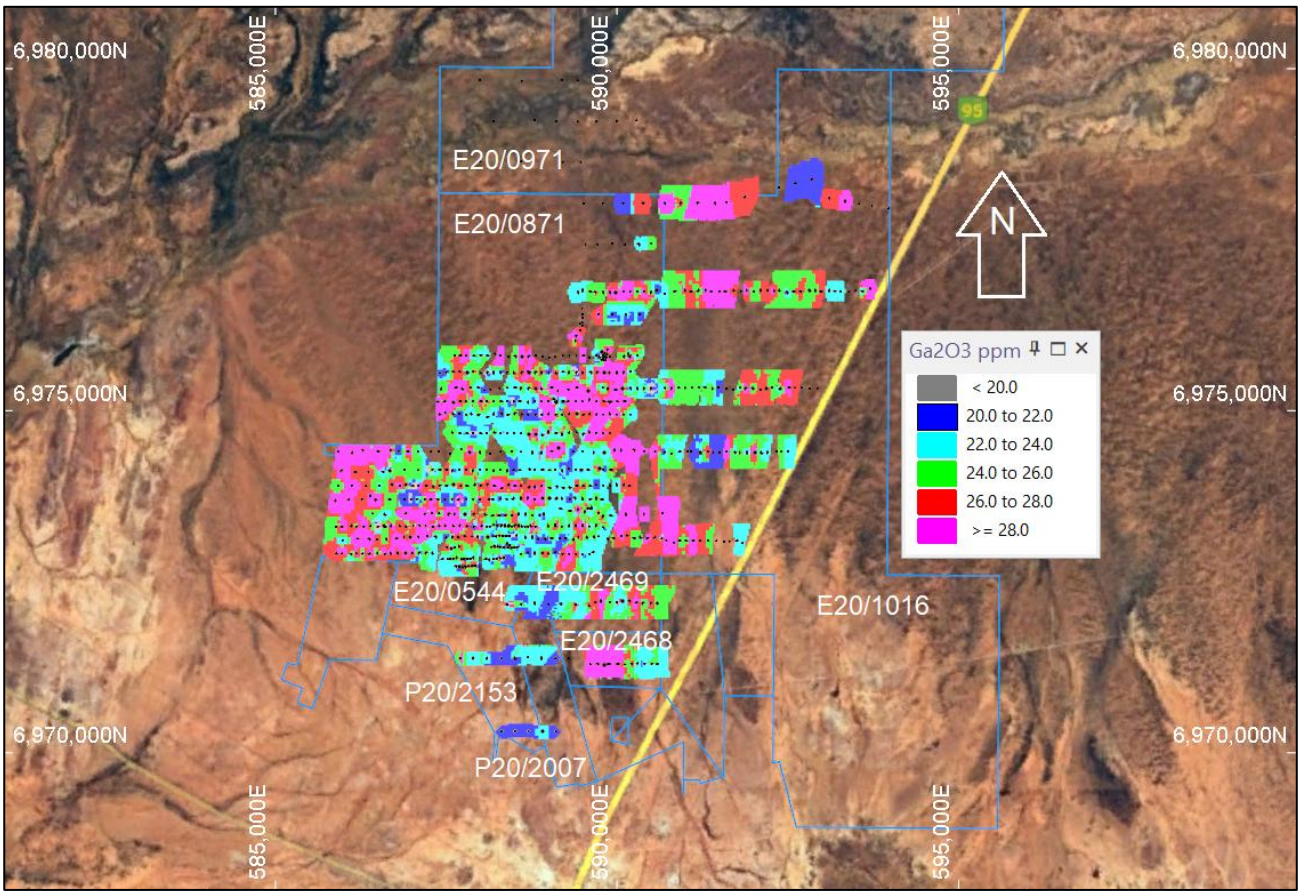

Figure 5: MRE Gallium oxide grade distribution at North Stanmore

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Regional Geology

Victory's tenements lie north of Cue, within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgaranga greenstone belts, and the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late-stage faults. The greenstone belts are intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions. Two large Archaean gabbroic intrusions occur south of Cue. These are the Dalgaranga-Mount Farmer gabbroid complex in the southwest, and the layered Windimurra gabbroic complex in the southeast.

Project Geology

Victory's REE, Sc and Ga discovery occurs in regolith above the North Stanmore alkaline intrusion, discovered north of Cue. Despite its magnetic signature, the North Stanmore intrusion had not been recognised previously on regional geological maps. Petrological data[5] for samples of diamond core indicate that the intrusion is post-tectonic and hence post-Archean in age.

The North Stanmore Intrusion is a large (approximately 16 km by 5 km) differentiated ultramafic to felsic intrusion. Lithologies identified in thin section include kaersutite and carbonate-bearing peridotite, orthopyroxenite, clinopyroxenite, leuco- and leuco-gabbro, ijolite, diorite, monzonite and syenite. Some regolith samples are strongly LREE enriched indicating that the intrusion also contains carbonatite. However, the uniformly high HREO/TREO of the regolith (of approximately 34% to 38%) indicates that carbonatite represents a subordinate phase in the intrusion.

The North Stanmore Intrusion is interpreted to be associated with an early Proterozoic plume track that was responsible for alkaline magmatism extending in a broad belt from Mt Weld carbonatite near Laverton through Leonora to Cue[6].

Deposit Type

The rare earth element mineralisation occurs in a relatively flat-laying saprolite-rich clay horizon beneath a veneer of unconsolidated colluvium that ranges in thickness from 0m to 36m. The uniformity of Nb/Ta ratios (Nb/Ta 16±4) in the regolith above the North Stanmore Intrusion indicates that the regolith developed *in situ.* Importantly, studies have shown that Nb/Ta ratio of regolith over carbonatites and other alkaline intrusions closely resembles the Nb/Ta ratio of their source plume generated lithologies[7].

Mineralised REE saprolite horizons above the North Stanmore Intrusion occur at depths between 12m and 77m. Ce/Ce* tracks regolith oxidation, and the upper parts of regolith enrichment zones have Ce/Ce* >1 reflecting gain of mobile Ce^{4+}, while the lower parts of enrichment zones have Ce/Ce* <1. Leachable clay REE deposits all have Ce/Ce* <1. The Ce/Ce* of the June 2024 updated MRE in the Indicated category is 0.86 (Tables 1 to 4).

[5] Refer VTM ASX release dated 10 August 2022, *Major Alkaline Igneous Complex Discovered*
[6] Fiorentini et al., (2020) Nature Sci. Repts. 10:19729
[7] Cornelius et al, (2005) Geochemistry: Exploration, Environment, Analysis, Vol. 5, 291–310; Zhukova et al., (2021) Ore Geology Reviews 139, 104539

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REEs are complexed with carbonate ions [CO_3^{2-}] and bicarbonate ions [HCO_3^-] or occur as REE^{3+} ions in soil as groundwater migrates downwards during tropical weathering. Based on Ce/Ce*systematics[8] and TREO concentrations, there appear to be four zones of REE enrichment at North Stanmore. These are 15m to 25m, 28m to 37m, 41m to 46m and a deeper zone between 53m and 77m. The regolith is complex and importantly some cores exhibit two zones of REE enrichment.

REEs are adsorbed onto kaolinite or form secondary REE phosphates, rhabdophane (after monazite), churchite (after xenotime), and florencite. QEMSCAN mineralogical studies show that the REEs are mainly hosted by <20-µm particles.

Scandium is enriched throughout the regolith profile due to the breakdown of pyroxene in the North Stanmore source lithologies. Sc is generally considered to behave differently to the REEs, which are adsorbed as outer-sphere complexes on clay surfaces, found in $Al(OH)_2SiO$ sites, or occur as hydrated REE bearing phosphates. However, Sc^{3+} behaves like the transition metals (Ni^{2+}, Co^{2+}, Cu^{2+}) and, due to its smaller ionic radius, it adsorbs onto vacancy sites in clay lattices or attaches to the surface of Mn oxides[9]. Sc is enriched throughout the regolith profile.

REO and Gallium Terminology

Yttrium is included as a REE because of its similar ionic radius to the lanthanides and has similar chemical properties to the HREEs [holmium (Ho) and erbium (Er)].

Scandium, a highly valuable critical element occurs in the same Group of the Periodic Table (Gp. 3) as the lanthanides. It occurs predominantly in HREE bearing ultramafic and mafic igneous like the North Stanmore Intrusion. By contrast, felsic alkaline rocks and granitoids are more LREE enriched and contain negligible amounts of Sc contents. The chemical properties of Sc are distinct from the other REEs, and Sc has recently been recognised to have superconducting properties. Sc has been deemed a critical mineral due to current Chinese and Russian control of the supply chain.

Gallium is a chemical element with the symbol Ga and atomic number 31. It is a soft, silvery metal that is solid at room temperature but melts just above it, making it unique among metals. Gallium is primarily used in the production of semiconductors, particularly in devices like light-emitting diodes (LEDs) and solar panels. It forms important compounds such as gallium arsenide (GaAs), which is widely used in electronics due to its excellent semiconductor properties. Additionally, gallium is known for its ability to form binary compounds with elements like phosphorus and arsenic, which are crucial in various technological applications.

Analytical data was determined by ALS using the ME-MS81 technique of fusion digestion followed by ICPMS analysis. Results were returned in elemental form and were converted to oxides.

TREO (Total Rare Earth Oxides), LREO (Light Rare Earth Oxides), HREO (Heavy Rare Earth Oxides), MREO (Magnet Rare Earth Oxides), and the ratio of HREO/TREO were calculated as follows:

- **TREO** is the sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O_3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3,. This follows the protocol recommended by the International Union of Pure and Applied Chemistry.[10] Yttrium and Scandium are included as

[8] Ce/Ce* = (2*(Ce_N)/(La_N+Pr_N)), where Ce_N, La_N and Pr_N are chondrite normalised values; La_N = La concentration /0.237, Ce_N =Ce concentration /0.613 and Pr_N =Pr concentration/0.0928; Ce/Ce* ratios >1 reflect the gain of Ce^{4+} at shallower regolith depths while Ce/Ce* ratios <1 reflect the loss of mobile Ce^{4+} from deeper parts of weathering profiles that contain Ce^{3+}.
[9] Zhang et al., (2024) Am. Mineralogist
[8] Williams Jones and Vasyukova (2018) Economic Geology

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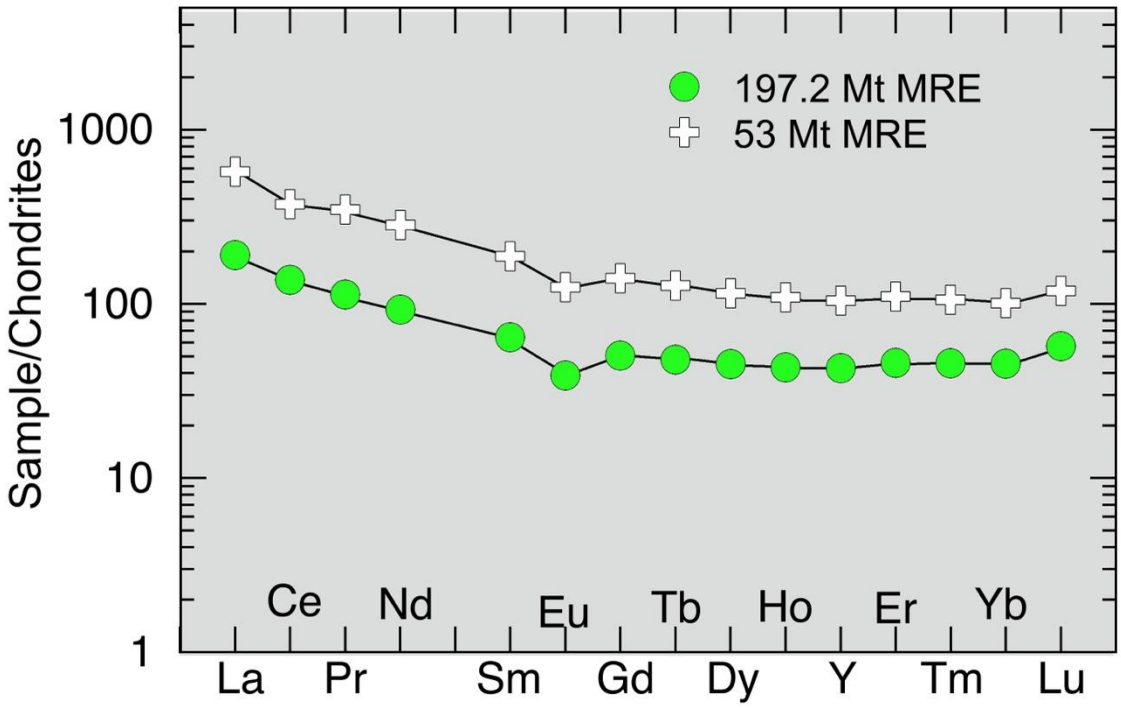
they share Group IIIA properties in the Periodic Table with the lanthanides. Importantly, yttrium exhibits similar geochemical properties to the HREOs.

- **TREOS** is the sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O_3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, Y_2O_3, and Sc_2O_3.
- **HREO** is the sum of Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3.
- **LREO** is the sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, and Sm_2O_3.
- **MREO** (Magnet Rare Earth Oxides) are the rare earths used in the production of magnets predominantly, Nd_2O_3, Pr_6O_{11} (**NdPr**) and Dy_2O_3, Tb_4O_7 (**DyTb**).
- HREO/TREOS is the ratio of the sum of Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3/sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, Y_2O_3, and Sc_2O_3.
- The quality of the assays is shown in Figure 6 by the smooth inter-element profiles in chondrite normalised plots for the 197.2 Mt and 53 Mt resource compositions.



Sampling and sub-sampling techniques

Air-core drilling samples were collected as 1m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite. Each sample was then split using a 3-tier (87.5% - 12.5%) splitter and the sample split was placed into calico sample bags for transport to Perth.

Sample weights and recoveries were recorded on site and weighed 1.5 - 2.5kg depending on the sample recovery from the drill hole. The mean bulk sample weight was 8.45kg.

A handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REO (Rare earth element) geochemistry (La, Ce, Pr, Nd, and Y) from the 1m sample piles. pXRF reading times were 45

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secs over 3 cycles for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their integrity was checked using Certified REO -bearing geochemical standards. The handheld pXRF is used as a guide to the relative presence or absence of certain elements, including REOs vectors (La, Ce, Pr, Nd, and Y) to help direct the sampling program. Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. REO anomalism thresholds are determined by VTM technical lead based on historical data analysis

Victory attended North Stanmore to collect the green sample bag which was transported by Victory to Victory's secure warehouse in Perth.

Measures taken to ensure sample representivity included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.

Drilling techniques

Drilling at North Stanmore to support the April 2025 MRE includes 755 drill holes for 42,118.9m, inclusive of 694 Air-core (AC) drillholes for 38,188m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory from 2022 to 2024.

The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m.

Mineral Resource Classification

A range of criteria has been considered in determining this classification including:

- Geological continuity and lode geometry
- Data quality
- Drill hole spacing

An Indicated Mineral Resource classification was based on drillhole spacing (250m x 100m, closing to 50m x 50m), acceptable underlying QAQC, and an RTK/DGPS survey of drillhole collars. An Inferred Mineral Resource classification was based on a drill spacing of ~500m x 100m.

Approximately 71% by tonnage of the April 2025 MRE is classified as Indicated Mineral Resources and approximately 29% by tonnage is classified as Inferred Mineral Resources.

Sample analysis method

Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory. The assay methods used include:

- ME-4ACD81: Four acid digestion followed by ICP-AES measurement
- ME-MS81: Lithium borate fusion followed by acid dissolution and ICP-AES measurement
- ME-ICP06: Fusion decomposition followed by ICP-AES measurement

REOs were all analysed by ME-MS81 (four acid digestion followed by ICP-AES measurement) with results returned in their elemental form. Elements were then converted to oxides using the appropriate stoichiometric conversion factors.

Base metals are assayed by ME-ICP06: Fusion decomposition.

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Non-ferrous metals are assayed by ME-4ACD81: Four acid digestion.

Using a riffle splitter, 1m composite samples were collected from the individual sample bags.

Quality control of the assaying comprised the collection of a bulk repeat sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples. The repeat sample was collected by passing the bulk reject obtained from the first split stage through the riffle splitter once more. The repeat sample is not a duplicate.

Validation

All ore block models were validated globally and locally. Global validation compared the wireframe volume and grade with the ore block model volume and grade, at a zero-cut-off grade. The global volume comparison between the wireframes and the sub celled ore block models was close. The global grade comparisons of grade within the low grade and high-grade wireframes compared to their respective modelled grades is within 5%, with small differences occurring due to the clustering of grades within the wireframes. Local validation was completed by comparing the composite grades used to estimate the block values against the estimated block values. There was close correlation between composite assays and estimated block grades, with some small differences resulting from the smoothing effect of ordinary kriging. Min/max checks were utilised to ensure all blocks were populated. OBM validation functions were used to check for overlapping blocks, there were no incidence of overlapping blocks.

Cut-off grade

The economic cut-off grade for the April 2025 MEC MRE was ≥330ppm TREO +Sc_2O_3. This cut-off grade was selected based on the evaluation of other like regolith hosted rare earth Mineral Resources.

Metallurgical Testwork

Four stages of metallurgical test work have been completed on the North Stanmore Project, focusing on beneficiation, and leach test work to establish potential recoveries and processing options.

Core Resources (**Core**) located in Brisbane completed the third stage of test work including beneficiation test work in March of 2024 and reported that the REE feed grade increased 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material[11]

The leach test work program involved diagnostic metallurgical testing on a composite blend of the beneficiated samples with a head grade of 1,283 ppm TREO. This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trialed at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) as well as the less valuable light rare earth elements Pr (94%), Nd (94%), with a combined recovery of 93% MREO.

Scandium recoveries of 50% had previously been achieved, with optimisation work occurring in parallel. These assays were conducted by Australian Laboratory Services Brisbane. The objective of

Williams Jones and Vasyukova (2018) Economic Geology
ore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries Refer VTM ASX release dated 14 May 2024, North Stanmore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries

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the diagnostic test work was to recover REE and Sc from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).

The most recent metallurgical test work, conducted by Core, utilised a composite sample derived from 12 individual samples across 7 drill holes distributed throughout the North Stanmore project area. This composite had an average Total Rare Earth Oxide (TREO) grade of 873ppm, with a Heavy Rare Earth Oxide (HREO) to TREO ratio of 29%.

The leach test was performed over a 4-hour duration at 90°C. The results demonstrated impressive metallurgical recoveries across a wide range of elements: La: 91%, Ce: 94%, Pr: 97%, Nd: 97%, Sm: 98%, Eu: 97%, Gd: 96%, Tb: 94%, Dy: 87%, Ho: 77%, Er: 82%, Tm: 76%, Yb: 77%, Lu: 71%, Y: 72%, Ga: 34%.

Reasonable Prospects for Eventual Economic Extraction

Clause 20 of the JORC (2012) Code requires that all reported Mineral Resources have reasonable prospects for eventual economic extraction. MEC has confirmed the reasonable prospects for eventual economic extraction in relation to the North Stanmore Project based on the following:

- **Shallow Mineralisation:** North Stanmore Mineral Resources occur close to surface and are believed to be amenable to an opencut mining operation.
- **Favourable Metallurgical Results:** Extensive metallurgical testwork has returned very favourable processing recoveries.
- **Proximity to Cue:** The North Stanmore Project is situated approximately 6km from the Cue township
- **Excellent connectivity:** Via the Great Northern Highway, a major arterial road linking the project to Geraldton Port (420 km).

This announcement has been authorised by the Board of Victory Metals Limited.

For further information please contact:

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Victory Metals Limited

Victory is dedicated to the exploration and development of its flagship North Stanmore Heavy Rare Earth Elements (HREE), Scandium, Gallium and Hafnium Project located in the Cue Region of Western Australia. The Company is committed to advancing this world-class project to unlock its significant potential.

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Competent Person Statement

Competent Person Statement – Dean O'Keefe

The information in this announcement that relates to the Mineral Resource estimate is derived from, and fairly represents information compiled by Mr Dean O'Keefe, a Fellow of the Australasian Institute of Mining and Metallurgy (FAusIMM #112948). Mr O'Keefe is Competent Person for this style of mineralisation and is a consultant to Victory Metals Limited. Mr O'Keefe is a full time employee of MEC Pty Ltd, an independent mining and exploration consultancy. Mr O'Keefe has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which they are undertaking to qualify as Competent Person as defined in the 2012 edition of the Australasian Code for the Reporting of Exploration Results, Mineral Resources, and Ore Reserves (JORC Code). The Competent Persons is not aware of any new information or omission of data that may materially affect the stated Mineral Resource estimate. Mr O'Keefe consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

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APPENDIX 4: Drillhole Collar Coordinates

HoleID	East	North	RL	Depth	Grid	Azimuth	Dip	HoleType	DateDrilled
AC0001	588308.8	6970311.9	446.9	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0002	588504.4	6970319.8	445.5	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0003	588702.9	6970314.8	445.1	50.0	MGA94_50	90	-90	AC	Sept 2024
AC0004	588910.0	6970310.0	444.8	54.0	MGA94_50	90	-90	AC	Sept 2024
AC0005	589105.2	6970311.5	444.5	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0006	587707.0	6971382.5	441.5	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0007	587896.1	6971379.8	441.5	54.0	MGA94_50	90	-90	AC	Sept 2024
AC0008	588098.4	6971380.2	441.0	50.0	MGA94_50	90	-90	AC	Sept 2024
AC0009	588302.8	6971380.3	441.7	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0010	588504.0	6971376.3	441.2	53.0	MGA94_50	90	-90	AC	Sept 2024
AC0011	588700.3	6971393.8	440.8	55.0	MGA94_50	90	-90	AC	Sept 2024
AC0012	588891.3	6971379.8	440.7	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0013	589101.2	6971379.0	440.7	67.0	MGA94_50	90	-90	AC	Sept 2024
AC0014	589294.6	6971375.6	440.2	26.0	MGA94_50	90	-90	AC	Sept 2024
AC0015	588397.8	6972166.6	438.1	46.0	MGA94_50	90	-90	AC	Sept 2024
AC0016	588597.5	6972171.7	437.9	51.0	MGA94_50	90	-90	AC	Sept 2024
AC0017	588796.3	6972187.7	437.9	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0018	589001.1	6972171.1	438.1	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0019	589185.0	6972175.2	438.3	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0020	589395.9	6972169.7	438.3	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0021	585878.0	6973686.2	428.8	54.0	MGA94_50	90	-90	AC	Sept 2024
AC0022	586077.2	6973695.7	429.2	64.0	MGA94_50	90	-90	AC	Sept 2024
AC0023	586265.3	6973707.8	429.4	60.0	MGA94_50	90	-90	AC	Sept 2024
AC0024	586464.7	6973695.2	429.8	55.0	MGA94_50	90	-90	AC	Sept 2024
AC0025	586676.1	6973705.4	430.2	16.0	MGA94_50	90	-90	AC	Sept 2024
AC0026	585915.9	6973899.7	428.1	46.0	MGA94_50	90	-90	AC	Sept 2024
AC0027	586117.4	6973910.9	428.4	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0028	586330.1	6973897.1	429.0	45.0	MGA94_50	90	-90	AC	Sept 2024
AC0029	586521.0	6973902.4	429.3	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0030	586711.4	6973921.6	429.4	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0031	585967.5	6974128.1	427.1	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0032	586172.6	6974105.3	428.0	49.0	MGA94_50	90	-90	AC	Sept 2024
AC0033	586362.9	6974105.2	428.3	51.0	MGA94_50	90	-90	AC	Sept 2024
AC0034	586578.1	6974107.5	428.6	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0035	585916.3	6974402.3	426.4	14.0	MGA94_50	90	-90	AC	Sept 2024
AC0036	586125.6	6974383.8	427.1	31.0	MGA94_50	90	-90	AC	Sept 2024
AC0037	586280.0	6974426.6	427.1	65.0	MGA94_50	90	-90	AC	Sept 2024
AC0038	589538.7	6977427.4	422.0	19.0	MGA94_50	90	-90	AC	Sept 2024
AC0039	589716.5	6977433.3	421.8	25.0	MGA94_50	90	-90	AC	Sept 2024
AC0040	589926.5	6977446.8	421.8	47.0	MGA94_50	90	-90	AC	Sept 2024
AC0041	590118.4	6977429.9	422.1	74.0	MGA94_50	90	-90	AC	Sept 2024
AC0042	590318.1	6977435.1	422.1	63.0	MGA94_50	90	-90	AC	Sept 2024
AC0043	590506.1	6977447.9	422.0	57.0	MGA94_50	90	-90	AC	Sept 2024
AC0044	588001.0	6978641.5	419.3	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0045	588595.8	6978641.0	419.4	3.0	MGA94_50	90	-90	AC	Sept 2024
AC0046	589469.8	6978632.4	419.6	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0051	588188.0	6979233.8	419.3	51.0	MGA94_50	90	-90	AC	Sept 2024

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HoleID	East	North	RL	Depth	Grid	Azimuth	Dip	HoleType	DateDrilled
AC0052	589112.2	6979232.2	419.6	47.0	MGA94_50	90	-90	AC	Sept 2024
AC0053	589424.8	6979227.5	419.8	47.0	MGA94_50	90	-90	AC	Sept 2024
AC0054	589701.6	6979230.6	420.0	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0055	589991.9	6979234.5	420.1	36.0	MGA94_50	90	-90	AC	Sept 2024
AC0056	590288.7	6979241.5	420.3	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0058	587991.8	6979829.7	419.4	66.0	MGA94_50	90	-90	AC	Sept 2024
AC0059	588605.8	6979820.4	419.1	59.0	MGA94_50	90	-90	AC	Sept 2024
AC0060	589422.8	6979831.9	419.9	62.0	MGA94_50	90	-90	AC	Sept 2024
AC0061	589489.9	6981957.0	420.8	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0062	590705.7	6981962.3	420.5	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0063	591304.4	6981949.7	422.6	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0065	590381.3	6982401.3	420.4	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0066	590918.6	6982405.2	420.6	3.0	MGA94_50	90	-90	AC	Sept 2024
AC0067	589499.7	6982866.4	420.7	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0068	590700.0	6982847.1	420.9	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0069	591300.0	6982840.0	422.0	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0070	589386.3	6983320.3	421.1	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0071	589978.3	6983304.4	421.2	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0072	591148.0	6983321.1	421.4	20.0	MGA94_50	90	-90	AC	Sept 2024
AC0073	589685.9	6983770.9	421.8	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0074	590274.5	6983775.4	421.8	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0075	591495.7	6983769.9	421.7	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0076	590287.4	6984234.3	422.3	7.0	MGA94_50	90	-90	AC	Sept 2024
AC0077	590886.9	6984265.2	422.4	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0078	591489.5	6984259.1	422.2	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0079	589994.7	6984778.0	422.8	12.0	MGA94_50	90	-90	AC	Sept 2024
AC0080	590585.4	6984781.5	423.0	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0081	591191.6	6984781.0	423.1	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0082	591700.5	6984785.3	423.0	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0083	590922.7	6984772.5	423.1	29.0	MGA94_50	90	-90	AC	Sept 2024
AC0084	586587.6	6973323.5	431.4	50.0	MGA94_50	90	-90	AC	Sept 2024
AC0085	586609.4	6973307.1	431.4	42.0	MGA94_50	90	-90	AC	Sept 2024
AC0086	589620.9	6973585.4	433.6	58.0	MGA94_50	90	-90	AC	Sept 2024
AC0087	589105.1	6975146.5	428.3	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0088	589630.1	6973563.7	433.7	51.0	MGA94_50	90	-90	AC	Sept 2024
AC0089	589091.7	6973334.4	434.3	45.0	MGA94_50	90	-90	AC	Sept 2024
AC0090	589116.2	6975127.4	428.5	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0091	589103.5	6973315.9	434.4	57.0	MGA94_50	90	-90	AC	Sept 2024
AC0092	588699.5	6975581.5	427.1	81.0	MGA94_50	90	-90	AC	Sept 2024
AC0093	588719.4	6975563.9	427.1	77.0	MGA94_50	90	-90	AC	Sept 2024
AC0094	589882.3	6975129.1	428.6	71.0	MGA94_50	90	-90	AC	Sept 2024
AC0095	590909.3	6984795.7	423.2	24.0	MGA94_50	90	-90	AC	Sept 2024
AC0096	590188.5	6975802.5	426.8	45.0	MGA94_50	90	-90	AC	Sept 2024
AC0097	589910.5	6975133.4	428.5	72.0	MGA94_50	90	-90	AC	Sept 2024
AC0098	589822.1	6975808.7	426.5	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0099	590169.5	6975832.2	426.7	32.0	MGA94_50	90	-90	AC	Sept 2024
AC0100	589803.8	6975768.7	426.6	52.0	MGA94_50	90	-90	AC	Sept 2024

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APPENDIX 5: Drillhole significant intersections > 330ppm TREO + Sc_2O_3

HoleID	From (m)	To (m)	Interval (m)	TREO ppm	LREO ppm	HREO ppm	MREO ppm	CREO ppm
AC0003	9.0	15.0	6.0	362.3	259.6	102.6	85.8	136.0
AC0004	6.0	12.0	6.0	529.9	364.8	165.1	104.8	188.9
AC0005	13.0	15.0	2.0	471.5	339.7	131.8	114.8	176.9
AC0006	19.0	20.0	1.0	755.2	676.6	78.6	142.1	154.6
AC0006	27.0	30.0	3.0	408.0	287.9	120.2	86.1	146.1
AC0007	14.0	23.0	9.0	520.6	381.5	139.1	98.9	167.1
AC0008	2.0	5.0	3.0	647.1	548.1	99.0	153.0	170.1
AC0008	27.0	28.0	1.0	316.3	212.7	103.6	62.5	116.8
AC0010	22.0	26.0	4.0	725.5	543.7	181.8	156.7	241.5
AC0011	23.0	29.0	6.0	1264.2	892.7	371.5	258.0	448.3
AC0011	44.0	47.0	3.0	534.9	459.9	75.1	132.2	153.0
AC0012	27.0	30.0	3.0	686.7	408.2	278.4	121.4	286.9
AC0015	18.0	25.0	7.0	848.0	637.6	210.4	208.8	296.5
AC0015	26.0	27.0	1.0	326.6	184.5	142.1	73.0	157.1
AC0016	14.0	22.0	8.0	633.4	454.5	179.0	135.6	223.3
AC0017	13.0	21.0	8.0	713.8	488.4	225.5	142.5	268.5
AC0018	10.0	14.0	4.0	417.8	294.7	123.0	67.1	134.0
AC0018	15.0	18.0	3.0	465.6	311.4	154.3	137.1	211.7
AC0019	22.0	27.0	5.0	664.0	501.4	162.6	125.3	202.3
AC0020	18.0	22.0	4.0	556.3	382.4	173.8	123.9	211.2
AC0021	13.0	14.0	1.0	322.3	160.7	161.6	56.2	150.7
AC0021	15.0	38.0	23.0	414.2	229.3	184.9	84.0	189.4
AC0021	43.0	49.0	6.0	389.7	218.9	170.7	80.2	176.8
AC0022	12.0	13.0	1.0	356.9	198.5	158.3	66.9	158.0
AC0022	14.0	17.0	3.0	487.3	326.8	160.6	107.4	189.7
AC0022	19.0	38.0	19.0	535.7	343.6	192.1	124.6	225.6
AC0022	39.0	46.0	7.0	394.0	207.5	186.5	80.2	188.1
AC0022	51.0	52.0	1.0	384.1	203.1	180.9	77.3	183.1
AC0022	54.0	55.0	1.0	413.7	223.0	190.6	84.7	194.8
AC0022	60.0	61.0	1.0	365.9	188.5	177.3	72.7	177.2
AC0022	62.0	63.0	1.0	407.1	240.2	166.9	86.1	179.1
AC0023	10.0	26.0	16.0	441.5	240.2	201.2	91.3	207.9
AC0023	27.0	35.0	8.0	463.0	270.4	192.6	98.3	206.3
AC0023	36.0	37.0	1.0	367.5	151.8	215.7	67.7	201.0
AC0023	38.0	40.0	2.0	344.8	158.3	186.5	66.1	179.4
AC0023	41.0	42.0	1.0	365.4	163.4	202.0	68.9	192.5
AC0023	44.0	46.0	2.0	760.6	538.6	222.0	193.5	295.1
AC0023	47.0	57.0	10.0	380.8	200.4	180.4	77.6	184.0
AC0023	58.0	59.0	1.0	363.5	204.7	158.8	78.2	168.5
AC0024	19.0	30.0	11.0	734.5	583.6	150.9	153.4	216.4
AC0024	31.0	38.0	7.0	474.1	290.1	184.0	118.4	215.6
AC0024	39.0	40.0	1.0	368.8	215.4	153.5	83.1	169.0
AC0024	49.0	53.0	4.0	434.0	226.5	207.5	86.5	205.6
AC0024	54.0	55.0	1.0	369.2	173.0	196.2	69.9	187.0
AC0025	11.0	14.0	3.0	792.1	365.5	426.6	161.1	417.8
AC0026	14.0	15.0	1.0	480.5	322.4	158.1	121.6	202.1
AC0026	21.0	22.0	1.0	317.8	174.6	143.2	67.6	150.6

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HoleID	From (m)	To (m)	Interval (m)	La2O3 ppm	CeO2 ppm	Pr6O11 ppm	Nd2O3 ppm	Sm2O3 ppm
AC0003	9.0	15.0	6.0	68.7	105.4	15.7	58.5	11.4
AC0004	6.0	12.0	6.0	72.9	193.2	17.5	67.3	13.9
AC0005	13.0	15.0	2.0	115.4	108.5	21.9	78.3	15.6
AC0006	19.0	20.0	1.0	228.7	301.0	32.1	98.2	16.6
AC0006	27.0	30.0	3.0	77.5	126.4	16.0	55.9	12.1
AC0007	14.0	23.0	9.0	82.5	203.0	17.3	65.5	13.2
AC0008	2.0	5.0	3.0	150.9	240.6	25.8	107.4	23.5
AC0008	27.0	28.0	1.0	45.9	107.2	10.5	40.8	8.3
AC0010	22.0	26.0	4.0	132.7	255.0	29.2	106.9	19.9
AC0011	23.0	29.0	6.0	182.5	457.8	45.8	171.5	35.1
AC0011	44.0	47.0	3.0	103.4	217.0	25.0	99.0	15.3
AC0012	27.0	30.0	3.0	90.2	210.5	18.7	73.4	15.4
AC0015	18.0	25.0	7.0	162.1	264.5	38.3	143.7	29.0
AC0015	26.0	27.0	1.0	65.6	50.4	11.7	47.4	9.5
AC0016	14.0	22.0	8.0	99.7	220.1	24.6	90.7	19.5
AC0017	13.0	21.0	8.0	124.9	224.3	26.2	94.5	18.5
AC0018	10.0	14.0	4.0	43.8	188.6	10.7	42.0	9.6
AC0018	15.0	18.0	3.0	103.4	70.1	24.1	95.9	17.9
AC0019	22.0	27.0	5.0	91.2	287.6	22.7	83.6	16.4
AC0020	18.0	22.0	4.0	84.7	176.0	21.8	82.5	17.5
AC0021	13.0	14.0	1.0	25.1	88.3	7.0	31.3	9.0
AC0021	15.0	38.0	23.0	48.4	103.8	12.7	51.3	13.0
AC0021	43.0	49.0	6.0	46.1	98.6	12.0	49.8	12.4
AC0022	12.0	13.0	1.0	51.8	87.0	10.5	39.0	10.3
AC0022	14.0	17.0	3.0	75.6	145.2	19.3	71.0	15.7
AC0022	19.0	38.0	19.0	81.2	139.9	20.8	83.0	18.7
AC0022	39.0	46.0	7.0	43.9	91.2	11.8	48.6	12.1
AC0022	51.0	52.0	1.0	42.2	91.0	11.7	46.3	11.9
AC0022	54.0	55.0	1.0	46.6	99.7	12.6	50.9	13.3
AC0022	60.0	61.0	1.0	39.5	85.1	10.6	42.6	10.7
AC0022	62.0	63.0	1.0	49.1	109.2	13.3	54.6	14.0
AC0023	10.0	26.0	16.0	52.7	103.5	13.2	56.4	14.3
AC0023	27.0	35.0	8.0	57.6	120.5	14.5	62.4	15.4
AC0023	36.0	37.0	1.0	30.8	66.3	8.9	35.5	10.3
AC0023	38.0	40.0	2.0	31.8	68.6	8.5	38.6	10.8
AC0023	41.0	42.0	1.0	33.3	71.9	9.0	38.8	10.4
AC0023	44.0	46.0	2.0	128.0	215.6	32.2	133.8	29.0
AC0023	47.0	57.0	10.0	43.1	87.6	11.0	47.2	11.5
AC0023	58.0	59.0	1.0	45.5	86.5	11.2	49.7	11.9
AC0024	19.0	30.0	11.0	111.2	316.3	28.9	105.5	21.8
AC0024	31.0	38.0	7.0	86.3	88.3	19.6	77.4	18.4
AC0024	39.0	40.0	1.0	45.0	90.5	12.5	53.1	14.3
AC0024	49.0	53.0	4.0	44.9	103.9	12.8	51.5	13.4
AC0024	54.0	55.0	1.0	35.5	78.7	9.7	39.3	9.7
AC0025	11.0	14.0	3.0	63.9	159.7	21.0	95.3	25.6
AC0026	14.0	15.0	1.0	86.8	114.0	19.9	84.3	17.4
AC0026	21.0	22.0	1.0	37.8	75.1	9.9	41.6	10.2

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HoleID	From (m)	To (m)	Interval (m)	Eu2O3 ppm	Gd2O3 ppm	Tb4O7 ppm	Dy2O3 ppm	Ho2O3 ppm
AC0003	9.0	15.0	6.0	3.0	10.7	1.7	10.0	2.0
AC0004	6.0	12.0	6.0	3.8	15.0	2.6	17.4	3.6
AC0005	13.0	15.0	2.0	3.8	14.8	2.3	12.3	2.6
AC0006	19.0	20.0	1.0	3.8	12.9	2.2	9.5	1.8
AC0006	27.0	30.0	3.0	2.7	12.5	2.1	12.1	2.4
AC0007	14.0	23.0	9.0	3.1	13.4	2.3	13.8	3.0
AC0008	2.0	5.0	3.0	6.1	27.1	3.7	16.1	2.3
AC0008	27.0	28.0	1.0	2.1	9.5	1.4	9.7	2.4
AC0010	22.0	26.0	4.0	4.9	19.7	2.8	17.9	3.6
AC0011	23.0	29.0	6.0	8.2	33.2	5.5	35.1	7.5
AC0011	44.0	47.0	3.0	3.7	12.0	1.4	6.7	1.3
AC0012	27.0	30.0	3.0	4.3	19.9	3.7	25.5	5.4
AC0015	18.0	25.0	7.0	6.6	25.5	3.9	22.9	4.3
AC0015	26.0	27.0	1.0	2.6	11.8	1.9	12.1	2.7
AC0016	14.0	22.0	8.0	4.8	18.8	3.0	17.4	3.7
AC0017	13.0	21.0	8.0	4.4	19.5	3.2	18.6	4.2
AC0018	10.0	14.0	4.0	2.4	10.6	1.8	12.6	2.5
AC0018	15.0	18.0	3.0	4.2	16.6	2.5	14.7	2.9
AC0019	22.0	27.0	5.0	4.1	16.8	2.7	16.3	3.4
AC0020	18.0	22.0	4.0	4.3	16.8	2.7	17.0	3.5
AC0021	13.0	14.0	1.0	1.7	12.9	2.3	15.6	3.6
AC0021	15.0	38.0	23.0	3.0	14.8	2.6	17.3	3.8
AC0021	43.0	49.0	6.0	2.8	13.7	2.3	16.0	3.6
AC0022	12.0	13.0	1.0	2.1	12.1	2.3	15.1	3.4
AC0022	14.0	17.0	3.0	3.1	14.3	2.5	14.6	3.3
AC0022	19.0	38.0	19.0	3.5	17.9	2.9	17.8	3.9
AC0022	39.0	46.0	7.0	2.7	14.7	2.6	17.2	3.9
AC0022	51.0	52.0	1.0	2.6	13.8	2.6	16.8	3.6
AC0022	54.0	55.0	1.0	2.8	15.2	2.7	18.6	3.9
AC0022	60.0	61.0	1.0	1.9	13.2	2.5	17.0	3.7
AC0022	62.0	63.0	1.0	1.8	14.5	2.4	15.8	3.4
AC0023	10.0	26.0	16.0	2.8	16.5	2.9	18.7	4.1
AC0023	27.0	35.0	8.0	2.7	16.8	2.9	18.4	4.0
AC0023	36.0	37.0	1.0	2.6	14.6	3.1	20.3	4.5
AC0023	38.0	40.0	2.0	2.4	13.4	2.5	16.4	3.8
AC0023	41.0	42.0	1.0	2.5	14.4	2.8	18.3	4.6
AC0023	44.0	46.0	2.0	5.0	27.7	4.0	23.4	4.6
AC0023	47.0	57.0	10.0	2.2	13.6	2.5	16.9	3.6
AC0023	58.0	59.0	1.0	2.2	12.7	2.2	15.1	3.3
AC0024	19.0	30.0	11.0	3.0	18.5	2.8	16.2	3.0
AC0024	31.0	38.0	7.0	3.5	20.3	3.2	18.2	3.7
AC0024	39.0	40.0	1.0	2.7	14.8	2.4	15.1	3.1
AC0024	49.0	53.0	4.0	1.7	16.0	2.9	19.3	4.4
AC0024	54.0	55.0	1.0	1.0	12.7	2.7	18.2	4.3
AC0025	11.0	14.0	3.0	7.5	34.2	6.0	38.9	8.5
AC0026	14.0	15.0	1.0	3.0	15.0	2.3	15.0	3.3
AC0026	21.0	22.0	1.0	2.0	11.1	2.0	14.0	3.0

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HoleID	From (m)	To (m)	Interval (m)	Er2O3 ppm	Tm2O3 ppm	Yb2O3 ppm	Lu2O3 ppm	Y2O3 ppm
AC0003	9.0	15.0	6.0	5.8	0.8	5.1	0.7	62.8
AC0004	6.0	12.0	6.0	11.6	1.6	10.2	1.5	97.8
AC0005	13.0	15.0	2.0	6.8	0.9	7.1	0.9	80.2
AC0006	19.0	20.0	1.0	3.8	0.4	3.1	0.3	40.9
AC0006	27.0	30.0	3.0	6.8	0.9	6.6	0.8	73.3
AC0007	14.0	23.0	9.0	9.0	1.3	9.5	1.2	82.4
AC0008	2.0	5.0	3.0	4.3	0.4	2.0	0.2	36.8
AC0008	27.0	28.0	1.0	6.4	1.1	7.3	1.0	62.7
AC0010	22.0	26.0	4.0	9.9	1.6	10.7	1.6	109.1
AC0011	23.0	29.0	6.0	22.8	3.5	23.9	3.8	227.9
AC0011	44.0	47.0	3.0	3.7	0.5	3.1	0.5	42.2
AC0012	27.0	30.0	3.0	18.2	2.5	16.3	2.7	179.9
AC0015	18.0	25.0	7.0	12.7	1.7	11.7	1.6	119.4
AC0015	26.0	27.0	1.0	8.1	1.1	7.6	1.1	93.2
AC0016	14.0	22.0	8.0	10.9	1.6	10.0	1.4	107.4
AC0017	13.0	21.0	8.0	13.1	1.9	11.1	1.8	147.7
AC0018	10.0	14.0	4.0	8.1	1.1	7.7	1.0	75.3
AC0018	15.0	18.0	3.0	8.9	1.2	7.8	1.1	94.4
AC0019	22.0	27.0	5.0	10.6	1.5	10.3	1.4	95.5
AC0020	18.0	22.0	4.0	11.0	1.7	10.5	1.6	104.8
AC0021	13.0	14.0	1.0	11.4	1.6	11.1	1.5	99.8
AC0021	15.0	38.0	23.0	12.3	1.9	12.3	1.8	115.2
AC0021	43.0	49.0	6.0	11.4	1.8	11.6	1.7	105.8
AC0022	12.0	13.0	1.0	10.1	1.6	10.7	1.4	99.6
AC0022	14.0	17.0	3.0	10.8	1.6	10.3	1.5	98.5
AC0022	19.0	38.0	19.0	12.6	1.7	11.7	1.7	118.3
AC0022	39.0	46.0	7.0	12.6	1.8	12.1	1.9	116.9
AC0022	51.0	52.0	1.0	11.8	1.7	11.7	1.6	114.9
AC0022	54.0	55.0	1.0	12.4	1.6	12.0	1.7	120.0
AC0022	60.0	61.0	1.0	11.6	1.6	11.0	1.7	113.1
AC0022	62.0	63.0	1.0	10.3	1.7	10.7	1.8	104.5
AC0023	10.0	26.0	16.0	12.6	1.8	12.6	2.0	127.1
AC0023	27.0	35.0	8.0	11.9	1.8	12.4	1.8	119.9
AC0023	36.0	37.0	1.0	13.7	1.9	13.3	2.0	139.7
AC0023	38.0	40.0	2.0	11.9	2.0	12.7	1.9	119.5
AC0023	41.0	42.0	1.0	12.7	2.0	12.5	2.1	130.2
AC0023	44.0	46.0	2.0	13.0	2.0	11.7	1.7	128.8
AC0023	47.0	57.0	10.0	11.5	1.8	11.2	1.9	115.2
AC0023	58.0	59.0	1.0	10.8	1.5	10.0	1.7	99.3
AC0024	19.0	30.0	11.0	8.7	1.2	7.4	1.1	88.9
AC0024	31.0	38.0	7.0	10.6	1.4	8.6	1.3	113.2
AC0024	39.0	40.0	1.0	9.1	1.3	8.2	1.1	95.8
AC0024	49.0	53.0	4.0	13.8	2.1	14.9	2.2	130.1
AC0024	54.0	55.0	1.0	13.1	2.1	14.1	2.3	125.8
AC0025	11.0	14.0	3.0	26.9	3.9	26.8	3.9	270.1
AC0026	14.0	15.0	1.0	9.5	1.5	9.4	1.7	97.4
AC0026	21.0	22.0	1.0	8.7	1.3	8.8	1.4	90.9

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HoleID	From (m)	To (m)	Interval (m)	Sc2O3 ppm	Th ppm	U ppm	Nb ppm	Ta ppm
AC0003	9.0	15.0	6.0	22.9	7.3	1.6	5.5	0.4
AC0004	6.0	12.0	6.0	21.2	6.2	1.2	4.5	0.4
AC0005	13.0	15.0	2.0	20.1	5.2	1.3	3.8	0.4
AC0006	19.0	20.0	1.0	38.2	10.6	3.6	12.4	0.6
AC0006	27.0	30.0	3.0	27.5	9.5	4.6	7.0	0.6
AC0007	14.0	23.0	9.0	26.3	8.5	3.7	6.6	0.6
AC0008	2.0	5.0	3.0	33.4	12.9	2.0	5.3	0.4
AC0008	27.0	28.0	1.0	22.2	7.5	2.0	5.8	0.4
AC0010	22.0	26.0	4.0	22.1	9.5	2.2	6.2	0.6
AC0011	23.0	29.0	6.0	26.4	8.5	3.9	6.9	0.6
AC0011	44.0	47.0	3.0	29.2	37.6	6.3	11.0	0.6
AC0012	27.0	30.0	3.0	20.1	10.3	2.8	6.4	0.5
AC0015	18.0	25.0	7.0	20.7	6.1	2.7	6.5	0.5
AC0015	26.0	27.0	1.0	20.7	5.2	2.0	4.5	0.4
AC0016	14.0	22.0	8.0	22.4	6.4	1.8	5.2	0.4
AC0017	13.0	21.0	8.0	20.9	4.9	1.4	4.6	0.4
AC0018	10.0	14.0	4.0	21.0	5.0	1.5	4.9	0.4
AC0018	15.0	18.0	3.0	18.4	5.0	1.0	4.5	0.4
AC0019	22.0	27.0	5.0	17.0	10.1	2.6	6.0	0.7
AC0020	18.0	22.0	4.0	22.0	7.4	1.5	6.2	0.5
AC0021	13.0	14.0	1.0	17.2	7.9	3.0	10.1	0.8
AC0021	15.0	38.0	23.0	17.1	8.1	2.8	9.9	0.8
AC0021	43.0	49.0	6.0	17.1	7.5	3.1	9.7	0.8
AC0022	12.0	13.0	1.0	14.0	8.5	1.8	7.9	0.6
AC0022	14.0	17.0	3.0	17.6	10.4	2.2	8.6	0.7
AC0022	19.0	38.0	19.0	16.7	7.6	2.5	8.5	0.6
AC0022	39.0	46.0	7.0	16.9	7.2	2.7	9.0	0.7
AC0022	51.0	52.0	1.0	16.0	6.8	2.0	8.7	0.6
AC0022	54.0	55.0	1.0	14.6	7.1	2.2	8.9	0.7
AC0022	60.0	61.0	1.0	16.4	6.5	1.9	7.9	0.6
AC0022	62.0	63.0	1.0	14.3	6.3	2.1	8.5	0.7
AC0023	10.0	26.0	16.0	17.2	6.3	2.0	8.2	0.6
AC0023	27.0	35.0	8.0	16.8	6.6	2.1	8.2	0.7
AC0023	36.0	37.0	1.0	21.9	6.1	2.2	8.8	0.7
AC0023	38.0	40.0	2.0	17.5	6.1	2.4	8.2	0.7
AC0023	41.0	42.0	1.0	14.4	6.5	2.6	8.2	0.7
AC0023	44.0	46.0	2.0	37.9	10.2	3.4	7.3	0.6
AC0023	47.0	57.0	10.0	18.3	6.4	2.0	9.0	0.7
AC0023	58.0	59.0	1.0	18.4	6.2	1.5	9.0	0.6
AC0024	19.0	30.0	11.0	55.8	10.9	5.9	6.3	0.4
AC0024	31.0	38.0	7.0	59.3	11.5	4.0	6.2	0.4
AC0024	39.0	40.0	1.0	54.0	10.9	3.3	4.8	0.3
AC0024	49.0	53.0	4.0	19.1	12.5	2.7	12.8	0.9
AC0024	54.0	55.0	1.0	7.5	11.8	2.5	12.9	0.9
AC0025	11.0	14.0	3.0	24.0	5.8	3.8	6.8	0.5
AC0026	14.0	15.0	1.0	11.8	5.3	1.7	7.4	0.6
AC0026	21.0	22.0	1.0	13.0	5.5	1.9	8.5	0.7

HoleID	From (m)	To (m)	Zr ppm	Hf ppm	Co ppm	Cu ppm	Ni ppm
AC0003	9.0	15.0	170.0	4.4	11.0	43.7	41.0
AC0004	6.0	12.0	151.0	3.6	18.2	25.8	45.7
AC0005	13.0	15.0	135.0	2.9	41.0	30.0	48.5
AC0006	19.0	20.0	246.0	5.9	1.0	20.0	8.0
AC0006	27.0	30.0	209.0	5.2	20.3	113.3	47.0
AC0007	14.0	23.0	199.0	5.6	25.8	32.6	37.8
AC0008	2.0	5.0	190.0	5.3	5.0	27.7	106.7
AC0008	27.0	28.0	195.0	5.0	11.0	34.0	42.0
AC0010	22.0	26.0	184.0	5.1	41.0	48.3	41.8
AC0011	23.0	29.0	178.0	4.8	14.5	60.3	34.3
AC0011	44.0	47.0	281.0	7.0	35.7	90.0	92.7
AC0012	27.0	30.0	161.0	4.2	17.0	34.7	31.7
AC0015	18.0	25.0	226.0	6.0	14.1	28.0	31.7
AC0015	26.0	27.0	125.0	3.3	37.0	30.0	59.0
AC0016	14.0	22.0	165.0	4.1	24.0	28.3	34.9
AC0017	13.0	21.0	134.0	3.5	21.9	36.6	58.5
AC0018	10.0	14.0	142.0	4.0	24.0	47.3	40.3
AC0018	15.0	18.0	150.0	4.0	31.7	20.0	43.7
AC0019	22.0	27.0	161.0	4.5	14.2	29.8	37.4
AC0020	18.0	22.0	162.0	4.4	29.0	30.3	49.8
AC0021	13.0	14.0	284.0	7.0	15.0	51.0	5.0
AC0021	15.0	38.0	339.0	9.6	4.9	8.5	3.7
AC0021	43.0	49.0	337.0	9.3	5.5	8.5	2.8
AC0022	12.0	13.0	217.0	5.9	1.0	3.0	2.0
AC0022	14.0	17.0	260.0	7.2	0.8	8.0	6.3
AC0022	19.0	38.0	263.0	7.3	4.8	9.0	5.5
AC0022	39.0	46.0	289.0	8.0	4.0	1.0	3.3
AC0022	51.0	52.0	276.0	8.0	2.0	1.0	3.0
AC0022	54.0	55.0	280.0	8.4	3.0	1.0	2.0
AC0022	60.0	61.0	245.0	7.3	1.0	1.0	4.0
AC0022	62.0	63.0	276.0	7.0	1.0	1.0	3.0
AC0023	10.0	26.0	238.0	6.6	5.8	2.9	7.9
AC0023	27.0	35.0	261.0	7.1	2.1	1.1	5.6
AC0023	36.0	37.0	377.0	10.4	2.0	7.0	5.0
AC0023	38.0	40.0	283.0	7.4	3.5	1.3	0.8
AC0023	41.0	42.0	262.0	7.1	3.0	1.0	3.0
AC0023	44.0	46.0	243.0	6.7	13.5	41.5	24.0
AC0023	47.0	57.0	291.0	7.7	4.2	1.6	3.6
AC0023	58.0	59.0	284.0	7.4	2.0	1.0	3.0
AC0024	19.0	30.0	185.0	5.0	30.3	133.1	76.0
AC0024	31.0	38.0	199.0	5.5	40.3	57.6	55.6
AC0024	39.0	40.0	221.0	5.8	31.0	37.0	74.0
AC0024	49.0	53.0	342.0	10.2	12.5	23.3	49.5
AC0024	54.0	55.0	261.0	8.2	1.0	3.0	4.0
AC0025	11.0	14.0	201.0	5.3	5.7	4.7	2.2
AC0026	14.0	15.0	225.0	6.2	5.0	13.0	5.0
AC0026	21.0	22.0	258.0	6.5	4.0	2.0	3.0

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HoleID	From (m)	To (m)	Interval (m)	TREO ppm	LREO ppm	HREO ppm	MREO ppm	CREO ppm
AC0026	25.0	27.0	2.0	342.4	189.8	152.6	73.2	160.6
AC0026	36.0	37.0	1.0	314.7	160.3	154.3	63.1	154.0
AC0027	16.0	20.0	4.0	759.4	567.5	191.9	186.4	269.4
AC0027	21.0	38.0	17.0	402.0	223.9	178.1	82.8	185.0
AC0027	40.0	43.0	3.0	367.8	189.7	178.1	72.2	177.1
AC0027	44.0	46.0	2.0	407.6	239.7	167.9	88.1	182.2
AC0027	48.0	49.0	1.0	357.5	212.5	145.0	76.1	156.2
AC0027	50.0	51.0	1.0	422.7	258.2	164.6	91.4	181.0
AC0027	52.0	54.0	2.0	359.0	212.9	146.1	74.8	157.7
AC0028	11.0	21.0	10.0	727.1	481.8	245.3	168.1	292.6
AC0028	23.0	25.0	2.0	332.3	179.8	152.5	70.6	158.0
AC0028	27.0	29.0	2.0	421.3	232.8	188.5	84.1	192.5
AC0028	30.0	34.0	4.0	430.3	256.0	174.3	96.2	189.4
AC0028	35.0	44.0	9.0	570.5	389.6	180.9	128.9	220.6
AC0029	13.0	23.0	10.0	637.5	356.6	280.9	113.5	283.3
AC0029	25.0	31.0	6.0	504.5	281.8	222.6	101.7	231.1
AC0029	32.0	34.0	2.0	367.7	163.9	203.8	68.3	193.5
AC0029	35.0	37.0	2.0	394.5	212.1	182.4	80.0	188.0
AC0029	38.0	41.0	3.0	468.7	301.5	167.3	102.4	190.5
AC0029	44.0	51.0	7.0	511.8	317.0	194.7	110.2	214.9
AC0029	52.0	56.0	4.0	342.1	148.9	193.2	61.2	181.6
AC0030	21.0	28.0	7.0	704.2	290.6	413.6	132.0	395.9
AC0030	30.0	36.0	6.0	346.4	178.9	167.4	66.3	167.3
AC0030	38.0	39.0	1.0	383.2	190.5	192.7	68.7	187.6
AC0031	10.0	11.0	1.0	340.7	180.2	160.5	71.2	166.8
AC0031	17.0	19.0	2.0	351.0	182.5	168.5	71.9	169.9
AC0031	29.0	30.0	1.0	370.7	218.9	151.8	79.6	165.4
AC0031	34.0	41.0	7.0	343.0	168.3	174.7	70.8	174.4
AC0032	18.0	28.0	10.0	453.7	285.8	167.9	101.0	190.3
AC0032	47.0	48.0	1.0	336.9	177.8	159.2	66.8	159.4
AC0033	16.0	44.0	28.0	408.0	228.6	179.5	84.9	187.3
AC0033	45.0	47.0	2.0	349.6	169.8	179.8	68.3	175.7
AC0034	18.0	20.0	2.0	398.2	252.9	145.3	78.7	157.0
AC0034	21.0	26.0	5.0	456.6	309.9	146.7	109.0	181.0
AC0034	27.0	28.0	1.0	485.3	309.6	175.6	102.0	197.0
AC0034	31.0	33.0	2.0	394.9	234.4	160.5	83.2	173.2
AC0034	34.0	35.0	1.0	417.0	260.6	156.4	93.4	177.0
AC0036	18.0	19.0	1.0	321.7	140.9	180.8	47.5	160.9
AC0036	20.0	29.0	9.0	444.2	267.2	177.1	93.5	191.9
AC0037	14.0	15.0	1.0	340.2	179.7	160.4	63.7	158.5
AC0037	25.0	27.0	2.0	348.2	201.4	146.8	53.7	136.8
AC0037	29.0	30.0	1.0	445.6	283.5	162.1	105.2	184.9
AC0037	31.0	32.0	1.0	468.4	264.0	204.4	98.7	211.8
AC0037	36.0	37.0	1.0	938.9	561.6	377.3	201.4	416.7
AC0037	38.0	41.0	3.0	372.7	198.6	174.1	78.2	175.6
AC0037	42.0	44.0	2.0	422.5	260.6	161.9	98.4	179.8
AC0037	49.0	50.0	1.0	380.7	223.7	156.9	83.8	170.6

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HoleID	From (m)	To (m)	Interval (m)	La2O3 ppm	CeO2 ppm	Pr6O11 ppm	Nd2O3 ppm	Sm2O3 ppm
AC0026	25.0	27.0	2.0	39.1	83.5	10.4	45.6	11.1
AC0026	36.0	37.0	1.0	33.7	70.0	8.7	37.9	10.0
AC0027	16.0	20.0	4.0	122.0	251.1	34.4	130.7	29.2
AC0027	21.0	38.0	17.0	49.1	98.5	12.8	50.9	12.6
AC0027	40.0	43.0	3.0	39.2	85.3	10.5	43.0	11.6
AC0027	44.0	46.0	2.0	48.3	107.1	13.9	56.3	14.1
AC0027	48.0	49.0	1.0	45.4	95.6	11.9	47.7	11.9
AC0027	50.0	51.0	1.0	54.7	116.5	14.7	57.9	14.6
AC0027	52.0	54.0	2.0	43.0	98.6	11.8	48.2	11.3
AC0028	11.0	21.0	10.0	114.1	202.3	27.6	111.9	26.0
AC0028	23.0	25.0	2.0	39.5	74.6	10.3	44.4	11.0
AC0028	27.0	29.0	2.0	53.1	103.7	12.5	51.2	12.3
AC0028	30.0	34.0	4.0	54.1	109.4	14.6	61.8	16.2
AC0028	35.0	44.0	9.0	80.1	181.9	22.2	86.7	18.7
AC0029	13.0	23.0	10.0	64.3	190.5	17.5	68.2	16.1
AC0029	25.0	31.0	6.0	68.8	120.1	15.8	62.7	14.4
AC0029	32.0	34.0	2.0	33.0	73.0	9.3	39.0	9.7
AC0029	35.0	37.0	2.0	44.2	94.8	12.0	49.5	11.7
AC0029	38.0	41.0	3.0	64.5	137.9	17.0	66.8	15.3
AC0029	44.0	51.0	7.0	69.1	142.8	18.1	70.4	16.6
AC0029	52.0	56.0	4.0	29.0	68.8	8.4	33.6	9.1
AC0030	21.0	28.0	7.0	64.4	115.0	17.1	74.4	19.6
AC0030	30.0	36.0	6.0	38.7	80.5	9.9	39.9	10.0
AC0030	38.0	39.0	1.0	42.2	87.2	10.1	40.2	10.7
AC0031	10.0	11.0	1.0	36.0	78.7	10.0	44.3	11.2
AC0031	17.0	19.0	2.0	34.5	83.6	9.8	43.1	11.5
AC0031	29.0	30.0	1.0	49.0	94.0	11.9	51.3	12.6
AC0031	34.0	41.0	7.0	33.1	71.9	9.7	42.3	11.3
AC0032	18.0	28.0	10.0	63.9	124.2	16.7	65.6	15.4
AC0032	47.0	48.0	1.0	36.5	81.7	10.2	39.5	9.9
AC0033	16.0	44.0	28.0	48.6	101.6	12.9	52.5	13.0
AC0033	45.0	47.0	2.0	34.5	75.6	9.5	39.8	10.4
AC0034	18.0	20.0	2.0	46.7	131.5	13.4	49.7	11.5
AC0034	21.0	26.0	5.0	74.3	127.5	19.3	72.8	16.0
AC0034	27.0	28.0	1.0	72.1	140.0	17.5	64.6	15.4
AC0034	31.0	33.0	2.0	50.6	106.0	13.1	52.6	12.1
AC0034	34.0	35.0	1.0	55.0	116.2	14.6	60.9	14.0
AC0036	18.0	19.0	1.0	17.4	89.1	5.2	22.6	6.6
AC0036	20.0	29.0	9.0	56.5	122.4	15.0	59.1	14.1
AC0037	14.0	15.0	1.0	40.1	82.7	10.3	36.5	10.2
AC0037	25.0	27.0	2.0	65.6	91.0	8.0	29.1	7.7
AC0037	29.0	30.0	1.0	66.6	116.0	16.6	69.2	15.1
AC0037	31.0	32.0	1.0	58.1	117.7	14.7	58.9	14.7
AC0037	36.0	37.0	1.0	137.8	234.0	31.7	128.3	29.8
AC0037	38.0	41.0	3.0	42.6	87.3	11.1	46.8	10.9
AC0037	42.0	44.0	2.0	56.6	109.3	15.1	62.6	16.9
AC0037	49.0	50.0	1.0	48.4	97.2	12.6	52.6	12.9

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HoleID	From (m)	To (m)	Interval (m)	Eu2O3 ppm	Gd2O3 ppm	Tb4O7 ppm	Dy2O3 ppm	Ho2O3 ppm
AC0026	25.0	27.0	2.0	2.0	12.4	2.3	14.8	3.3
AC0026	36.0	37.0	1.0	2.0	11.8	2.3	14.2	3.2
AC0027	16.0	20.0	4.0	5.0	21.5	3.1	18.2	3.8
AC0027	21.0	38.0	17.0	2.6	13.7	2.5	16.6	3.7
AC0027	40.0	43.0	3.0	2.6	13.2	2.5	16.2	3.9
AC0027	44.0	46.0	2.0	2.6	14.3	2.4	15.4	3.6
AC0027	48.0	49.0	1.0	1.7	12.6	2.3	14.2	3.3
AC0027	50.0	51.0	1.0	2.4	14.6	2.6	16.2	3.4
AC0027	52.0	54.0	2.0	2.0	11.9	2.1	12.7	3.0
AC0028	11.0	21.0	10.0	5.1	26.5	4.1	24.5	5.0
AC0028	23.0	25.0	2.0	2.8	13.7	2.2	13.7	3.1
AC0028	27.0	29.0	2.0	2.9	15.0	2.7	17.7	4.1
AC0028	30.0	34.0	4.0	3.5	17.2	2.9	17.0	3.6
AC0028	35.0	44.0	9.0	3.5	18.3	2.8	17.2	3.7
AC0029	13.0	23.0	10.0	2.0	19.6	3.6	24.2	5.5
AC0029	25.0	31.0	6.0	1.7	17.6	3.1	20.1	4.4
AC0029	32.0	34.0	2.0	1.0	12.5	2.4	17.6	4.1
AC0029	35.0	37.0	2.0	1.4	13.5	2.5	16.1	3.6
AC0029	38.0	41.0	3.0	1.2	15.9	2.6	16.0	3.4
AC0029	44.0	51.0	7.0	1.7	17.5	3.1	18.6	4.0
AC0029	52.0	56.0	4.0	0.8	12.8	2.6	16.6	4.1
AC0030	21.0	28.0	7.0	5.2	29.2	5.3	35.2	8.4
AC0030	30.0	36.0	6.0	1.7	12.2	2.1	14.5	3.2
AC0030	38.0	39.0	1.0	1.3	12.2	2.3	16.1	3.6
AC0031	10.0	11.0	1.0	2.1	11.6	2.1	14.7	3.4
AC0031	17.0	19.0	2.0	2.4	13.5	2.6	16.5	3.5
AC0031	29.0	30.0	1.0	2.6	13.4	2.1	14.2	3.1
AC0031	34.0	41.0	7.0	2.7	13.3	2.4	16.5	3.7
AC0032	18.0	28.0	10.0	2.9	15.2	2.5	16.2	3.4
AC0032	47.0	48.0	1.0	2.0	12.0	2.4	14.7	3.3
AC0033	16.0	44.0	28.0	2.7	14.0	2.5	17.0	3.7
AC0033	45.0	47.0	2.0	1.7	12.1	2.4	16.6	3.8
AC0034	18.0	20.0	2.0	1.4	11.0	2.0	13.5	3.2
AC0034	21.0	26.0	5.0	2.0	13.9	2.4	14.5	3.1
AC0034	27.0	28.0	1.0	2.1	16.0	3.0	16.9	3.6
AC0034	31.0	33.0	2.0	1.5	13.3	2.5	15.0	3.6
AC0034	34.0	35.0	1.0	1.7	14.8	2.5	15.6	3.2
AC0036	18.0	19.0	1.0	1.6	10.0	2.3	17.4	3.8
AC0036	20.0	29.0	9.0	3.0	14.4	2.6	16.8	3.6
AC0037	14.0	15.0	1.0	2.1	12.0	2.0	14.9	3.6
AC0037	25.0	27.0	2.0	1.8	9.6	1.8	14.8	3.0
AC0037	29.0	30.0	1.0	3.5	17.2	2.5	16.9	3.4
AC0037	31.0	32.0	1.0	2.8	16.1	3.0	22.1	4.2
AC0037	36.0	37.0	1.0	6.4	36.1	5.8	35.6	7.4
AC0037	38.0	41.0	3.0	2.7	14.6	2.4	18.0	3.5
AC0037	42.0	44.0	2.0	3.3	18.7	2.9	17.8	3.3
AC0037	49.0	50.0	1.0	3.0	15.6	2.6	16.0	3.4

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HoleID	From (m)	To (m)	Interval (m)	Er2O3 ppm	Tm2O3 ppm	Yb2O3 ppm	Lu2O3 ppm	Y2O3 ppm
AC0026	25.0	27.0	2.0	9.8	1.5	9.1	1.5	95.9
AC0026	36.0	37.0	1.0	10.4	1.6	9.8	1.5	97.7
AC0027	16.0	20.0	4.0	12.2	1.8	12.1	1.8	112.4
AC0027	21.0	38.0	17.0	11.7	1.7	11.5	1.7	112.5
AC0027	40.0	43.0	3.0	12.1	1.7	11.4	1.8	112.7
AC0027	44.0	46.0	2.0	10.6	1.6	10.2	1.6	105.5
AC0027	48.0	49.0	1.0	8.7	1.3	9.1	1.5	90.3
AC0027	50.0	51.0	1.0	10.3	1.5	9.8	1.7	102.0
AC0027	52.0	54.0	2.0	9.4	1.3	9.5	1.4	92.8
AC0028	11.0	21.0	10.0	14.8	2.0	14.2	2.0	147.1
AC0028	23.0	25.0	2.0	9.5	1.4	9.6	1.5	94.9
AC0028	27.0	29.0	2.0	12.1	1.8	12.2	2.0	118.0
AC0028	30.0	34.0	4.0	11.0	1.6	11.5	1.8	104.3
AC0028	35.0	44.0	9.0	11.0	1.6	10.7	1.7	110.4
AC0029	13.0	23.0	10.0	18.1	2.5	17.5	2.7	185.3
AC0029	25.0	31.0	6.0	14.1	2.0	13.9	2.2	143.6
AC0029	32.0	34.0	2.0	13.9	2.0	14.5	2.2	133.5
AC0029	35.0	37.0	2.0	11.6	1.6	11.7	1.8	118.6
AC0029	38.0	41.0	3.0	10.7	1.5	10.3	1.6	103.8
AC0029	44.0	51.0	7.0	12.6	1.8	12.5	1.8	121.1
AC0029	52.0	56.0	4.0	12.2	1.9	12.4	1.8	127.9
AC0030	21.0	28.0	7.0	25.5	3.6	22.2	3.2	275.7
AC0030	30.0	36.0	6.0	10.8	1.6	10.5	1.7	109.2
AC0030	38.0	39.0	1.0	12.9	1.9	12.9	1.9	127.6
AC0031	10.0	11.0	1.0	9.7	1.6	10.2	1.6	103.5
AC0031	17.0	19.0	2.0	10.6	1.6	10.8	1.6	105.4
AC0031	29.0	30.0	1.0	8.9	1.5	9.3	1.6	95.1
AC0031	34.0	41.0	7.0	10.8	1.7	11.3	1.7	110.5
AC0032	18.0	28.0	10.0	10.8	1.6	10.5	1.6	103.0
AC0032	47.0	48.0	1.0	10.7	1.5	10.1	1.8	100.7
AC0033	16.0	44.0	28.0	11.8	1.8	11.7	1.8	112.5
AC0033	45.0	47.0	2.0	12.1	1.8	12.4	1.8	115.1
AC0034	18.0	20.0	2.0	9.9	1.7	10.7	1.6	90.4
AC0034	21.0	26.0	5.0	9.4	1.4	9.4	1.4	89.3
AC0034	27.0	28.0	1.0	11.5	1.6	9.2	1.3	110.5
AC0034	31.0	33.0	2.0	10.5	1.5	9.6	1.5	101.6
AC0034	34.0	35.0	1.0	10.1	1.5	9.4	1.5	96.4
AC0036	18.0	19.0	1.0	12.4	1.8	12.8	1.8	117.1
AC0036	20.0	29.0	9.0	11.5	1.7	11.4	1.7	110.4
AC0037	14.0	15.0	1.0	10.3	1.6	9.4	1.6	103.0
AC0037	25.0	27.0	2.0	10.4	1.8	12.2	2.0	89.3
AC0037	29.0	30.0	1.0	10.7	1.6	11.6	1.7	92.8
AC0037	31.0	32.0	1.0	12.7	2.3	14.1	2.2	125.0
AC0037	36.0	37.0	1.0	21.7	3.0	18.1	2.5	240.6
AC0037	38.0	41.0	3.0	11.6	1.8	12.0	1.8	105.8
AC0037	42.0	44.0	2.0	9.8	1.4	10.0	1.5	93.3
AC0037	49.0	50.0	1.0	8.8	1.3	8.5	1.3	96.5

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HoleID	From (m)	To (m)	Interval (m)	Sc2O3 ppm	Th ppm	U ppm	Nb ppm	Ta ppm
AC0026	25.0	27.0	2.0	16.0	5.6	1.6	10.0	0.7
AC0026	36.0	37.0	1.0	16.6	7.0	2.5	9.7	0.8
AC0027	16.0	20.0	4.0	20.4	7.4	3.6	9.1	0.7
AC0027	21.0	38.0	17.0	18.2	7.4	2.8	9.5	0.7
AC0027	40.0	43.0	3.0	14.9	8.0	2.6	10.4	0.8
AC0027	44.0	46.0	2.0	13.9	7.1	2.2	9.1	0.7
AC0027	48.0	49.0	1.0	12.0	5.0	1.5	8.3	0.6
AC0027	50.0	51.0	1.0	12.1	5.8	1.8	8.6	0.6
AC0027	52.0	54.0	2.0	11.1	5.6	1.6	8.7	0.7
AC0028	11.0	21.0	10.0	19.4	7.1	1.7	8.5	0.6
AC0028	23.0	25.0	2.0	17.5	6.9	1.7	8.8	0.7
AC0028	27.0	29.0	2.0	15.2	7.0	1.8	8.5	0.6
AC0028	30.0	34.0	4.0	18.8	7.6	2.0	8.9	0.7
AC0028	35.0	44.0	9.0	20.8	8.2	2.8	10.1	0.7
AC0029	13.0	23.0	10.0	14.9	14.3	2.0	14.1	1.0
AC0029	25.0	31.0	6.0	15.5	14.5	1.9	14.3	1.0
AC0029	32.0	34.0	2.0	14.9	13.3	2.7	13.4	1.1
AC0029	35.0	37.0	2.0	11.7	11.8	1.7	12.0	0.9
AC0029	38.0	41.0	3.0	11.7	14.4	1.7	11.4	0.9
AC0029	44.0	51.0	7.0	10.0	10.6	1.8	11.0	0.8
AC0029	52.0	56.0	4.0	8.5	8.2	1.5	11.3	0.8
AC0030	21.0	28.0	7.0	17.5	9.2	1.5	9.8	0.7
AC0030	30.0	36.0	6.0	13.7	9.6	1.6	10.8	0.8
AC0030	38.0	39.0	1.0	8.9	10.4	1.7	10.0	0.8
AC0031	10.0	11.0	1.0	19.3	9.3	3.0	9.5	0.6
AC0031	17.0	19.0	2.0	16.8	6.6	2.3	8.9	0.6
AC0031	29.0	30.0	1.0	14.0	5.9	1.5	8.4	0.6
AC0031	34.0	41.0	7.0	16.1	7.4	3.0	9.5	0.7
AC0032	18.0	28.0	10.0	14.4	8.7	1.8	8.7	0.7
AC0032	47.0	48.0	1.0	15.2	6.6	2.4	9.3	0.6
AC0033	16.0	44.0	28.0	20.8	9.0	2.0	9.9	0.7
AC0033	45.0	47.0	2.0	16.3	6.5	1.6	9.5	0.7
AC0034	18.0	20.0	2.0	15.0	13.0	2.2	12.2	1.1
AC0034	21.0	26.0	5.0	11.7	15.0	1.7	11.9	1.0
AC0034	27.0	28.0	1.0	12.9	12.1	1.9	9.6	0.9
AC0034	31.0	33.0	2.0	10.2	10.6	2.3	9.9	0.9
AC0034	34.0	35.0	1.0	8.6	10.3	2.0	10.7	0.8
AC0036	18.0	19.0	1.0	22.2	11.2	2.4	10.3	0.7
AC0036	20.0	29.0	9.0	16.4	7.5	2.7	9.0	0.6
AC0037	14.0	15.0	1.0	10.9	8.8	1.3	9.4	0.6
AC0037	25.0	27.0	2.0	18.8	10.4	1.6	10.7	0.7
AC0037	29.0	30.0	1.0	19.6	10.3	1.5	10.5	0.8
AC0037	31.0	32.0	1.0	20.2	10.3	2.1	10.5	0.7
AC0037	36.0	37.0	1.0	16.1	10.7	2.1	12.9	0.8
AC0037	38.0	41.0	3.0	20.2	8.7	1.5	10.1	0.7
AC0037	42.0	44.0	2.0	16.6	9.8	1.9	10.9	0.8
AC0037	49.0	50.0	1.0	12.6	8.0	2.0	10.4	0.7

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HoleID	From (m)	To (m)	Zr ppm	Hf ppm	Co ppm	Cu ppm	Ni ppm
AC0026	25.0	27.0	227.0	6.4	6.0	1.0	2.0
AC0026	36.0	37.0	285.0	8.4	4.0	7.0	1.0
AC0027	16.0	20.0	340.0	8.6	3.0	63.8	12.5
AC0027	21.0	38.0	300.0	8.1	4.8	26.2	7.4
AC0027	40.0	43.0	326.0	9.0	2.3	6.3	2.7
AC0027	44.0	46.0	280.0	7.5	2.0	2.5	3.5
AC0027	48.0	49.0	199.0	5.4	2.0	1.0	2.0
AC0027	50.0	51.0	232.0	6.8	2.0	1.0	3.0
AC0027	52.0	54.0	247.0	6.6	1.0	1.5	2.0
AC0028	11.0	21.0	256.0	7.1	6.4	8.0	10.1
AC0028	23.0	25.0	271.0	6.5	4.0	16.5	3.0
AC0028	27.0	29.0	299.0	7.5	2.5	19.5	3.5
AC0028	30.0	34.0	291.0	8.3	2.3	12.0	2.5
AC0028	35.0	44.0	283.0	7.0	10.6	17.0	25.3
AC0029	13.0	23.0	306.0	9.6	6.9	10.9	13.1
AC0029	25.0	31.0	340.0	10.7	3.5	4.8	14.2
AC0029	32.0	34.0	373.0	12.0	2.0	3.0	5.5
AC0029	35.0	37.0	259.0	8.7	3.5	5.5	20.0
AC0029	38.0	41.0	262.0	8.8	5.3	4.3	12.0
AC0029	44.0	51.0	265.0	7.8	2.7	2.4	7.9
AC0029	52.0	56.0	251.0	6.9	1.5	1.8	8.3
AC0030	21.0	28.0	290.0	7.8	3.3	6.4	9.4
AC0030	30.0	36.0	248.0	7.3	5.3	2.2	10.8
AC0030	38.0	39.0	299.0	9.2	14.0	3.0	30.0
AC0031	10.0	11.0	290.0	7.5	5.0	20.0	7.0
AC0031	17.0	19.0	229.0	6.4	2.5	12.5	3.5
AC0031	29.0	30.0	230.0	6.3	1.0	0.5	0.5
AC0031	34.0	41.0	316.0	8.7	1.7	9.0	1.1
AC0032	18.0	28.0	280.0	7.7	3.3	21.5	3.6
AC0032	47.0	48.0	262.0	7.2	4.0	4.0	2.0
AC0033	16.0	44.0	309.0	8.9	2.3	5.4	3.9
AC0033	45.0	47.0	276.0	7.7	1.0	2.0	0.8
AC0034	18.0	20.0	335.0	8.9	3.5	39.5	9.5
AC0034	21.0	26.0	305.0	8.8	2.4	9.4	3.2
AC0034	27.0	28.0	245.0	6.9	10.0	16.0	9.0
AC0034	31.0	33.0	297.0	8.0	7.0	74.5	12.5
AC0034	34.0	35.0	275.0	7.5	3.0	36.0	3.0
AC0036	18.0	19.0	407.0	10.2	1.0	43.0	3.0
AC0036	20.0	29.0	314.0	8.1	2.7	28.6	3.1
AC0037	14.0	15.0	233.0	6.0	2.0	4.0	4.0
AC0037	25.0	27.0	404.0	12.1	3.5	60.5	6.5
AC0037	29.0	30.0	382.0	11.2	1.0	26.0	3.0
AC0037	31.0	32.0	427.0	12.1	3.0	58.0	3.0
AC0037	36.0	37.0	361.0	10.0	2.0	8.0	1.0
AC0037	38.0	41.0	365.0	10.4	2.3	1.7	2.0
AC0037	42.0	44.0	431.0	11.4	2.0	2.5	2.0
AC0037	49.0	50.0	358.0	9.2	3.0	3.0	0.5

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HoleID	From (m)	To (m)	Interval (m)	TREO ppm	LREO ppm	HREO ppm	MREO ppm	CREO ppm
AC0037	51.0	53.0	2.0	468.0	289.1	178.9	106.1	201.1
AC0037	54.0	57.0	3.0	412.8	239.6	173.2	86.9	184.0
AC0037	58.0	61.0	3.0	438.7	259.8	178.8	91.1	190.3
AC0040	30.0	40.0	10.0	640.7	266.4	374.3	137.8	376.4
AC0043	42.0	43.0	1.0	2425.6	2037.4	388.2	777.4	839.3
AC0043	44.0	51.0	7.0	876.7	641.4	235.4	225.1	332.1
AC0082	26.0	27.0	1.0	437.8	230.4	207.4	99.0	216.8
AC0082	33.0	40.0	7.0	471.6	284.9	186.6	96.6	194.1
AC0083	21.0	27.0	6.0	651.0	234.5	416.5	126.1	392.1
AC0084	9.0	26.0	17.0	693.5	347.4	346.1	136.6	348.5
AC0084	36.0	38.0	2.0	341.4	183.8	157.6	67.5	160.3
AC0085	11.0	16.0	5.0	685.5	280.1	405.4	139.8	393.2
AC0086	32.0	33.0	1.0	552.6	441.2	111.4	144.8	179.2
AC0086	36.0	38.0	2.0	593.9	327.9	266.0	117.2	278.8
AC0087	45.0	56.0	11.0	1077.4	731.8	345.7	170.5	375.0
AC0088	31.0	37.0	6.0	1196.6	746.5	450.1	258.5	516.9
AC0089	26.0	29.0	3.0	1714.4	1290.9	423.5	513.9	671.7
AC0089	30.0	35.0	5.0	572.6	353.3	219.3	99.1	226.0
AC0090	51.0	52.0	1.0	326.6	260.3	66.3	121.0	133.5
AC0091	23.0	25.0	2.0	482.9	384.0	98.9	100.4	141.0
AC0091	31.0	38.0	7.0	902.1	658.4	243.7	200.3	313.7
AC0092	55.0	59.0	4.0	297.1	185.0	112.1	73.1	127.8
AC0092	75.0	77.0	2.0	999.1	338.3	660.8	226.6	644.9
AC0093	57.0	58.0	1.0	312.0	208.5	103.5	85.0	122.7
AC0093	59.0	60.0	1.0	338.4	220.5	117.9	81.7	125.5
AC0093	61.0	75.0	14.0	484.5	182.5	302.0	104.6	289.7
AC0094	43.0	52.0	9.0	920.8	616.7	304.2	218.6	368.5
AC0095	21.0	24.0	3.0	492.8	178.8	314.0	102.0	297.6
AC0096	29.0	35.0	6.0	1048.0	707.7	340.4	239.6	412.7
AC0097	38.0	48.0	10.0	1437.9	711.4	726.6	333.8	776.7
AC0097	49.0	50.0	1.0	332.9	187.7	145.2	59.3	155.9
AC0098	26.0	29.0	3.0	739.4	527.5	211.9	198.4	290.9
AC0098	33.0	36.0	3.0	434.2	195.9	238.3	85.8	240.8
AC0099	22.0	26.0	4.0	698.9	394.8	304.1	173.3	337.9
AC0100	20.0	23.0	3.0	1561.9	1445.1	116.7	424.2	384.4
AC0100	28.0	35.0	7.0	785.1	486.3	298.7	179.3	338.4

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HoleID	From (m)	To (m)	Interval (m)	La2O3 ppm	CeO2 ppm	Pr6O11 ppm	Nd2O3 ppm	Sm2O3 ppm
AC0037	51.0	53.0	2.0	59.3	128.1	15.8	68.8	17.2
AC0037	54.0	57.0	3.0	51.2	106.1	13.3	55.0	14.0
AC0037	58.0	61.0	3.0	57.7	116.7	13.9	57.3	14.2
AC0040	30.0	40.0	10.0	82.2	61.5	19.6	82.5	20.5
AC0043	42.0	43.0	1.0	557.1	648.6	152.2	570.4	109.1
AC0043	44.0	51.0	7.0	137.9	274.3	39.5	157.4	32.3
AC0082	26.0	27.0	1.0	56.5	82.1	15.6	61.1	15.1
AC0082	33.0	40.0	7.0	41.9	152.2	13.2	60.6	17.1
AC0083	21.0	27.0	6.0	34.7	95.6	14.1	69.5	20.7
AC0084	9.0	26.0	17.0	76.1	148.6	19.9	82.3	20.5
AC0084	36.0	38.0	2.0	38.1	84.4	10.2	41.1	10.1
AC0085	11.0	16.0	5.0	45.3	113.2	16.9	81.6	23.1
AC0086	32.0	33.0	1.0	98.6	194.1	26.8	101.7	19.9
AC0086	36.0	38.0	2.0	101.2	120.9	17.9	73.0	15.0
AC0087	45.0	56.0	11.0	100.5	470.4	27.4	108.7	24.8
AC0088	31.0	37.0	6.0	166.1	330.9	42.7	170.5	36.3
AC0089	26.0	29.0	3.0	354.2	404.1	95.6	365.5	71.5
AC0089	30.0	35.0	5.0	64.9	198.9	15.2	60.6	13.7
AC0090	51.0	52.0	1.0	80.6	52.0	22.7	89.0	16.2
AC0091	23.0	25.0	2.0	73.8	207.6	19.4	69.0	14.2
AC0091	31.0	38.0	7.0	131.7	328.0	36.5	134.7	27.5
AC0092	55.0	59.0	4.0	43.7	72.1	11.8	47.6	9.9
AC0092	75.0	77.0	2.0	123.7	23.4	32.3	124.5	34.4
AC0093	57.0	58.0	1.0	33.4	92.3	13.8	55.3	13.8
AC0093	59.0	60.0	1.0	35.9	106.4	13.2	49.9	15.1
AC0093	61.0	75.0	14.0	54.3	40.0	14.5	58.0	15.8
AC0094	43.0	52.0	9.0	143.2	260.1	38.0	144.9	30.4
AC0095	21.0	24.0	3.0	22.9	70.1	10.7	57.5	17.7
AC0096	29.0	35.0	6.0	127.6	346.0	40.5	159.1	34.5
AC0097	38.0	48.0	10.0	223.0	182.9	52.7	206.8	46.1
AC0097	49.0	50.0	1.0	56.2	75.2	9.6	38.0	8.7
AC0098	26.0	29.0	3.0	91.6	234.8	32.4	137.8	30.9
AC0098	33.0	36.0	3.0	44.6	74.0	11.5	53.0	12.9
AC0099	22.0	26.0	4.0	63.7	166.1	23.8	113.5	27.8
AC0100	20.0	23.0	3.0	444.3	551.6	94.7	307.5	47.1
AC0100	28.0	35.0	7.0	83.2	232.1	25.6	118.4	27.0

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HoleID	From (m)	To (m)	Interval (m)	Eu2O3 ppm	Gd2O3 ppm	Tb4O7 ppm	Dy2O3 ppm	Ho2O3 ppm
AC0037	51.0	53.0	2.0	3.7	18.9	3.0	18.6	3.8
AC0037	54.0	57.0	3.0	3.0	14.7	2.4	16.1	3.4
AC0037	58.0	61.0	3.0	2.3	15.9	2.6	17.3	3.7
AC0040	30.0	40.0	10.0	6.1	27.6	4.7	30.9	6.9
AC0043	42.0	43.0	1.0	23.6	69.7	9.5	45.3	7.7
AC0043	44.0	51.0	7.0	8.1	27.5	4.1	24.1	4.6
AC0082	26.0	27.0	1.0	5.2	19.1	3.2	19.1	4.3
AC0082	33.0	40.0	7.0	6.4	20.5	3.4	19.5	4.2
AC0083	21.0	27.0	6.0	11.2	30.2	5.4	37.1	8.1
AC0084	9.0	26.0	17.0	5.9	24.8	4.3	30.1	6.5
AC0084	36.0	38.0	2.0	1.6	11.5	2.1	14.2	3.0
AC0085	11.0	16.0	5.0	7.7	31.5	5.3	36.1	7.8
AC0086	32.0	33.0	1.0	5.4	18.4	2.4	13.8	2.5
AC0086	36.0	38.0	2.0	4.5	19.1	3.4	22.9	4.9
AC0087	45.0	56.0	11.0	7.6	27.5	4.5	29.9	6.5
AC0088	31.0	37.0	6.0	10.2	39.6	6.3	39.0	8.8
AC0089	26.0	29.0	3.0	15.5	59.8	8.4	44.5	8.3
AC0089	30.0	35.0	5.0	3.6	16.7	3.0	20.4	4.6
AC0090	51.0	52.0	1.0	3.9	11.4	1.6	7.8	1.4
AC0091	23.0	25.0	2.0	3.0	10.5	1.7	10.3	2.0
AC0091	31.0	38.0	7.0	6.5	24.9	4.0	25.0	5.3
AC0092	55.0	59.0	4.0	2.5	10.9	1.9	11.8	2.6
AC0092	75.0	77.0	2.0	9.9	47.2	8.4	61.4	12.9
AC0093	57.0	58.0	1.0	3.3	11.7	2.1	13.8	2.9
AC0093	59.0	60.0	1.0	3.6	12.3	2.4	16.2	3.2
AC0093	61.0	75.0	14.0	4.6	22.9	4.0	28.2	6.3
AC0094	43.0	52.0	9.0	10.3	31.0	4.9	30.8	6.2
AC0095	21.0	24.0	3.0	10.3	24.5	4.4	29.5	6.1
AC0096	29.0	35.0	6.0	10.0	33.9	5.5	34.5	7.2
AC0097	38.0	48.0	10.0	14.2	56.5	9.7	64.7	13.8
AC0097	49.0	50.0	1.0	2.4	10.9	1.5	10.1	2.3
AC0098	26.0	29.0	3.0	7.7	27.2	4.2	24.0	4.5
AC0098	33.0	36.0	3.0	4.2	18.9	2.9	18.4	4.3
AC0099	22.0	26.0	4.0	8.4	31.1	5.1	30.9	6.6
AC0100	20.0	23.0	3.0	8.4	25.7	3.7	18.2	2.7
AC0100	28.0	35.0	7.0	5.5	28.4	4.7	30.6	6.4

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HoleID	From (m)	To (m)	Interval (m)	Er2O3 ppm	Tm2O3 ppm	Yb2O3 ppm	Lu2O3 ppm	Y2O3 ppm
AC0037	51.0	53.0	2.0	10.6	1.6	10.0	1.6	107.1
AC0037	54.0	57.0	3.0	10.9	1.6	11.8	1.7	107.5
AC0037	58.0	61.0	3.0	11.4	1.6	11.5	1.8	110.8
AC0040	30.0	40.0	10.0	21.5	2.8	19.1	2.6	252.1
AC0043	42.0	43.0	1.0	20.5	2.6	16.8	2.0	190.5
AC0043	44.0	51.0	7.0	13.4	1.8	11.7	1.6	138.3
AC0082	26.0	27.0	1.0	12.6	1.8	11.9	1.9	128.3
AC0082	33.0	40.0	7.0	12.2	1.9	12.4	1.9	104.3
AC0083	21.0	27.0	6.0	25.8	3.4	22.7	3.7	268.9
AC0084	9.0	26.0	17.0	21.4	3.2	20.8	3.2	225.9
AC0084	36.0	38.0	2.0	10.1	1.5	10.6	1.5	101.4
AC0085	11.0	16.0	5.0	25.1	3.5	22.3	3.6	262.5
AC0086	32.0	33.0	1.0	6.5	0.9	4.9	0.7	55.9
AC0086	36.0	38.0	2.0	17.1	2.2	14.6	2.3	174.9
AC0087	45.0	56.0	11.0	20.5	3.0	19.1	2.7	224.4
AC0088	31.0	37.0	6.0	26.2	3.6	22.0	3.5	290.9
AC0089	26.0	29.0	3.0	22.7	3.3	20.3	2.9	237.9
AC0089	30.0	35.0	5.0	14.1	2.1	14.3	2.2	138.5
AC0090	51.0	52.0	1.0	3.9	0.5	4.0	0.5	31.2
AC0091	23.0	25.0	2.0	6.2	0.8	6.5	0.9	57.0
AC0091	31.0	38.0	7.0	15.4	2.2	14.8	2.1	143.5
AC0092	55.0	59.0	4.0	7.8	1.2	8.2	1.3	64.0
AC0092	75.0	77.0	2.0	38.0	5.2	32.5	4.8	440.7
AC0093	57.0	58.0	1.0	8.8	1.3	9.8	1.6	48.3
AC0093	59.0	60.0	1.0	10.3	1.9	12.9	1.8	53.5
AC0093	61.0	75.0	14.0	19.1	2.8	16.5	2.7	194.9
AC0094	43.0	52.0	9.0	19.2	2.9	18.8	2.6	177.5
AC0095	21.0	24.0	3.0	18.9	2.7	18.6	3.0	196.0
AC0096	29.0	35.0	6.0	21.0	2.9	19.0	2.7	203.6
AC0097	38.0	48.0	10.0	41.6	5.6	34.2	5.0	481.4
AC0097	49.0	50.0	1.0	6.7	0.9	5.7	0.9	103.9
AC0098	26.0	29.0	3.0	12.6	1.7	11.2	1.6	117.2
AC0098	33.0	36.0	3.0	12.8	1.7	11.0	1.7	162.3
AC0099	22.0	26.0	4.0	19.1	2.8	17.4	2.6	180.1
AC0100	20.0	23.0	3.0	5.9	0.7	4.3	0.6	46.5
AC0100	28.0	35.0	7.0	19.0	2.9	19.1	2.9	179.2

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HoleID	From (m)	To (m)	Interval (m)	Sc2O3 ppm	Th ppm	U ppm	Nb ppm	Ta ppm
AC0037	51.0	53.0	2.0	17.9	7.8	2.2	10.3	0.7
AC0037	54.0	57.0	3.0	13.1	7.0	1.8	9.4	0.7
AC0037	58.0	61.0	3.0	11.5	6.6	2.2	8.9	0.7
AC0040	30.0	40.0	10.0	42.0	0.8	0.6	1.2	0.1
AC0043	42.0	43.0	1.0	37.7	5.6	3.1	6.3	0.4
AC0043	44.0	51.0	7.0	19.9	5.7	2.2	5.9	0.4
AC0082	26.0	27.0	1.0	13.7	6.2	2.4	7.6	0.8
AC0082	33.0	40.0	7.0	25.5	7.7	3.5	9.6	0.7
AC0083	21.0	27.0	6.0	70.6	1.3	2.2	9.2	0.5
AC0084	9.0	26.0	17.0	25.2	6.1	3.1	8.3	0.5
AC0084	36.0	38.0	2.0	10.6	9.7	2.0	9.7	0.7
AC0085	11.0	16.0	5.0	35.1	5.4	2.6	7.1	0.5
AC0086	32.0	33.0	1.0	38.7	4.4	2.9	4.7	0.4
AC0086	36.0	38.0	2.0	22.7	11.5	2.7	9.1	0.6
AC0087	45.0	56.0	11.0	55.0	2.4	1.5	4.2	0.3
AC0088	31.0	37.0	6.0	28.1	4.8	2.2	5.1	0.2
AC0089	26.0	29.0	3.0	22.9	6.9	2.3	7.0	0.4
AC0089	30.0	35.0	5.0	15.1	5.0	1.9	5.3	0.3
AC0090	51.0	52.0	1.0	21.9	2.3	1.1	5.3	0.3
AC0091	23.0	25.0	2.0	40.9	11.1	2.2	6.8	0.5
AC0091	31.0	38.0	7.0	17.9	5.5	2.2	5.5	0.3
AC0092	55.0	59.0	4.0	65.8	6.0	1.8	4.9	0.4
AC0092	75.0	77.0	2.0	54.2	4.0	1.5	2.6	0.3
AC0093	57.0	58.0	1.0	45.4	9.4	1.8	6.6	0.5
AC0093	59.0	60.0	1.0	52.1	7.4	2.5	7.4	0.5
AC0093	61.0	75.0	14.0	48.8	10.5	1.8	5.4	0.6
AC0094	43.0	52.0	9.0	20.9	5.4	1.6	6.7	0.4
AC0095	21.0	24.0	3.0	61.5	1.5	1.2	7.0	0.4
AC0096	29.0	35.0	6.0	21.0	5.8	3.0	7.1	0.5
AC0097	38.0	48.0	10.0	37.2	6.8	1.7	6.0	0.5
AC0097	49.0	50.0	1.0	21.9	6.4	1.1	7.6	0.5
AC0098	26.0	29.0	3.0	18.7	3.7	3.8	7.4	0.4
AC0098	33.0	36.0	3.0	15.2	3.3	1.4	7.5	0.4
AC0099	22.0	26.0	4.0	18.2	5.9	1.3	7.4	0.5
AC0100	20.0	23.0	3.0	51.3	5.4	3.0	7.3	0.5
AC0100	28.0	35.0	7.0	17.9	13.1	4.1	9.2	0.6

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HoleID	From (m)	To (m)	Zr ppm	Hf ppm	Co ppm	Cu ppm	Ni ppm
AC0037	51.0	53.0	344.0	8.6	3.0	1.0	3.0
AC0037	54.0	57.0	292.0	7.7	2.0	7.3	7.7
AC0037	58.0	61.0	253.0	6.7	1.7	9.3	4.7
AC0040	30.0	40.0	36.0	1.1	204.2	97.2	389.9
AC0043	42.0	43.0	225.0	5.2	7.0	31.0	21.0
AC0043	44.0	51.0	195.0	4.7	12.0	28.0	17.1
AC0082	26.0	27.0	216.0	5.0	5.0	32.0	21.0
AC0082	33.0	40.0	311.0	8.0	89.4	59.9	57.1
AC0083	21.0	27.0	455.0	8.9	31.8	25.2	12.8
AC0084	9.0	26.0	262.0	6.8	9.8	9.7	7.1
AC0084	36.0	38.0	219.0	6.7	3.0	4.0	4.0
AC0085	11.0	16.0	191.0	5.3	21.4	8.4	4.8
AC0086	32.0	33.0	134.0	3.5	5.0	43.0	22.0
AC0086	36.0	38.0	215.0	6.0	38.0	50.5	32.0
AC0087	45.0	56.0	140.0	3.5	123.6	114.8	37.5
AC0088	31.0	37.0	197.0	4.8	5.7	26.0	14.3
AC0089	26.0	29.0	237.0	5.8	16.7	54.7	32.3
AC0089	30.0	35.0	168.0	4.3	32.0	36.4	25.6
AC0090	51.0	52.0	226.0	4.9	8.0	33.0	16.0
AC0091	23.0	25.0	279.0	7.3	3.5	40.0	22.5
AC0091	31.0	38.0	189.0	4.6	27.1	29.7	30.4
AC0092	55.0	59.0	124.0	3.6	76.8	100.3	48.3
AC0092	75.0	77.0	67.0	2.0	67.0	121.5	145.0
AC0093	57.0	58.0	257.0	7.4	17.0	69.0	18.0
AC0093	59.0	60.0	208.0	5.7	27.0	89.0	31.0
AC0093	61.0	75.0	100.0	3.1	44.2	92.2	45.0
AC0094	43.0	52.0	242.0	6.0	9.6	55.0	55.4
AC0095	21.0	24.0	417.0	8.7	30.7	18.3	5.7
AC0096	29.0	35.0	239.0	5.4	8.7	24.5	15.3
AC0097	38.0	48.0	202.0	4.5	7.1	53.6	42.7
AC0097	49.0	50.0	264.0	5.8	11.0	19.0	31.0
AC0098	26.0	29.0	237.0	5.5	20.3	22.3	17.0
AC0098	33.0	36.0	271.0	5.8	32.0	14.7	8.7
AC0099	22.0	26.0	231.0	5.3	12.8	18.5	14.5
AC0100	20.0	23.0	260.0	6.4	5.0	20.0	34.7
AC0100	28.0	35.0	351.0	9.9	13.7	28.9	15.4

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APPENDIX 6: Drillhole significant intersections within HGMIN zone (Gallium oxide)

HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
MAFAC006	AC	2022	588370.0	6973470.0	433.1	MGA94_Z50	40	42	2	33.6
MAFAC008	AC	2022	588182.0	6973464.0	432.9	MGA94_Z50	52	56	4	25.5
MAFAC010	AC	2022	588700.0	6973310.0	434.0	MGA94_Z50	36	44	8	22.9
MAFAC011	AC	2022	588652.0	6973304.0	434.0	MGA94_Z50	32	36	4	20.2
MAFAC012	AC	2022	588604.0	6973311.0	433.9	MGA94_Z50	28	31	3	25.5
MAFAC013	AC	2022	588556.0	6973318.0	433.8	MGA94_Z50	28	32	4	24.2
MAFAC015	AC	2022	588460.0	6973310.0	433.8	MGA94_Z50	52	56	4	24.2
MAFAC016	AC	2022	588412.0	6973315.0	433.7	MGA94_Z50	64	68	4	25.5
MAFAC019	AC	2022	588248.0	6973326.0	433.5	MGA94_Z50	24	32	8	22.9
MAFAC022	AC	2022	588096.0	6973307.0	433.5	MGA94_Z50	24	28	4	25.5
MAFAC026	AC	2022	588281.0	6973177.0	434.1	MGA94_Z50	24	32	8	24.2
MAFAC027	AC	2022	588233.0	6973161.0	434.1	MGA94_Z50	20	24	4	22.9
MAFAC027	AC	2022	588233.0	6973161.0	434.1	MGA94_Z50	44	48	4	22.9
MAFAC031	AC	2022	588460.0	6972992.0	434.9	MGA94_Z50	20	24	4	34.9
MAFAC032	AC	2022	588403.0	6972997.0	434.8	MGA94_Z50	12	20	8	31.6
MAFAC034	AC	2022	588289.0	6973007.0	434.6	MGA94_Z50	16	20	4	21.5
MAFAC037	AC	2022	588158.0	6973010.0	434.5	MGA94_Z50	36	44	8	25.5
MAFAC038	AC	2022	588430.0	6973036.0	434.7	MGA94_Z50	12	16	4	24.2
MAFAC039	AC	2022	588386.0	6973060.0	434.6	MGA94_Z50	24	32	8	25.5
MAFAC040	AC	2022	588342.0	6972851.0	434.8	MGA94_Z50	16	20	4	29.6
MAFAC042	AC	2022	588238.0	6972837.0	434.6	MGA94_Z50	20	24	4	18.8
MAFAC043	AC	2022	588186.0	6972830.0	434.6	MGA94_Z50	28	32	4	32.3
MAFAC045	AC	2022	588082.0	6972832.0	434.5	MGA94_Z50	32	36	4	21.5
NSE009	AC	2022	591874.0	6978123.0	427.0	MGA94_Z50	53	54	1	21.6
NSE011	AC	2022	591436.0	6978035.0	427.0	MGA94_Z50	44	46	2	35.3
NSE012	AC	2022	591176.0	6978038.0	427.0	MGA94_Z50	36	37	1	29.6
NSE012	AC	2022	591176.0	6978038.0	427.0	MGA94_Z50	48	55	7	27.2
NSE013	AC	2022	590927.0	6978037.0	427.0	MGA94_Z50	51	53	2	26.3
NSE018	AC	2022	593276.0	6976746.0	438.0	MGA94_Z50	48	52	4	23.0
NSE024	AC	2022	592689.0	6976746.0	436.0	MGA94_Z50	58	59	1	36.2
NSE025	AC	2022	592588.0	6976746.0	436.0	MGA94_Z50	58	60	2	24.4
NSE026	AC	2022	592490.0	6976732.0	436.0	MGA94_Z50	48	51	3	20.7
NSE027	AC	2022	592377.0	6976753.0	435.0	MGA94_Z50	49	53	4	26.0
NSE028	AC	2022	592297.0	6976752.0	433.0	MGA94_Z50	57	60	3	33.2
NSE029	AC	2022	592203.0	6976755.0	435.0	MGA94_Z50	31	34	3	26.9
NSE031	AC	2022	592003.0	6976742.0	435.0	MGA94_Z50	38	41	3	26.1
NSE032	AC	2022	591893.0	6976756.0	434.0	MGA94_Z50	54	57	3	26.2
NSE034	AC	2022	591709.0	6976753.0	430.0	MGA94_Z50	49	53	4	25.5
NSE035	AC	2022	591588.0	6976745.0	430.0	MGA94_Z50	60	62	2	27.6
NSE036	AC	2022	591500.0	6976750.0	431.0	MGA94_Z50	52	56	4	29.0
NSE041	AC	2022	590992.0	6976757.0	430.0	MGA94_Z50	25	31	6	31.4
NSE042	AC	2022	590843.0	6976746.0	429.0	MGA94_Z50	27	33	6	29.1
NSE051	AC	2022	592103.0	6975306.0	431.0	MGA94_Z50	32	35	3	25.9
NSE052	AC	2022	591989.0	6975327.0	432.0	MGA94_Z50	40	41	1	26.2
NSE053	AC	2022	591880.0	6975329.0	432.0	MGA94_Z50	37	39	2	27.4
NSE058	AC	2022	591393.0	6975323.0	432.0	MGA94_Z50	24	26	2	27.1
NSE060	AC	2022	591206.0	6975342.0	433.0	MGA94_Z50	25	27	2	25.1
NSE065	AC	2022	590700.0	6975331.0	433.0	MGA94_Z50	21	23	2	23.5
NSE067	AC	2022	592408.0	6974402.0	435.0	MGA94_Z50	31	35	4	26.2
NSE070	AC	2022	592112.0	6974383.0	435.0	MGA94_Z50	8	10	2	22.5

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
NSE071	AC	2022	592015.0	6974391.0	435.0	MGA94_Z50	16	17	1	32.3
NSE073	AC	2022	591793.0	6974388.0	436.0	MGA94_Z50	28	30	2	27.6
NSE073	AC	2022	591793.0	6974388.0	436.0	MGA94_Z50	33	35	2	25.0
NSE074	AC	2022	591726.0	6974395.0	436.0	MGA94_Z50	24	27	3	22.9
NSE075	AC	2022	591604.0	6974401.0	436.0	MGA94_Z50	26	27	1	36.4
NSE094	AC	2022	590915.0	6973100.0	440.0	MGA94_Z50	32	34	2	29.0
NSE095	AC	2022	590834.0	6973076.0	440.0	MGA94_Z50	31	34	3	30.6
NSTAC001	AC	2022	587920.0	6972734.0	434.0	MGA94_Z50	40	44	4	25.5
NSTAC002	AC	2022	587879.0	6972730.0	433.9	MGA94_Z50	56	60	4	25.5
NSTAC003	AC	2022	587827.0	6972726.0	433.8	MGA94_Z50	64	72	8	31.6
NSTAC004	AC	2022	587780.0	6972722.0	433.8	MGA94_Z50	48	64	16	26.2
NSTAC005	AC	2022	587739.0	6972718.0	433.7	MGA94_Z50	20	28	8	29.6
NSTAC007	AC	2022	587629.0	6973000.0	434.0	MGA94_Z50	44	48	4	25.5
NSTAC008	AC	2022	587572.0	6972988.0	433.9	MGA94_Z50	32	36	4	28.2
NSTAC008	AC	2022	587572.0	6972988.0	433.9	MGA94_Z50	40	44	4	26.9
NSTAC009	AC	2022	587515.0	6973008.0	433.8	MGA94_Z50	36	40	4	26.9
NSTAC012	AC	2022	587900.0	6972850.0	434.3	MGA94_Z50	36	44	8	22.9
NSTAC015	AC	2022	587761.0	6972834.0	434.1	MGA94_Z50	60	64	4	21.5
NSTAC016	AC	2022	587720.0	6972831.0	434.1	MGA94_Z50	40	44	4	24.2
NSTAC017	AC	2022	587650.0	6972850.0	434.1	MGA94_Z50	32	36	4	25.5
NSTAC018	AC	2022	587606.0	6972840.0	434.0	MGA94_Z50	24	28	4	22.9
NSTAC021	AC	2022	587448.0	6972828.0	433.8	MGA94_Z50	12	20	8	20.2
NSTAC024	AC	2022	587740.0	6972710.0	433.7	MGA94_Z50	20	28	8	24.9
NSTAC027	AC	2022	590300.0	6975815.0	427.3	MGA94_Z50	16	17	1	24.5
NSTAC028	AC	2022	590185.0	6975795.0	426.8	MGA94_Z50	24	26	2	32.4
NSTAC028	AC	2022	590185.0	6975795.0	426.8	MGA94_Z50	29	35	6	28.8
NSTAC029	AC	2022	590105.0	6975798.0	426.7	MGA94_Z50	20	25	5	25.6
NSTAC030	AC	2022	589795.0	6975805.0	426.5	MGA94_Z50	19	20	1	27.3
NSTAC030	AC	2022	589795.0	6975805.0	426.5	MGA94_Z50	28	29	1	20.4
NSTAC032	AC	2022	589809.0	6975787.0	426.6	MGA94_Z50	21	28	7	18.9
NSTAC032	AC	2022	589809.0	6975787.0	426.6	MGA94_Z50	32	34	2	24.0
NSTAC033	AC	2022	589695.0	6975808.0	426.6	MGA94_Z50	21	23	2	22.7
NSTAC035	AC	2022	589508.0	6975810.0	426.6	MGA94_Z50	32	35	3	28.4
NSTAC043	AC	2022	588704.0	6975795.0	426.3	MGA94_Z50	56	58	2	27.0
NSTAC049	AC	2022	588105.0	6975805.0	425.8	MGA94_Z50	41	42	1	26.1
NSTAC051	AC	2022	587905.0	6975800.0	425.5	MGA94_Z50	46	48	2	24.4
NSTAC054	AC	2022	587628.0	6975813.0	425.4	MGA94_Z50	61	63	2	21.6
NSTAC056	AC	2022	590100.0	6974948.0	429.1	MGA94_Z50	40	43	3	25.2
NSTAC057	AC	2022	590000.0	6974948.0	429.1	MGA94_Z50	60	66	6	25.3
NSTAC058	AC	2022	589893.0	6974950.0	429.1	MGA94_Z50	29	31	2	36.3
NSTAC059	AC	2022	589797.0	6974949.0	429.2	MGA94_Z50	21	23	2	34.3
NSTAC059	AC	2022	589797.0	6974949.0	429.2	MGA94_Z50	45	48	3	31.0
NSTAC060	AC	2022	589701.0	6974948.0	429.1	MGA94_Z50	22	23	1	23.3
NSTAC060	AC	2022	589701.0	6974948.0	429.1	MGA94_Z50	41	44	3	27.6
NSTAC061	AC	2022	589600.0	6974952.0	429.1	MGA94_Z50	38	44	6	29.1
NSTAC063	AC	2022	589411.0	6974955.0	429.1	MGA94_Z50	33	36	3	26.6
NSTAC067	AC	2022	589002.0	6974951.0	429.0	MGA94_Z50	45	50	5	29.7
NSTAC068	AC	2022	588900.0	6974944.0	428.9	MGA94_Z50	25	28	3	22.6
NSTAC075	AC	2022	588200.0	6974950.0	428.3	MGA94_Z50	26	29	3	25.5
NSTAC080	AC	2022	587687.0	6974955.0	427.6	MGA94_Z50	34	36	2	20.5

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
NSTAC082	AC	2022	587484.0	6974973.0	427.4	MGA94_Z50	52	56	4	33.8
NSTAC084	AC	2022	590186.0	6973903.0	432.2	MGA94_Z50	35	39	4	27.5
NSTAC085	AC	2022	590103.0	6973915.0	432.2	MGA94_Z50	57	59	2	27.9
NSTAC086	AC	2022	589991.0	6973914.0	432.2	MGA94_Z50	26	29	3	25.5
NSTAC091	AC	2022	589509.0	6973899.0	432.4	MGA94_Z50	18	21	3	27.0
NSTAC092	AC	2022	589414.0	6973903.0	432.5	MGA94_Z50	9	11	2	26.6
NSTAC093	AC	2022	589306.0	6973879.0	432.6	MGA94_Z50	28	30	2	26.0
NSTAC094	AC	2022	589217.0	6973873.0	432.5	MGA94_Z50	18	20	2	25.3
NSTAC096	AC	2022	589018.0	6973876.0	432.4	MGA94_Z50	19	22	3	23.7
NSTAC097	AC	2022	588899.0	6973897.0	432.4	MGA94_Z50	18	29	11	26.3
NSTAC098	AC	2022	588797.0	6973883.0	432.3	MGA94_Z50	21	30	9	26.0
NSTAC099	AC	2022	588713.0	6973882.0	432.2	MGA94_Z50	21	25	4	30.5
NSTAC100	AC	2022	588593.0	6973900.0	431.9	MGA94_Z50	41	43	2	22.7
NSTAC101	AC	2022	588506.0	6973902.0	431.8	MGA94_Z50	30	34	4	32.8
NSTAC101	AC	2022	588506.0	6973902.0	431.8	MGA94_Z50	38	39	1	25.3
NSTAC101	AC	2022	588506.0	6973902.0	431.8	MGA94_Z50	44	47	3	23.4
NSTAC102	AC	2022	588413.0	6973916.0	431.7	MGA94_Z50	56	59	3	21.6
NSTAC103	AC	2022	588315.0	6973866.0	432.0	MGA94_Z50	51	52	1	26.3
NSTAC104	AC	2022	588204.0	6973901.0	431.6	MGA94_Z50	40	42	2	32.5
NSTAC105	AC	2022	588102.0	6973925.0	431.5	MGA94_Z50	35	36	1	24.2
NSTAC105	AC	2022	588102.0	6973925.0	431.5	MGA94_Z50	50	51	1	21.9
NSTAC106	AC	2022	588005.0	6973908.0	431.3	MGA94_Z50	39	43	4	27.2
NSTAC113	AC	2022	587309.0	6973893.0	430.3	MGA94_Z50	47	53	6	31.9
NSTAC119	AC	2022	589242.0	6973139.0	435.0	MGA94_Z50	20	25	5	22.2
NSTAC120	AC	2022	589165.0	6973139.0	435.0	MGA94_Z50	18	23	5	22.8
NSTAC121	AC	2022	589042.0	6973133.0	434.9	MGA94_Z50	10	15	5	21.9
NSTAC122	AC	2022	588951.0	6973123.0	434.9	MGA94_Z50	14	15	1	20.2
NSTAC123	AC	2022	588849.0	6973127.0	434.8	MGA94_Z50	16	18	2	20.5
NSTAC124	AC	2022	588764.0	6973151.0	434.6	MGA94_Z50	17	24	7	24.5
NSTAC125	AC	2022	588656.0	6973147.0	434.5	MGA94_Z50	25	26	1	23.7
NSTAC126	AC	2022	588533.0	6973178.0	434.3	MGA94_Z50	20	23	3	19.8
NSTAC129	AC	2022	587877.0	6973160.0	433.7	MGA94_Z50	54	56	2	22.4
NSTAC129	AC	2022	587877.0	6973160.0	433.7	MGA94_Z50	67	72	5	27.0
NSTAC130	AC	2022	587771.0	6973165.0	433.6	MGA94_Z50	69	72	3	25.4
NSTAC131	AC	2022	587671.0	6973150.0	433.5	MGA94_Z50	51	52	1	26.3
NSTAC131	AC	2022	587671.0	6973150.0	433.5	MGA94_Z50	53	55	2	27.1
NSTAC132	AC	2022	587586.0	6973153.0	433.4	MGA94_Z50	43	45	2	25.7
NSTAC132	AC	2022	587586.0	6973153.0	433.4	MGA94_Z50	47	48	1	24.5
NSTAC134	AC	2022	587347.0	6973154.0	432.9	MGA94_Z50	17	18	1	28.9
NSTAC141	AC	2022	586489.0	6973121.0	432.0	MGA94_Z50	22	28	6	25.2
NSTAC142	AC	2022	586381.0	6973121.0	432.0	MGA94_Z50	13	29	16	23.4
NSTAC143	AC	2022	586379.0	6973123.0	432.0	MGA94_Z50	13	29	16	27.6
NSTAC144	AC	2022	586205.0	6973127.0	431.5	MGA94_Z50	25	26	1	23.1
NSTAC145	AC	2022	585981.0	6973106.0	431.0	MGA94_Z50	14	17	3	20.0
NSTAC155	AC	2022	590705.0	6978036.0	430.0	MGA94_Z50	58	61	3	24.6
NSTAC160	AC	2022	590698.0	6976716.0	428.0	MGA94_Z50	28	31	3	24.7
NSTAC162	AC	2022	590493.0	6976734.0	428.0	MGA94_Z50	20	22	2	28.8
NSTAC162	AC	2022	590493.0	6976734.0	428.0	MGA94_Z50	28	29	1	31.1
NSTAC163	AC	2022	590392.0	6976745.0	427.6	MGA94_Z50	30	32	2	25.6
NSTAC164	AC	2022	590301.0	6976740.0	427.3	MGA94_Z50	31	37	6	26.8

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
NSTAC166	AC	2022	590094.0	6976751.0	426.6	MGA94_Z50	23	25	2	29.7
NSTAC166	AC	2022	590094.0	6976751.0	426.6	MGA94_Z50	29	38	9	28.7
NSTAC166	AC	2022	590094.0	6976751.0	426.6	MGA94_Z50	41	45	4	28.2
NSTAC167	AC	2022	589985.0	6976726.0	426.1	MGA94_Z50	60	62	2	29.2
NSTAC168	AC	2022	589904.0	6976733.0	425.8	MGA94_Z50	57	60	3	30.0
NSTAC170	AC	2022	589681.0	6976734.0	424.3	MGA94_Z50	28	38	10	27.1
NSTAC170	AC	2022	589681.0	6976734.0	424.3	MGA94_Z50	48	50	2	23.8
NSTAC171	AC	2022	589609.0	6976740.0	424.1	MGA94_Z50	30	38	8	25.1
NSTAC172	AC	2022	589494.0	6976757.0	424.0	MGA94_Z50	27	29	2	21.6
NSTAC174	AC	2022	590495.0	6975329.0	433.0	MGA94_Z50	24	29	5	17.5
NSTAC175	AC	2022	590391.0	6975325.0	431.5	MGA94_Z50	25	31	6	24.9
NSTAC176	AC	2022	590303.0	6975325.0	430.3	MGA94_Z50	22	23	1	21.8
NSTAC177	AC	2022	590204.0	6975330.0	428.8	MGA94_Z50	25	30	5	26.1
NSTAC178	AC	2022	590080.0	6975328.0	428.1	MGA94_Z50	36	37	1	29.7
NSTAC178	AC	2022	590080.0	6975328.0	428.1	MGA94_Z50	49	51	2	24.3
NSTAC180	AC	2022	589868.0	6975322.0	428.1	MGA94_Z50	42	45	3	24.8
NSTAC181	AC	2022	589791.0	6975336.0	428.1	MGA94_Z50	32	40	8	21.0
NSTAC284	AC	2022	590656.0	6973133.0	438.0	MGA94_Z50	28	29	1	28.2
NSTAC285	AC	2022	590552.0	6973147.0	438.0	MGA94_Z50	45	46	1	26.6
NSTAC286	AC	2022	590442.0	6973137.0	439.0	MGA94_Z50	46	48	2	25.3
NSTAC287	AC	2022	590344.0	6973148.0	439.0	MGA94_Z50	34	35	1	24.2
NSTAC288	AC	2022	590253.0	6973141.0	440.0	MGA94_Z50	32	34	2	25.4
NSTAC289	AC	2022	590145.0	6973178.0	439.0	MGA94_Z50	36	39	3	27.9
NSTAC289	AC	2022	590145.0	6973178.0	439.0	MGA94_Z50	52	54	2	26.3
NSTAC291	AC	2022	589953.0	6973140.0	437.7	MGA94_Z50	45	47	2	27.2
NSTAC298	AC	2022	590588.0	6972184.0	438.0	MGA94_Z50	27	32	5	23.1
NSTAC302	AC	2022	590183.0	6972222.0	438.0	MGA94_Z50	30	31	1	26.9
NSTAC304	AC	2022	590000.0	6972198.0	439.0	MGA94_Z50	26	27	1	26.5
NSTAC305	AC	2022	589892.0	6972204.0	439.0	MGA94_Z50	26	27	1	28.1
NSTAC305	AC	2022	589892.0	6972204.0	439.0	MGA94_Z50	33	35	2	28.3
NSTAC306	AC	2022	589760.0	6972216.0	438.0	MGA94_Z50	40	42	2	30.2
NSTAC307	AC	2022	589683.0	6972196.0	438.0	MGA94_Z50	33	34	1	25.5
NSTAC307	AC	2022	589683.0	6972196.0	438.0	MGA94_Z50	41	44	3	28.7
NSTAC308	AC	2022	589589.0	6972143.0	439.0	MGA94_Z50	50	55	5	28.4
NSTAC309	AC	2022	590588.0	6971298.0	438.0	MGA94_Z50	27	30	3	23.3
NSTAC310	AC	2022	590508.0	6971301.0	437.0	MGA94_Z50	26	30	4	23.6
NSTAC313	AC	2022	590217.0	6971303.0	431.0	MGA94_Z50	33	35	2	25.5
NSTAC316	AC	2022	589879.0	6971295.0	430.0	MGA94_Z50	28	29	1	35.8
NSTAC318	AC	2022	589717.0	6971303.0	431.0	MGA94_Z50	45	46	1	20.3
NSTAC320	AC	2022	589781.0	6975860.0	426.4	MGA94_Z50	24	25	1	25.5
NSTAC320	AC	2022	589781.0	6975860.0	426.4	MGA94_Z50	27	31	4	21.1
NSTAC321	AC	2022	589821.0	6975837.0	426.4	MGA94_Z50	25	26	1	26.9
NSTAC321	AC	2022	589821.0	6975837.0	426.4	MGA94_Z50	32	34	2	25.3
NSTAC322	AC	2022	589851.0	6975820.0	426.5	MGA94_Z50	32	36	4	26.3
NSTAC323	AC	2022	589740.0	6975788.0	426.6	MGA94_Z50	20	23	3	26.8
NSTAC324	AC	2022	589840.0	6975783.0	426.6	MGA94_Z50	37	38	1	33.2
NSTAC325	AC	2022	589779.0	6975748.0	426.7	MGA94_Z50	25	30	5	24.4
NSTAC326	AC	2022	589803.0	6975747.0	426.7	MGA94_Z50	29	32	3	26.1
NSTAC327	AC	2022	589837.0	6975734.0	426.8	MGA94_Z50	36	38	2	24.5
NSTAC328	AC	2022	589856.0	6975895.0	426.3	MGA94_Z50	20	28	8	31.7

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
23NSTRC022	RC	2023	588890.0	6975318.6	427.9	MGA94_Z50	46	51	5	30.5
23NSTRC030	RC	2023	586509.4	6974407.4	427.5	MGA94_Z50	30	35	5	22.2
23NSTRC032	RC	2023	586804.6	6974412.5	428.0	MGA94_Z50	20	25	5	25.7
23NSTRC033	RC	2023	586940.8	6974407.7	428.1	MGA94_Z50	26	28	2	31.8
23NSTRC039	RC	2023	587843.0	6974394.3	429.3	MGA94_Z50	32	36	4	33.2
23NSTRC040	RC	2023	587993.4	6974394.3	429.9	MGA94_Z50	30	33	3	23.7
23NSTRC043	RC	2023	588459.7	6974409.3	430.2	MGA94_Z50	22	25	3	24.5
23NSTRC044	RC	2023	588592.4	6974397.1	430.3	MGA94_Z50	17	22	5	22.9
23NSTRC046	RC	2023	588895.3	6974387.9	430.6	MGA94_Z50	21	31	10	25.6
23NSTRC047	RC	2023	589044.0	6974414.0	430.6	MGA94_Z50	29	32	3	31.9
23NSTRC048	RC	2023	589144.5	6974459.7	430.7	MGA94_Z50	47	48	1	34.5
23NSTRC053	RC	2023	589959.2	6974424.4	430.7	MGA94_Z50	51	54	3	31.8
23NSTRC054	RC	2023	590054.9	6974423.1	430.7	MGA94_Z50	46	49	3	34.0
23NSTRC055	RC	2023	590254.5	6974426.3	430.7	MGA94_Z50	49	51	2	29.6
23NSTRC056	RC	2023	590397.6	6974411.5	430.6	MGA94_Z50	69	71	2	26.2
23NSTRC058	RC	2023	586423.7	6973494.9	430.6	MGA94_Z50	18	20	2	27.6
23NSTRC058	RC	2023	586423.7	6973494.9	430.6	MGA94_Z50	23	26	3	23.7
23NSTRC058	RC	2023	586423.7	6973494.9	430.6	MGA94_Z50	55	59	4	25.5
23NSTRC061	RC	2023	587189.2	6973492.9	431.4	MGA94_Z50	34	37	3	33.6
23NSTRC062	RC	2023	587399.2	6973497.7	431.6	MGA94_Z50	40	41	1	25.3
23NSTRC063	RC	2023	587617.5	6973489.7	432.0	MGA94_Z50	46	51	5	28.1
23NSTRC070	RC	2023	589423.7	6973554.8	433.8	MGA94_Z50	29	30	1	28.5
23NSTRC070	RC	2023	589423.7	6973554.8	433.8	MGA94_Z50	33	35	2	28.4
23NSTRC071	RC	2023	589616.5	6973567.5	433.7	MGA94_Z50	33	40	7	28.5
23NSTRC072	RC	2023	589909.3	6973465.0	433.6	MGA94_Z50	41	42	1	25.5
23NSTRC076	RC	2023	589571.7	6973577.7	433.7	MGA94_Z50	33	40	7	29.2
DD001	DDH	2023	589807.0	6975787.3	426.6	MGA94_Z50	19	21	1.9	20.2
DD001	DDH	2023	589807.0	6975787.3	426.6	MGA94_Z50	21	27	5.9	20.4
DD001	DDH	2023	589807.0	6975787.3	426.6	MGA94_Z50	32	35	3	21.2
DD002	DDH	2023	589868.3	6975322.7	428.1	MGA94_Z50	42	45	3	25.6
DD003	DDH	2023	588893.3	6973895.1	432.4	MGA94_Z50	16	29	13.2	25.5
DD004	DDH	2023	589045.0	6974413.4	430.6	MGA94_Z50	30	32	2.1	29.4
DD005	DDH	2023	589494.1	6973714.3	433.2	MGA94_Z50	23	24	1.2	24.3
DD005	DDH	2023	589494.1	6973714.3	433.2	MGA94_Z50	26	26	0.3	21.9
DD006	DDH	2023	589811.3	6975559.4	427.2	MGA94_Z50	33	36	3.1	31.6
DD006	DDH	2023	589811.3	6975559.4	427.2	MGA94_Z50	40	40	0.4	14.8
DD007	DDH	2023	589602.1	6973902.9	432.3	MGA94_Z50	23	24	1.1	26.2
DD008	DDH	2023	589104.0	6975127.5	428.4	MGA94_Z50	39	48	9	23.5
DD008	DDH	2023	589104.0	6975127.5	428.4	MGA94_Z50	49	53	4	21.4
DD009	DDH	2023	589494.1	6973322.6	434.5	MGA94_Z50	30	33	2.4	29.4
DD010	DDH	2023	589042.9	6973134.8	434.9	MGA94_Z50	10	15	5.1	25.2
DD011	DDH	2023	589073.6	6975167.7	428.4	MGA94_Z50	51	57	6	19.7
IF001	AC	2023	587851.7	6975333.6	426.6	MGA94_Z50	38	39	1	26.3
IF002	AC	2023	587968.7	6975335.1	426.8	MGA94_Z50	32	36	4	22.9
IF004	AC	2023	588393.0	6975332.6	427.6	MGA94_Z50	22	30	8	24.3
IF006	AC	2023	588707.0	6975329.7	427.9	MGA94_Z50	31	33	2	27.4
IF009	AC	2023	589287.1	6975312.0	428.2	MGA94_Z50	69	71	2	26.2
IF010	AC	2023	589581.9	6975286.8	428.1	MGA94_Z50	53	55	2	36.6
IF010	AC	2023	589581.9	6975286.8	428.1	MGA94_Z50	67	69	2	25.8
IF011	AC	2023	587375.6	6975130.6	426.8	MGA94_Z50	31	34	3	24.6

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
IF011	AC	2023	587375.6	6975130.6	426.8	MGA94_Z50	46	51	5	24.4
IF012	AC	2023	587480.2	6975135.0	427.0	MGA94_Z50	51	53	2	27.4
IF014	AC	2023	587709.9	6975135.9	427.1	MGA94_Z50	40	49	9	28.6
IF017	AC	2023	588013.8	6975140.4	427.2	MGA94_Z50	29	32	3	28.5
IF018	AC	2023	588091.0	6975137.3	427.5	MGA94_Z50	27	32	5	26.7
IF019	AC	2023	588198.8	6975138.1	427.7	MGA94_Z50	20	24	4	24.3
IF020	AC	2023	588306.2	6975133.4	427.9	MGA94_Z50	23	24	1	22.9
IF020	AC	2023	588306.2	6975133.4	427.9	MGA94_Z50	31	33	2	25.3
IF021	AC	2023	588387.6	6975144.9	427.9	MGA94_Z50	22	23	1	18.3
IF024	AC	2023	588701.7	6975126.0	428.3	MGA94_Z50	37	39	2	24.5
IF026	AC	2023	589813.3	6975562.2	427.2	MGA94_Z50	33	36	3	30.5
IF026	AC	2023	589813.3	6975562.2	427.2	MGA94_Z50	40	41	1	29.8
IF028	AC	2023	589997.1	6975561.6	427.5	MGA94_Z50	32	34	2	23.8
IF031	AC	2023	589403.0	6975135.4	428.5	MGA94_Z50	21	27	6	38.6
IF031	AC	2023	589403.0	6975135.4	428.5	MGA94_Z50	55	59	4	29.5
IF032	AC	2023	589489.5	6975137.5	428.5	MGA94_Z50	23	30	7	40.4
IF033	AC	2023	589589.2	6975163.1	428.4	MGA94_Z50	24	26	2	39.5
IF033	AC	2023	589589.2	6975163.1	428.4	MGA94_Z50	44	45	1	31.9
IF034	AC	2023	589700.2	6975134.1	428.5	MGA94_Z50	52	54	2	21.6
IF035	AC	2023	589806.7	6975136.6	428.6	MGA94_Z50	56	57	1	29.6
IF036	AC	2023	589898.5	6975130.8	428.6	MGA94_Z50	40	45	5	29.7
IF040	AC	2023	587702.2	6974671.4	428.5	MGA94_Z50	33	37	4	24.2
IF041	AC	2023	587803.9	6974670.1	428.5	MGA94_Z50	23	26	3	25.3
IF044	AC	2023	588089.8	6974673.9	429.0	MGA94_Z50	22	24	2	24.9
IF046	AC	2023	588300.7	6974669.2	429.4	MGA94_Z50	18	20	2	22.1
IF047	AC	2023	588395.8	6974665.7	429.3	MGA94_Z50	14	15	1	23.3
IF049	AC	2023	588599.3	6974665.8	429.5	MGA94_Z50	17	20	3	22.0
IF049	AC	2023	588599.3	6974665.8	429.5	MGA94_Z50	24	27	3	23.3
IF050	AC	2023	588711.2	6974657.3	429.7	MGA94_Z50	33	38	5	26.9
IF052	AC	2023	588903.9	6974647.2	429.9	MGA94_Z50	27	30	3	22.4
IF053	AC	2023	588999.3	6974689.9	429.9	MGA94_Z50	24	32	8	28.6
IF054	AC	2023	589110.1	6974677.3	430.0	MGA94_Z50	37	42	5	23.8
IF055	AC	2023	589199.5	6974654.2	429.9	MGA94_Z50	31	36	5	26.5
IF056	AC	2023	589303.0	6974681.0	430.0	MGA94_Z50	29	31	2	26.9
IF060	AC	2023	589693.9	6974679.0	429.9	MGA94_Z50	37	40	3	29.9
IF062	AC	2023	589901.0	6974677.5	429.9	MGA94_Z50	35	39	4	27.3
IF070	AC	2023	587092.7	6974130.1	429.1	MGA94_Z50	33	36	3	23.5
IF070	AC	2023	587092.7	6974130.1	429.1	MGA94_Z50	39	41	2	22.6
IF071	AC	2023	587300.9	6974138.5	429.5	MGA94_Z50	37	45	8	25.9
IF073	AC	2023	587511.0	6974135.2	429.7	MGA94_Z50	41	42	1	32.1
IF075	AC	2023	587695.0	6974134.6	430.2	MGA94_Z50	39	41	2	23.6
IF079	AC	2023	588094.5	6974141.2	430.8	MGA94_Z50	35	38	3	24.8
IF080	AC	2023	588192.8	6974126.9	430.8	MGA94_Z50	36	38	2	24.4
IF081	AC	2023	588289.9	6974133.7	431.0	MGA94_Z50	33	38	5	21.9
IF082	AC	2023	588390.5	6974124.5	431.1	MGA94_Z50	36	38	2	25.1
IF085	AC	2023	588719.5	6974145.8	431.4	MGA94_Z50	19	21	2	23.7
IF086	AC	2023	588794.8	6974142.3	431.4	MGA94_Z50	30	35	5	28.2
IF087	AC	2023	588907.6	6974135.5	431.5	MGA94_Z50	26	30	4	22.9
IF088	AC	2023	589012.6	6974129.6	431.6	MGA94_Z50	24	31	7	23.7
IF096	AC	2023	589802.2	6974144.9	431.6	MGA94_Z50	25	27	2	22.2

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
IF097	AC	2023	589914.3	6974138.8	431.6	MGA94_Z50	26	27	1	28.9
IF107	AC	2023	587070.7	6973711.4	430.4	MGA94_Z50	26	27	1	18.5
IF109	AC	2023	587274.4	6973708.8	431.0	MGA94_Z50	44	46	2	32.3
IF109	AC	2023	587274.4	6973708.8	431.0	MGA94_Z50	49	50	1	35.4
IF112	AC	2023	587583.7	6973707.2	431.3	MGA94_Z50	40	44	4	24.6
IF112	AC	2023	587583.7	6973707.2	431.3	MGA94_Z50	46	47	1	21.4
IF113	AC	2023	587679.1	6973698.1	431.3	MGA94_Z50	21	23	2	28.5
IF115	AC	2023	587898.2	6973710.8	431.7	MGA94_Z50	22	24	2	24.6
IF117	AC	2023	588125.7	6973704.0	432.2	MGA94_Z50	25	32	7	25.9
IF119	AC	2023	588295.4	6973714.5	432.5	MGA94_Z50	35	37	2	21.2
IF121	AC	2023	588483.5	6973713.0	432.3	MGA94_Z50	32	33	1	22.7
IF123	AC	2023	588686.8	6973725.2	432.7	MGA94_Z50	14	15	1	30.8
IF123	AC	2023	588686.8	6973725.2	432.7	MGA94_Z50	33	35	2	13.8
IF124	AC	2023	588796.1	6973708.5	432.8	MGA94_Z50	23	26	3	32.2
IF125	AC	2023	588911.5	6973720.5	432.9	MGA94_Z50	17	19	2	29.2
IF125	AC	2023	588911.5	6973720.5	432.9	MGA94_Z50	23	28	5	21.9
IF126	AC	2023	589012.6	6973717.3	432.9	MGA94_Z50	21	26	5	22.0
IF128	AC	2023	589189.2	6973716.1	433.0	MGA94_Z50	21	22	1	23.0
IF129	AC	2023	589308.2	6973709.5	433.0	MGA94_Z50	20	22	2	22.7
IF130	AC	2023	589385.2	6973726.1	433.1	MGA94_Z50	25	27	2	23.2
IF132	AC	2023	587535.3	6973491.8	432.1	MGA94_Z50	44	45	1	38.0
IF133	AC	2023	587773.7	6973486.4	432.4	MGA94_Z50	43	48	5	23.6
IF134	AC	2023	588070.5	6973478.8	432.8	MGA94_Z50	26	28	2	26.9
IF135	AC	2023	589312.0	6973533.6	433.7	MGA94_Z50	21	25	4	24.0
IF136	AC	2023	589522.8	6973525.6	433.7	MGA94_Z50	25	28	3	26.5
IF137	AC	2023	589723.4	6973510.7	433.7	MGA94_Z50	37	41	4	26.2
IF138	AC	2023	589498.1	6973703.1	433.2	MGA94_Z50	23	26	3	24.5
IF140	AC	2023	589695.1	6973722.9	433.0	MGA94_Z50	18	19	1	26.1
IF141	AC	2023	589778.5	6973700.5	432.9	MGA94_Z50	21	23	2	23.1
IF144	AC	2023	586112.4	6973316.3	430.6	MGA94_Z50	15	16	1	20.8
IF144	AC	2023	586112.4	6973316.3	430.6	MGA94_Z50	23	25	2	19.2
IF145	AC	2023	586185.0	6973310.8	430.8	MGA94_Z50	31	32	1	31.6
IF146	AC	2023	586296.6	6973309.7	431.1	MGA94_Z50	15	17	2	27.5
IF146	AC	2023	586296.6	6973309.7	431.1	MGA94_Z50	20	25	5	26.1
IF147	AC	2023	586394.5	6973314.4	431.2	MGA94_Z50	20	24	4	24.0
IF148	AC	2023	586501.5	6973309.1	431.3	MGA94_Z50	13	18	5	23.8
IF149	AC	2023	586597.3	6973309.7	431.4	MGA94_Z50	11	20	9	25.5
IF150	AC	2023	586695.8	6973312.9	431.4	MGA94_Z50	13	19	6	27.8
IF151	AC	2023	586815.9	6973313.9	431.6	MGA94_Z50	14	16	2	24.5
IF153	AC	2023	587014.8	6973318.9	431.8	MGA94_Z50	43	46	3	27.6
IF155	AC	2023	587199.3	6973316.4	432.1	MGA94_Z50	32	40	8	31.8
IF157	AC	2023	587399.4	6973314.3	432.2	MGA94_Z50	24	26	2	30.0
IF158	AC	2023	587483.1	6973315.1	432.6	MGA94_Z50	25	30	5	28.0
IF159	AC	2023	587601.2	6973313.5	432.5	MGA94_Z50	48	50	2	29.1
IF160	AC	2023	587700.4	6973322.5	432.9	MGA94_Z50	39	40	1	28.5
IF161	AC	2023	587803.0	6973311.5	433.2	MGA94_Z50	51	54	3	26.3
IF162	AC	2023	587906.1	6973309.2	433.3	MGA94_Z50	29	37	8	21.4
IF163	AC	2023	588017.3	6973312.5	433.4	MGA94_Z50	30	35	5	30.6
IF164	AC	2023	588809.1	6973309.4	434.1	MGA94_Z50	18	22	4	28.7
IF165	AC	2023	588990.5	6973314.8	434.4	MGA94_Z50	17	26	9	22.9

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
IF166	AC	2023	588990.5	6973314.8	434.4	MGA94_Z50	17	26	9	26.3
IF167	AC	2023	589089.9	6973319.7	434.3	MGA94_Z50	29	40	11	26.1
IF168	AC	2023	589187.4	6973306.5	434.4	MGA94_Z50	17	21	4	24.1
IF169	AC	2023	589298.8	6973315.6	434.5	MGA94_Z50	26	31	5	25.0
IF170	AC	2023	589396.8	6973322.6	434.4	MGA94_Z50	29	30	1	28.8
IF170	AC	2023	589396.8	6973322.6	434.4	MGA94_Z50	34	37	3	28.7
IF171	AC	2023	589493.5	6973323.7	434.5	MGA94_Z50	31	33	2	28.5
IF172	AC	2023	589597.3	6973311.2	434.5	MGA94_Z50	17	24	7	25.3
IF173	AC	2023	589690.0	6973322.4	434.4	MGA94_Z50	25	27	2	26.8
IF174	AC	2023	589800.2	6973293.5	434.2	MGA94_Z50	28	39	11	24.6
IF177	AC	2023	586109.4	6972908.7	431.9	MGA94_Z50	20	26	6	24.5
IF178	AC	2023	586183.8	6972914.8	432.2	MGA94_Z50	23	30	7	25.6
IF179	AC	2023	586273.6	6972911.5	432.5	MGA94_Z50	28	35	7	25.1
IF180	AC	2023	586377.8	6972910.7	432.9	MGA94_Z50	16	29	13	27.0
IF182	AC	2023	586602.8	6972908.2	432.9	MGA94_Z50	17	26	9	28.3
IF183	AC	2023	586683.2	6972910.9	432.8	MGA94_Z50	42	46	4	26.1
IF184	AC	2023	586786.7	6972917.1	432.9	MGA94_Z50	31	50	19	26.2
IF185	AC	2023	586904.1	6972917.8	433.2	MGA94_Z50	27	31	4	34.9
IF186	AC	2023	587000.8	6972918.6	433.6	MGA94_Z50	26	30	4	33.7
IF188	AC	2023	587201.2	6972925.3	433.7	MGA94_Z50	29	31	2	27.4
IF189	AC	2023	587300.1	6972914.4	433.9	MGA94_Z50	15	22	7	21.2
IF190	AC	2023	588597.0	6972910.1	435.3	MGA94_Z50	16	20	4	25.8
IF191	AC	2023	588699.5	6972926.0	435.3	MGA94_Z50	14	16	2	21.4
IF192	AC	2023	588798.0	6972916.5	435.5	MGA94_Z50	16	22	6	22.8
IF193	AC	2023	588910.9	6972924.0	435.6	MGA94_Z50	26	29	3	24.2
IF194	AC	2023	588994.4	6972911.8	435.7	MGA94_Z50	27	31	4	27.0
IF196	AC	2023	589204.4	6972903.5	435.8	MGA94_Z50	12	13	1	26.3
IF196	AC	2023	589204.4	6972903.5	435.8	MGA94_Z50	24	26	2	27.7
IF197	AC	2023	589301.2	6972907.6	435.9	MGA94_Z50	17	18	1	29.8
IF197	AC	2023	589301.2	6972907.6	435.9	MGA94_Z50	25	30	5	27.1
IF198	AC	2023	589397.6	6972907.8	436.0	MGA94_Z50	30	38	8	29.3
IF199	AC	2023	589494.1	6972895.5	435.9	MGA94_Z50	29	33	4	25.3
IF200	AC	2023	589600.6	6972906.5	435.7	MGA94_Z50	21	26	5	23.4
IF201	AC	2023	589651.6	6972930.9	435.6	MGA94_Z50	21	25	4	25.3
IF203	AC	2023	587644.7	6975336.3	426.4	MGA94_Z50	54	57	3	31.2
IF205	AC	2023	587432.0	6975317.6	426.4	MGA94_Z50	28	29	1	27.8
IF205	AC	2023	587432.0	6975317.6	426.4	MGA94_Z50	55	56	1	31.6
IF206	AC	2023	589285.6	6975134.7	428.6	MGA94_Z50	21	27	6	38.0
IF206	AC	2023	589285.6	6975134.7	428.6	MGA94_Z50	34	35	1	31.9
IF206	AC	2023	589285.6	6975134.7	428.6	MGA94_Z50	49	53	4	32.1
IF206	AC	2023	589285.6	6975134.7	428.6	MGA94_Z50	61	66	5	29.8
IF208	AC	2023	589102.9	6975130.3	428.5	MGA94_Z50	39	52	13	27.3
IF209	AC	2023	588992.3	6975142.0	428.3	MGA94_Z50	32	34	2	31.4
IF210	AC	2023	589708.1	6975561.4	427.3	MGA94_Z50	41	45	4	31.7
IF213	AC	2023	589404.9	6975561.4	427.4	MGA94_Z50	26	27	1	19.6
IF217	AC	2023	589002.5	6975555.0	427.2	MGA94_Z50	49	52	3	22.5
IF218	AC	2023	588892.9	6975562.0	427.2	MGA94_Z50	59	64	5	29.6
IF219	AC	2023	588805.8	6975564.7	427.0	MGA94_Z50	62	67	5	24.1
IF220	AC	2023	588707.1	6975563.7	427.1	MGA94_Z50	56	65	9	32.1
IF220	AC	2023	588707.1	6975563.7	427.1	MGA94_Z50	72	77	5	23.7

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HoleID	Method	Year	East	North	RL	Grid	mFrom	mTo	mInterval	Ga_2O_3_ppm
IF221	AC	2023	588604.1	6975563.6	427.2	MGA94_Z50	50	53	3	23.2
IF222	AC	2023	588488.1	6975551.7	427.0	MGA94_Z50	46	47	1	24.6
IF228	AC	2023	587899.1	6975570.6	426.1	MGA94_Z50	42	43	1	22.0
IF229	AC	2023	587805.6	6975560.2	426.1	MGA94_Z50	41	44	3	27.3
IF231	AC	2023	587603.7	6975568.3	425.7	MGA94_Z50	59	61	2	26.3
IF232	AC	2023	587500.0	6975563.7	425.9	MGA94_Z50	37	41	4	22.3
IF232	AC	2023	587500.0	6975563.7	425.9	MGA94_Z50	45	46	1	24.9
IF238	AC	2023	589791.8	6973458.0	433.7	MGA94_Z50	39	40	1	26.3
AC0010	AC	2024	588504.0	6971376.3	441.2	MGA94_Z50	23	25	2	24.9
AC0011	AC	2024	588700.3	6971393.8	440.8	MGA94_Z50	24	28	4	26.7
AC0012	AC	2024	588891.3	6971379.8	440.7	MGA94_Z50	27	29	2	22.6
AC0015	AC	2024	588397.8	6972166.6	438.1	MGA94_Z50	18	24	6	27.7
AC0016	AC	2024	588597.5	6972171.7	437.9	MGA94_Z50	14	20	6	23.7
AC0017	AC	2024	588796.3	6972187.7	437.9	MGA94_Z50	13	20	7	22.1
AC0019	AC	2024	589185.0	6972175.2	438.3	MGA94_Z50	22	25	3	23.7
AC0020	AC	2024	589395.9	6972169.7	438.3	MGA94_Z50	18	20	2	26.3
AC0021	AC	2024	585878.0	6973686.2	428.8	MGA94_Z50	19	20	1	32.4
AC0022	AC	2024	586077.2	6973695.7	429.2	MGA94_Z50	22	29	7	27.2
AC0023	AC	2024	586265.3	6973707.8	429.4	MGA94_Z50	27	28	1	24.1
AC0023	AC	2024	586265.3	6973707.8	429.4	MGA94_Z50	44	46	2	29.6
AC0024	AC	2024	586464.7	6973695.2	429.8	MGA94_Z50	21	28	7	36.7
AC0024	AC	2024	586464.7	6973695.2	429.8	MGA94_Z50	29	32	3	32.9
AC0024	AC	2024	586464.7	6973695.2	429.8	MGA94_Z50	51	52	1	32.9
AC0025	AC	2024	586676.1	6973705.4	430.2	MGA94_Z50	12	14	2	23.0
AC0027	AC	2024	586117.4	6973910.9	428.4	MGA94_Z50	16	18	2	30.7
AC0028	AC	2024	586330.1	6973897.1	429.0	MGA94_Z50	15	20	5	25.8
AC0028	AC	2024	586330.1	6973897.1	429.0	MGA94_Z50	40	43	3	22.7
AC0029	AC	2024	586521.0	6973902.4	429.3	MGA94_Z50	14	20	6	23.1
AC0029	AC	2024	586521.0	6973902.4	429.3	MGA94_Z50	26	29	3	22.2
AC0029	AC	2024	586521.0	6973902.4	429.3	MGA94_Z50	46	48	2	18.0
AC0030	AC	2024	586711.4	6973921.6	429.4	MGA94_Z50	22	27	5	26.3
AC0040	AC	2024	589926.5	6977446.8	421.8	MGA94_Z50	30	40	10	20.1
AC0084	AC	2024	586587.6	6973323.5	431.4	MGA94_Z50	12	20	8	26.1
AC0085	AC	2024	586609.4	6973307.1	431.4	MGA94_Z50	11	17	6	25.5
AC0086	AC	2024	589620.9	6973585.4	433.6	MGA94_Z50	36	37	1	23.9
AC0087	AC	2024	589105.1	6975146.5	428.3	MGA94_Z50	40	52	12	29.3
AC0088	AC	2024	589630.1	6973563.7	433.7	MGA94_Z50	32	36	4	21.0
AC0089	AC	2024	589091.7	6973334.4	434.3	MGA94_Z50	29	39	10	21.8
AC0091	AC	2024	589103.5	6973315.9	434.4	MGA94_Z50	32	35	3	23.3
AC0092	AC	2024	588699.5	6975581.5	427.1	MGA94_Z50	56	59	3	27.8
AC0092	AC	2024	588699.5	6975581.5	427.1	MGA94_Z50	75	77	2	22.6
AC0093	AC	2024	588719.4	6975563.9	427.1	MGA94_Z50	64	67	3	27.1
AC0093	AC	2024	588719.4	6975563.9	427.1	MGA94_Z50	72	74	2	24.3
AC0094	AC	2024	589882.3	6975129.1	428.6	MGA94_Z50	43	47	4	29.5
AC0096	AC	2024	590188.5	6975802.5	426.8	MGA94_Z50	29	35	6	29.0
AC0097	AC	2024	589910.5	6975133.4	428.5	MGA94_Z50	40	45	5	30.0
AC0098	AC	2024	589822.1	6975808.7	426.5	MGA94_Z50	33	34	1	22.3
AC0099	AC	2024	590169.5	6975832.2	426.7	MGA94_Z50	22	25	3	25.6
AC0100	AC	2024	589803.8	6975768.7	426.6	MGA94_Z50	20	27	7	26.9
AC0100	AC	2024	589803.8	6975768.7	426.6	MGA94_Z50	29	33	4	28.2

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APPENDIX 1: 2012 JORC CODE - TABLE 1

Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as downhole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information*	• Victory Metals Australia (ASX:VTM) completed one Air-core (AC) drilling campaign at North Stanmore during the period September – November 2024. • Victory Metals Australia (ASX:VTM) completed one Air-core (AC) drilling campaign and a diamond drilling program at North Stanmore during the period September-December 2023. • Victory Metals Australia (ASX:VTM) completed a reverse circulation (RC) drilling programme a reverse circulation (RC) drilling programme from January–March 2023. • (AC) holes were drilled vertically and spaced 100m apart along 200m - 400m spaced drill lines. • (AC) drilling samples were collected as 1-m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite. • Each sample was then split using a 3-tier (87.5% - 12.5%) splitter and the split sample was placed into calico sample bags for transport to Perth. • Sample weights and recoveries were recorded on site and weighed 1.5 - 2.5 kg depending on the sample recovery from the drill hole. The mean bulk sample weight was 8.45kg. • A reputable commercial transport company was used to transport the bags. • A handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REO (Rare earth element) geochemistry (La, Ce, Pr, Nd and Y) from the 1-m sample piles. pXRF reading times were 45 secs over 3 cycles for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their integrity was checked using Certified REO -bearing geochemical standards. • The handheld pXRF is used as a guide to the relative presence or absence of certain elements, including REOs vectors (La, Ce, Pr, Nd and Y) to help direct the sampling program. Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. REO anomalism thresholds are determined by VTM technical lead based on historical data analysis • Victory attended North Stanmore to collect the green sample bag which was transported by Victory to Victory's secure warehouse in Perth. • Measures taken to ensure sample representivity included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight. • RC drill samples were collected as 1-m samples from the rig cyclone and placed on top of black plastic, that was laid on the natural ground surface to prevent contamination, in separate piles and in orderly rows.

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Criteria	JORC Code explanation	Commentary
		A hand-held trowel was used to collect 4-m composite samples from the 1-m piles. Compositing did not account for lithology changes. These composite samples weighed between 2 and 3 kg
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	• (AC) drilling uses a three bladed steel or tungsten drill bit to penetrate the weathered layer of loose soil and rock fragments. The drill rods are hollow and feature an inner tube with an outer barrel (similar to RC drilling). • (AC) drilling uses small compressors (750 cfm/250 psi) to drill holes into the weathered layer of loose soil and fragments of rock. • (RC) Drilling used a 5½" face sampling hammer with 1,350cfm/500 psi onboard compressor, which was occasionally supplemented with an additional booster (2,100cfm/1,000 psi). • After drilling is complete, an injection of compressed air is unleashed into the space between the inner tube and the drill rods inside wall, which flushes the cuttings up and out of the drill hole through the rod's inner tube, causing Less chance of cross-contamination. • (AC) drill rigs are lighter in weight than other rigs, meaning they are quicker and more manoeuvrable in the bush. • (AC) Drilling was performed by Seismic Drilling Pty Ltd and Orlando Drilling Pty Ltd, and the RC drilling was performed by Orlando Drilling Pty Ltd. • The drill rigs were regularly inspected by VTM personnel and contract staff. The drill rig with automatic rod handlers, with fire and dust suppression systems, mobile and radio communications, qualified and ticketed safety trained operators and offsiders, are required by Victory's work health and safety systems.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• The majority of samples were dry and sample recovery was variable, where excessive water flows were encountered during drilling. • Representative percussion drillhole samples were collected as 1-meter intervals, with corresponding chips placed into chip trays and kept for reference at VTM's facilities. • Measures taken to ensure sample representivity and recovery included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	• All percussion samples in the chip trays were lithologically logged using standard industry logging software on a notebook computer. • All (AC) samples have been logged for lithology, alteration, quartz veins, colour, fabrics. • All (AC) samples have been analysed by a handheld pXRF. • All samples were subjected to a NIR spectrometer for the identification of minerals and the variations in mineral chemistry to detect alteration assemblages and regolith profiles. • All geological information noted above has been completed by a competent person as recognized by JORC.

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Criteria	JORC Code explanation	Commentary
	• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.*	• Logging is qualitative in nature. • (AC) samples have been photographed.
	• *The total length and percentage of the relevant intersections logged.*	• 90% of the sample intervals were logged.
Subsampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.*	• Diamond drilling was PQ core. • Half core samples were taken, with the exception of when twin samples were collected and then the samples were quarter core.
	• *If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.*	• Air core and RC sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. • Most 1-meter samples were dry and weighed between 1.5 and 2.5 kgs. • Samples from the cyclone were placed into green drill bags in laid out in orderly rows on the ground. • Using a hand-held trowel, 1m samples were collected from the one-meter drill bags after splitting of the sample. • These samples were placed into calico bags and weighed between 1.5 and 2.5 kgs.

	• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*	• Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory. The assay methods used include:
		  ○ ME-4ACD81: Four acid digestion followed by ICP-AES measurement
		  ○ ME-MS81: Lithium borate fusion followed by acid dissolution and ICP-AES measurement
		  ○ ME-ICP06: Fusion decomposition followed by ICP-AES measurement
		• REOs were all analysed by ME-MS81 (four acid digestion followed by ICP-AES measurement) with results returned in their elemental form. Elements were then converted to oxides using the appropriate stoichiometric conversion factors.
		• Base metals are assayed by ME-ICP06: Fusion decomposition.
		• Non-ferrous metals are assayed by ME-4ACD81: Four acid digestion.

	• *Quality control procedures adopted for all subsampling stages to maximise representivity of samples.*	• Using a riffle splitter, 1m composite samples were collected from the individual sample bags. • Quality control of the assaying comprised the collection of a bulk repeat sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples. The repeat sample was collected by passing the bulk reject obtained from the first split stage through the riffle splitter once more. The repeat sample is not a duplicate.

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Criteria	JORC Code explanation	Commentary
	• *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.*	• Fourteen twin samples of quarter core (diamond PQ) were compared to the original sample for each REO element and results were found to be acceptable.
	• *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Composite samples weighed between 1 and 2 Kg's. • Sample sizes are considered appropriate to the grain size of the material being sampled.

Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	• All samples were analysed in the field using a handheld Olympus Vanta XRF unit to identify geochemical thresholds. These results are not considered dependable without calibration using chemical analysis. They were used as a guide to the relative presence or absence of certain elements, including REOs to help guide the drill program and which samples were submitted for analytical analysis.
		• All pXRF anomalous samples were sent to ALS Wangara in Perth for analysis. Over time the mineralised sample criteria has evolved from an initial sampling threshold value of La+Ce+Nd+Pr+Y > 200ppm (for the RSC MRE), to Ce>30ppm (for the post RSC to July 2024 MRE), and most recently Y>30ppm (POST July 2024 to April 2025 MRE).
		• Samples were submitted for sample preparation and geochemical analysis by ALS in Wangara, Perth, a NATA accredited laboratory. All samples were crushed and pulverized to generate a pulp aliquot sample with 95% of the aliquot sample passing 75µ (ALS methods CRU-31, PUL-31). Aliquots were analysed using the following methods:
		  ○ Lithium borate fusion prior to acid dissolution and ICP-AES (ALS method ME-MS81, a total assay technique) for Ba, Ce, Cr, Cs, Dy, Er, Eu, Ga, Gd, Hf, Ho, La, Lu, Nb, Nd, Pr, Rb, Sc, Sm, Sn, Sr, Ta, Tb, Th, Ti, Tm, U, V, W, Y, Yb, and Zr.
		  ○ Lithium borate fusion prior to acid dissolution and ICP-AES (ALS method ME-ICP06, a total assay technique) for Al2O3, BaO, CaO, Cr2O3, Fe2O3, K2O, MgO, MnO, Na2O, P2O5, SiO2, SrO, TiO2, and Total.
		  ○ 4-acid digest and read by ICP-AES (ALS method ME-4ACD81, a partial assay technique) for Ag, As, Cd, Co, Cu, Li, Mo, Ni, Pb, Sc, Tl, and Zn (base metals).
		  ○ Thermogravimetric analysis to determine loss on ignition (LOI) content.
		• The sample preparation and analysis are considered appropriate for the analytes.

	• *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	• At Victory's Perth facility spot checks were completed on selected samples using a handheld Olympus Vanta XRF unit. The pXRF device was used to determine anomalous REO geochemistry (La, Ce, Nd, Pr and Y) from the 1-m sample piles. • pXRF reading times were 45 secs over 3 beams for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their analytical accuracy was checked using REO -bearing geochemical standards. • The pXRF results were not used for estimation.
	• *Nature of quality control procedures adopted (e.g. standards, blanks,*	• Sample weights were measured for 174 of the AC drillholes, and recovery was measured for 7 of the diamond drillholes. Sample recovery for the diamond drillholes recovery was 103%. Based on the

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	duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	information available, sample recovery is acceptable for the diamond holes. The discrepancy between the target weight and the measured weight for the air-core samples indicates potential for bias, however, there may have been an issue with the target weight, and this should be reassessed.
		• Assay analytical precision was established by laboratory repeats and was deemed acceptable to the CP.
		• The overall performance of standards was deemed to be acceptable, see **Error! Reference source not found.**.
		  ○ It was noted that La, Pr, Ce and Eu in the CRM OREAS464 have expected values above the detection limits of the lab method ME_MS81.
		  ○ It was noted that Co and Ni in the CRMs OREAS461 and OREAS464 are over reported against the expected values using the lab method ME_4ACD81.
		  ○ It was noted that Cu and Sc in the CRM OREAS464 are under reported against the expected values using the lab method ME_4ACD81.
		• The overall performance of the blanks was deemed to be acceptable, see **Error! Reference source not found.**.
		• Field diamond duplicate data points taken from the same drillholes is available only for 14 samples from diamond drill core. The mean grade of the original sample was generally reproduced by the duplicate for the various analytes and is acceptable to the CP's.
		• In April 2024, 37 samples were submitted to an umpire laboratory, Intertek Genalysis in Perth. The results were compared to the original assay results from ALS laboratories for the key analytes of interest to the project. There was no observable bias between the original assays completed by ALS and the checks completed by Intertek Genalysis Perth.
		• Twinned hole results are discussed in the relevant section below.

Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.*	• Victory's representative Prof Kenneth Collerson (PhD, FAusIMM) undertook verification of significant intersections.
	• *The use of twinned holes.*	• Eleven percussion (air core and RC) drillholes have been twinned with diamond drilling (DD001 to DD011). Samples were submitted to the laboratory for analysis only if the initial screening by handheld pXRF satisfied the anomalous value threshold as set by company policy, whereas the diamond drilling was sampled and assayed along the entire length of the drillhole. • QQ plots were prepared between the percussion and diamond assays paired at 5m, with good correlation between the two drillhole types.
	• *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*	• ALS laboratories routinely re-assayed anomalous assays as part of their normal QAQC procedures
	• *Discuss any adjustment to assay data.*	• REO assay results were adjusted to convert elemental values to the oxide equivalent for REOs. The stoichiometric conversion factors used are provided below: **Element** | **Oxide** | **Element to stoichiometric oxide conversion factor**

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Ce (Cerium)	CeO_2	1.2284
Dy (Dysprosium)	Dy_2O_3	1.1477
Er (Erbium)	Er_2O_3	1.1435
Eu (Europium)	Eu_2O_3	1.1579
Ga (Gallium)	Ga_2O_3	1.3442
Gd (Gadolinium)	Gd_2O_3	1.1526
Ho (Holmium)	Ho_2O_3	1.1455
La (Lanthanum)	La_2O_3	1.1728
Lu (Lutetium)	Lu_2O_3	1.1371
Nd (Neodymium)	Nd_2O_3	1.1664
Pr (Praseodymium)	Pr_6O_{11}	1.2082
Sc (Scandium)	Sc_2O_3	1.5338
Sm (Samarium)	Sm_2O_3	1.1596
Tb (Terbium)	Tb_4O_7	1.1762
Tm (Thulium)	Tm_2O_3	1.1421
Y (Yttrium)	Y_2O_3	1.2699
Yb (Ytterbium)	Yb_2O_3	1.1387

Criteria	JORC Code explanation	Commentary
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	• 51% of the drillholes were surveyed by RTK/DGPS. The remaining holes were surveyed by handheld GPS with a horizontal accuracy of +/- 5 m. Elevation values (Z) were assigned from the topography surface where no DGPS data was available. • There were no downhole surveys completed. Drill holes were both vertical (92%) and inclined (8%). The majority of drill intervals (99%) were less than a drill hole depth of 100m.
	• *Specification of the grid system used.*	• All coordinates are in GDA94 Zone 50.
	• *Quality and adequacy of topographic control.*	• A three second SRTM Digital Elevation Model was used to represent the topographical surface sourced from Geoscience Australia. The topography was adjusted by using the DGPS surveyed collar coordinates to model a more accurate topographical surface. It is recommended that a LiDAR based DEM is used in future.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.*	• The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m.
	• *Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*	• Given the nature of the exploration programs, the spacing of the exploration drilling is appropriate for understanding the exploration potential and the identification of structural controls on the mineralisation. In areas of closer spaced drilling the spacing demonstrates grade and geological continuity sufficient to support Indicated Mineral Resources. Where drillhole spacing increases, grade and geological continuity can be implied and has been classified as an Inferred Mineral Resource. Areas where the drillhole spacing is

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Criteria	JORC Code explanation	Commentary
		such that grade and geological continuity cannot be implied, have been excluded from the Mineral Resource. • The applied Mineral Resource classification is commensurate with the grade continuity demonstrated.
	• *Whether sample compositing has been applied.*	• Percussion samples were collected as 1.0m samples. Core was collected at a nominal 1.0m samples. Air core samples were collected as 1.0m and 4.0m samples. Core, percussion and air core samples were composited to 1.0m for grade estimation purposes.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	• Mineralisation is sub horizontal, as such the vertical drillholes are suitable to test mineralisation thickness. • It is concluded from aerial magnetics that the mineralisation trends 010-030. Dips are unknown as the area is covered by a 2-25m blanket of transported cover. • Air core drilling was vertical as the mineralisation is interpreted to be sub parallel to the regolith profile. RC percussion drilling was angled. • Downhole widths of mineralisation are known with percussion drilling methods to +/- 1 meter.
	• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Mineralisation is sub-horizontal. Azimuths and dips of drilling was designed to intersect the strike of the rocks at right angles.
Sample security	• *The measures taken to ensure sample security.*	• All samples were packaged and managed by VTM personnel. • Larger packages of samples were couriered to Core from Cue by professional transport companies in sealed bulka bags. • Unused samples from the percussion drilling are stored at Victory's secure warehouse in Perth.

Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• MEC conducted an audit of the project data and the historic MRE in April of 2024. The findings were as follows -
		  ○ Several validation issues have now been corrected in the drillhole database, and the data is of sufficient quality to inform an Indicated and Inferred mineral resource.
		  ○ There are no downhole surveys so there is a risk of the hole paths deviating from planned, particularly with the deeper drillholes >100m which account for less than 1% of all drilled metres.
		  ○ Satisfactory QAQC data (standards, blanks, and pulp repeats) are available to support the MRE.

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Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The North Stanmore REO Project MRE comprises ten tenements E20/0544, E20/0871, E20/0971, E20/1016, E20/2468, E20/2469, P20/0543, P20/2007, P20/2153, and P20/2403. All tenements are held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory Metals Ltd. MEC has verified that at the time of the report date that all tenements are currently in good standing. • Native Title claim WC2004/010 (Wajarri Yamatji #1) was registered by the Yaatji Marlpa Aboriginal Corp in 2004 and covers the entire project area, including Coodardy and Emily Wells.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• The area has been previously explored by Harmony Gold (2007-2010) in JV with Big Bell Ops, Mt Kersey (1994- 1996), and Westgold (2011), and Metals X (2013). • Exploration by these companies has been piecemeal and not regionally systematic. • Harmony Gold intersected 3m @ 2.5 g/t Au and 2m @ 8.85 g/t Au in the Mafeking Bore area but did not follow up these intersections. • Other historical drill holes in the area commonly intersected > 100 ppb Au. • There has been no historical exploration for REOs in the tenement.
Geology	• *Deposit type, geological setting and style of mineralisation*	• Victory's tenements lie north of Cue, within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgaranga greenstone belts, the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late faults. The greenstone belts were intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions. • Two large Archaean gabbroid intrusions occur south of Cue. These are the Dalgaranga-Mount Farmer gabbroid complex in the southwest, and the layered Windimurra gabbroid complex in the southeast. The North Stanmore alkaline intrusion, north of Cue, was not recognised on regional geological maps. The petrological and geochemical data indicate that it is post-tectonic and post Archean in age. Similar alkaline intrusions in the vicinity of Cue are interpreted to be related to the early Proterozoic plume track responsible for alkaline magmatism, that extends in a belt from Mt Weld through Leonora to Cue.

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Criteria	JORC Code explanation	Commentary
		• Mafic and ultramafic sills are abundant in all areas of the Cue greenstones. Gabbro sills are often differentiated with basal pyroxenite and/or peridotite and upper leucogabbric units. • The greenstones are deformed by large scale fold structures which are dissected by major faults and shear zones which can be mineralised. Two large suites of granitoids intrude the greenstone belts. • The western margin of the project has a signature reflecting a rhyolite, rhyolite-dacite and/or dacitic rock (predominantly acid or felsic rock type). This coincides with an area of elevated TREO/LREO/HREO grades and greater average mineralisation thickness. • The deposit type is regolith-hosted REO mineralisation overlying the North Stanmore alkaline intrusion. The REO mineralisation at North Stanmore is predominantly hosted within a relatively flat-laying saprolite-clay horizon and partially extends into the Sap rock. The Saprolite is covered by 0–36m of unconsolidated colluvium. The saprolite thickness ranges from 14–58m, and overlies a basement of granite, mafic rocks, and other felsic rocks. Mineralogy studies demonstrate that the REOs are mainly hosted by sub-20-µm phases interpreted to be churchite (after xenotime) and rhabdophane (after monazite). The mineralisation is hosted in the saprolite zone of the weathering profile, between the basement granite and surface colluvium.

Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*
	  ○ *easting and northing of the drill hole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*
		• Seven hundred and fifty-five (755) drill holes for 42,118.9m, inclusive of 694 Air-core (AC) drillholes for 38,188m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory from 2022 to 2024.
		• Drillhole coordinates are shown in **APPENDIX 4** of the JORC MRE report.
		• Drillhole intersections are reported in **APPENDIX 5** of the JORC MRE report, > 330ppm TREO + Sc_2O_3.
		• Drillhole intersections are reported in **APPENDIX 6** of the JORC MRE report for Gallium oxide within the HGMIN zone.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g., cutting of high grades) and cut-off grades are usually Material and should be stated.*	• No top cuts were applied as few extreme values were identified. • Samples were composited to 1m intervals based on the dominant raw sample length. • A geological cutoff grade of 150ppm TREO + Sc representing the on-set of mineralisation was used during interpretation to separate mineralised from unmineralised material for the

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Criteria	JORC Code explanation	Commentary
	• *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	MIN domain. A high-grade (HGMIN) domain was modelled above a TREO + Sc 600ppm cut-off. • All MRE were reported above an economic cut-off grade of 330ppm TREO + Sc.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• The clay regolith hosted REO mineralisation is interpreted to be sub horizontal. • 88% of the drillholes are vertical, and the remaining are drilled at a dip of -60˚. As such intersections approximate the true width of mineralised lodes.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views*	• Drillhole collars and tenements are shown below -

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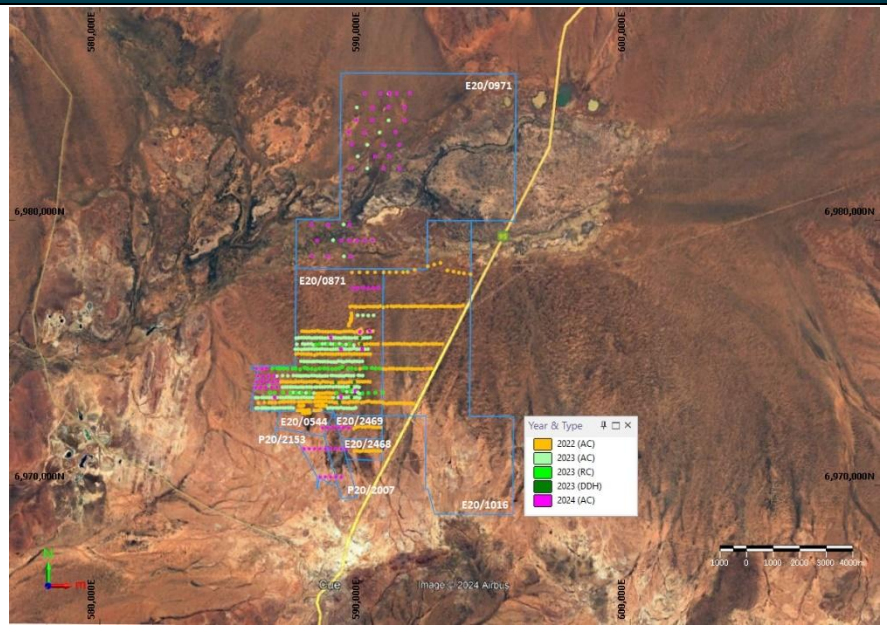
Criteria	JORC Code explanation	Commentary
		
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All exploration results have been reported above a 150ppm TREO + Sc cut-off.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances*	• Metallurgical testwork: ○ Three stages of metallurgical test work have been completed on the North Stanmore project, focusing on beneficiation, and on leach test work to establish potential recoveries ○ Core Resources ("Core") in Brisbane completed Stage 3 test work including beneficiation test work in March of 2024 and reported an increase, to the Rare Earth Element ("REO") feed grade of 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material.

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		○ The Leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide plus Yttrium (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trialled at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREO"). ○ Additionally, Scandium oxide (Sc_2O_3) recoveries of (50%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO and Sc_2O_3 from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Further metallurgical testwork will focus on further optimization of the leaching of the upgraded samples and the generation of Mixed Rare Earth Carbonate (MREC) for potential off takers. Additional variability leach testing of individual samples is also planned. Variability leach testwork will inform geo-metallurgical variability across the North Stanmore project. Further metallurgical test work will also focus on the most optimized leaching conditions and removal of gangue materials against the higher rare earth extractions that can be achieved. • Mincore Melbourne have been appointed to conduct a Scoping Study on the North Stanmore Project

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Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	• An initial Database was supplied to MEC by RSC, the database was then integrated with newly acquired data by MEC for a data audit before commencing an MRE. All validation issues relating to data were identified and remedied prior to MRE.
	• *Data validation procedures used.*	• Drillhole collar, downhole survey, assay, geology, and recovery data were imported into Micromine software. • The imported data was then compared to the database values with no discrepancies identified. • The data was then desurveyed in Micromine and reviewed spatially with no discrepancies identified.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	• Dean O'Keefe, the competent person for this Mineral Resource Estimate visited the North Stanmore project site on May 30, 2024.
	• *If no site visits have been undertaken indicate why this is the case.*	• A site visit has been conducted by Dean O'Keefe.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	• Confidence in the interpretation of the transported colluvium that truncates the saprolite is commensurate with the drillhole spacing and ranges from low to moderate confidence. • The mineralisation is hosted within the saprolite, with some mineralisation extending into the bedrock. • There is reasonable confidence in the interpretation of the saprolite commensurate with the available drilling.
	• *Nature of the data used and of any assumptions made.*	• Surface AC, RC, as well as diamond drilling, have been used to inform the MRE.
	• *The effect, if any, of alternative interpretations on Mineral Resource estimation.*	• The potential for alternate interpretations at a prospect scale is considered unlikely. However, there is a likelihood of variation at the local scale, and this has been reflected in the Mineral Resource classification.
	• *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• The MRE has been interpreted as mineralised domains (MIN) representing the on-set of REO mineralisation at 150ppm TREO + Sc_2O_3, and high-grade pods (HGMIN) within the mineralised domains where the mineralisation grade is greater than 600ppm TREO + Sc_2O_3.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The North Stanmore deposit extends over 8km across and along strike and is around 70m thick; mineralisation varies between 4m to 60m in true thickness. • The southwestern part of the deposit is thicker than the remainder of the deposit.

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Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*	• The final interpretational wireframes and estimation work was completed using Micromine v2024.5. • The estimation was constrained by hard domain boundaries generated from mineralisation wireframes. • The available samples were coded by domains (HGMIN, MIN), and 1.0m composites were created honouring these boundaries. • The REO analyte grades were estimated using ordinary kriging of the 1.0m composite grades each of the individual REO grades: HREO, and LREO. • The estimation for credit elements was completed using Inverse Distance Cubed for Cu, Ni, Co, Hf, Sc_2O_3, and Ga_2O_3. • There were no extreme values observed that required topcuts to be applied. • For estimation purposes, all boundaries were treated as hard boundaries. • The primary search was 500 m in the direction of maximum continuity, 400 m along the intermediate direction of continuity, and 25 m in the minor direction of continuity. Up to 5 samples per octant sector (maximum number of informing samples was 40 samples) were used. • The secondary search was 1,000 m in the direction of maximum continuity, 800 m along the intermediate direction of continuity, and 50 m in the minor direction of continuity, up to 5 samples per octant sector (maximum of 40 informing samples) was used. • The third search was 1,500 m in the direction of maximum continuity, 1,200 m along the intermediate direction of continuity, and 75m in the minor direction of continuity, with a maximum of 150 informing samples (no octant search applied). • The maximum distance for extrapolation for the Inferred Mineral Resource was 1,500 m. • Values were calculated for HREO, LREO, and TREO + Sc by summing the respective REO estimated grades and Scandium oxide for each OBM block.
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*	• The April 2025 MEC MRE was compared to the August 2023 RSC MRE and the July & November 2024 MEC MRE's.

MRE	CUTOFF ppm	Tonnage Mt	TREO ppm	TREO + Sc_2O_3 ppm	MREO ppm	HREO ppm	NdPr ppm	TREO t	TREO + Sc_2O_3 t
RSC Aug 2023	400	250	520		110	170	90	130,000	
MEC July 2024	330	235		520	107	180	87		122,300
MEC Nov 2024	330	250		525	108	178	89		131,250
MEC Jan 2025	330	247		520	107	176	88		128,690

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<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>

An economic cutoff grade of TREO + Sc ≥330ppm was applied to the MEC April 2025 MRE due to scandium oxide, being a potential credit element along with the presence of hafnium, nickel, cobalt, and copper.
MEC reported the MRE at a reduced cut-off grade to the RSC MRE as the TREO + Sc was inclusive of scandium oxide.
The April 2025 MEC Indicated and Inferred Mineral Resource for the North Stanmore Project is estimated at ~247 Mt of REE-bearing saprolite and bedrock at 520 ppm TREO + Sc2O3, for 128,690 tonnes of contained TREO + Sc2O3. The MEC Mineral Resource is not limited to tenement E20/871. However, the April 2025 MEC MRE incorporated additional drillhole data which compensated for the discrepancy with the RSC estimate.
A like for like comparison of the April 2025 MEC MRE with the historic RSC MRE is RSC 250Mt for 520ppm TREO versus the April 2025 MEC MRE within tenement E20/871 of 91.5Mt for 522 TREO, when restricted to the same reporting area. A significant difference in tonnage resulted from the RSC estimation issue.

<table>
<tr><th></th><th>CUTOFF ppm</th><th>Tonnage Mt</th><th>TREO ppm</th><th>TREO + Sc_2O_3 ppm</th><th>MREO ppm</th><th>HREO ppm</th><th>NdPr ppm</th><th>TREO t</th></tr>
<tr><td>RSC Aug 2023</td><td>400</td><td>250</td><td>520</td><td>NR</td><td>110</td><td>170</td><td>90</td><td>130,000</td></tr>
<tr><td>MEC Jan 2025</td><td>330</td><td>91.5</td><td>522</td><td>548</td><td>114</td><td>187</td><td>93</td><td>47,700</td></tr>
</table>
</td></tr>
<tr><td></td><td>• The assumptions made regarding recovery of by-products.</td><td>

Test work has demonstrated that Scandium is recoverable and may become a byproduct.
Test work has demonstrated that Gallium is recoverable and may become a byproduct.
Available metallurgical test work has demonstrated that likely processing will be able to recover significant proportions of Scandium, Gallium, Nickel, Cobalt, Copper and Hafnium.

</td></tr>
<tr><td></td><td>• Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).</td><td>

Test work completed by Victory Metals included analysis of Uranium (U) and Thorium (Th) levels across the project.
The assessed levels of uranium and thorium were very low values across the project. Due to the low values within both ore and waste the uranium and thorium were not estimated, however, both values may be estimated in the future if required for integration into processing studies.

Waste
U Max = 24ppm, Mean = 1.7ppm
Th Max = 67ppm, Mean = 7.9ppm

MIN Domain (≥150ppm TREO + Sc_2O_3)
U Max = 12ppm, Mean = 2.11ppm
Th Max = 61ppm, Mean = 7.15ppm
</td></tr>
</table>

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Criteria	JORC Code explanation	Commentary
		HGMIN Domain (≥600ppm TREO + Sc_2O_3) U Max = 11ppm, Mean = 1.8ppm Th Max = 68ppm, Mean = 6.9ppm • Metallurgical recovery to date of deleterious Uranium (U) 2.4ppm and Thorium (Th) 5ppm are less than average abundances in the upper continental crust (U) 3ppm (Th) 10ppm. • Scandium oxide, Gallium oxide, Hafnium, Copper, Cobalt, and Nickel were estimated within this MRE and are considered significant. • Sulphur (S) has not been analysed by the laboratory and cannot currently be estimated.
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*	• Drillhole spacing is consistent and varies in the East and North-East of the deposit. Nominal drillhole spacing is 50 x 50m expanding to ~250 north by 100m east across strike. • The block size used for the estimation 50m east x 50m north and 1 mRL, with sub celled blocks to 25m east x 25m north and 0.5mRL.
	• *Any assumptions behind modelling of selective mining units.*	• No support correction was applied to allow for selective mining units at this stage of the project life.
	• *Any assumptions about correlation between variables*	• No assumptions were made regarding correlations between variables.
	• *Description of how the geological interpretation was used to control the resource estimates.*	• A geological cutoff grade of 150ppm was chosen to distinguish the mineralised material from poorly unmineralised material. • The mineralised domain MIN was then Interpreted at 150ppm TREO Sc_2O_3 reflecting the on-set of mineralisation. • The interpretation was carried out in section lines and a high-grade mineralised domain HGMIN was delineated at 600ppm TREO + Sc_2O_3.
	• *Discussion of basis for using or not using grade cutting or capping.*	• Few extreme values were present and no topcuts were applied.

	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*	• The OBM estimate was validated, validation approaches included:
		  ○ Visual checks for composite grades versus estimated block grades.
		  ○ Comparison of global mean grades of composites versus blocks for each Domain. This check ensures that the global statistics for each estimated variable represent the composited statistics in that domain.
		  ○ Histograms of composites versus block distributions to check preservation of the distribution post-estimate.

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		○ Swath plots (also known as trend plots) to compare the spatial variation of grades between composites and blocks across the block model. ○ On completion of the OBM, checks were conducted for overlapping or missing blocks, and none were found. • Primary relevant elements of interest were estimated individually (Dy_2O_3, Er_2O_3, Eu_2O_3, Gd_2O_3, Ho_2O_3, La_2O_3, Lu_2O_3, Nd_2O_3, Pr_6O_{11}, Sm_2O_3, Tb_4O_7, Tm_2O_3, Y_2O_3, Yb_2O_3, Sc_2O_3, Ga_2O_3).
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages were estimated on a dry basis.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The MRE was reported at a 330ppm TREO + Sc_2O_3 cutoff grade. • The RSC August 2023 MRE economic cut-off grade was ≥400 ppm TREO, inclusive of Yttrium. The economic cut-off grade for the April 2025 MEC MRE was ≥330ppm TREO + Sc_2O_3, inclusive of Yttrium oxide and Scandium oxide. Asra Minerals Limited (ASX: ASR) reported in an ASX Announcement, 16 April 2024, a maiden JORC (2012) Mineral Resource Estimate (MRE) for its 100%-owned Yttria Rare Earth Element (REE) deposit, located on its Mt Stirling Project near Leonora in the northern Goldfields region of Western Australia. The MRE was reported above an economic cut-off grade of 200 ppm TREO, inclusive of Yttrium, minus CeO_2. Asra Minerals Ltd commented that this cut-off grade was selected based on the evaluation of other clay hosted rare earth Mineral Resources.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources* • • *not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• The CP's deem that there are reasonable prospects for eventual economic extraction using open pit mining methods as a function of: ○ The relative shallow depth of the mineralisation and presence of loosely consolidated transported Colluvium above the mineralisation. ○ Proximity to significant existing infrastructure (located adjacent to the Gt Northern Highway and the township of Cue). • Future pit optimisation studies will confirm the designation of the blocks for RPEEE.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and*	• Extensive metallurgical studies by Core metallurgy regarding the beneficiation and extraction of Ce, Dy, Er, Eu, Ga, Gd, Ho, La, Lu, Mn, Nd, Pr, Sc, Sm, Tb, Th, Tm, U, Y, and Yb have been completed.

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	parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	• The leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trailed at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREO"). • Additionally, Scandium oxide (Sc_2O_3) recoveries of (50%) were achieved and Gallium oxide (Ga_2O_3) recoveries of (34%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO, Sc_2O_3 and Ga_2O_3 from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The North Stanmore prospect is located in the Murchison of Western Australia, a mining district with considerable mining history and well understood environmental standards and protocols. • No environmental assumptions were made for the MRE. Scoping studies will assess these requirements in the future.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*	• Downhole geophysical density is available for 10 diamond drillholes at 10cm depth increments, for a total of 5,896 readings. • Core length, diameter and weight are available for 8 of the diamond drillholes for 50 readings • Regression analysis was performed to compare the two different approaches to measuring density. • A single density value was applied to each geology domain regardless of mineralisation profile. Densities were used to estimate the MRE tonnage.
	• *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity,*	• Downhole density measurements were obtained from 10 diamond drillholes at 10cm depth increments, for 5,896 readings. No anomalous density readings were observed in the data. Downhole geophysical density measurements were

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<tr><td></td><td>etc.), moisture and differences between rock and alteration zones within the deposit.</td><td>taken in rod, then corrected to account for this, using a factor calculated from a calibration drillhole (DD004).</td></tr>
<tr><td></td><td>• Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</td><td>• Core length, diameter and weight are available for 8 of the diamond drillholes for a total of 50 readings. From this information, density was calculated using the formula:
$$Density = \frac{m}{\pi r^2 h}$$
• Where “r” is the radius of the PQ core (0.0425m), “h” is the length of the core in metres, and “m” is the mass in kilograms. The density was converted from kg/m3 to g/cm3 for consistency with units used for downhole geophysical density. Four anomalous calculated density values were identified where density <1 g/cm3. Regression analysis was applied to calculate the density from geophysical measurements for the high grade and low-grade domains. The mean density from regression analysis for the High-grade domain is 1.75t/m3, and for the low-grade domain 2.02t/m3.
• The following densities have been applied to the MRE.
<table><tr><th>Geology domain</th><th>Dry bulk density (t/m^3)</th></tr><tr><td>Colluvium</td><td>1.70</td></tr><tr><td>Saprolite (LG & HG)</td><td>1.80</td></tr><tr><td>Basement (LG & HG)</td><td>2.10</td></tr></table></td></tr>
<tr><td>Classification</td><td>• The basis for the classification of the Mineral Resources into varying confidence categories.</td><td>• Mineral Resources were classified as Indicated and Inferred. Material not classified as either indicated or inferred Material remains unclassified and has been reported as an Exploration Target. Indicated Mineral Resource classification was based on drillhole spacing (250 x 100m closing to 50 x 50m in some areas), acceptable underlying QAQC, and RTK/DGPS survey of drillhole collar. The DGPS survey provided increased certainty regarding the drillhole collar location and compensated for a low-resolution topography survey. The topographical surface was adjusted to include the DGPS surveyed drillhole collar coordinates.</td></tr>
</table>

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		• 71% (by tonnage) of the MRE are classified as Indicated Mineral Resources, 29% (by tonnage) are classified as Inferred Mineral Resources.
	• *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*	• Grade and tonnage estimation has been considered for the MRE classification. • The CP's have considered all relevant factors
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• The MRE classification of Inferred and Indicated MRE reflects the CP's understanding of the deposit.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• MEC has conducted an internal review of the RSC August 2023 MRE.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.*	• No statistical test of the accuracy and confidence in the MRE has been undertaken. The low variability of the mineralisation grades, the relatively consistent mineralisation geometry, the geometry and large areal extent of the mineralisation provide qualitative confidence in the MRE.
	• *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.*	• The estimate is considered a good global estimate, and the relative confidence in the underlying data (QAQC), drillhole spacing, geological continuity and interpretation, has been appropriately reflected by the CP's in the Resource Classification.
	• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• There has been no production at the North Stanmore project.